

ORDINANCE NO. 01-2026

AN ORDINANCE OF THE CITY OF DELTONA, FLORIDA, AMENDING THE OFFICIAL ZONING MAP TO REZONE APPROXIMATELY 14.43 ACRES OF LAND LOCATED AT 2830, 2846, AND 2855 LAKE HELEN OSTEEN ROAD FROM RESIDENTIAL ESTATE ONE (RE-1) TO MIXED USE PLANNED UNIT DEVELOPMENT (MPUD); PROVIDING FOR RECORDING, CONFLICTS, SEVERABILITY, AND AN EFFECTIVE DATE.

WHEREAS, the City of Deltona, Florida (the “City”), has received an application from New Hope Baptist Church of Deltona, Inc. and New Hope Church of Deltona, Inc. (the “Applicant”) to rezone ±14.43-acres of land located at 2830, 2846, and 2855 Lake Helen Osteen Road, Deltona, Florida 32738 (the “Subject Property”) from Residential Estate-One (RE-1) to Mixed Use Planned Unit Development (MPUD); and

WHEREAS, the Applicant has stipulated to a Master Development Plan, certain allowable and prohibited uses, housing affordability restrictions, parking requirements, enhanced landscaping standards, architectural controls, transportation/traffic impacts, development phasing, and other miscellaneous conditions applicable to the Subject Property, as further described in the Development Agreement and associated exhibits attached hereto and incorporated herein; and

WHEREAS, the City and its Planning and Zoning Board, sitting as the Local Planning Agency, have complied with the requirements of the Municipal Home Rule Powers Act, sections 166.011 et. seq., Florida Statutes, in considering the proposed MPUD rezoning; and

WHEREAS, after said public hearing, the City Commission of the City of Deltona, Florida, has determined that the MPUD zoning is consistent with the Comprehensive Plan of the City of Deltona, Florida.

**NOW, THEREFORE, BE IT ORDAINED BY THE CITY COMMISSION OF
THE CITY OF DELTONA, FLORIDA, AS FOLLOWS:**

Section 1. Findings. The foregoing Whereas clauses are hereby ratified and incorporated as the legislative intent of this ordinance.

Section 2. Property Zoning Amendment Approved. Located in the City of Deltona, Florida this Mixed Planned Unit Development (MPUD) zoning amendment is hereby approved and includes Exhibit "A", Development Agreement as a written agreement for the Mixed-Use Planned Unit Development, Exhibit "B", Legal Description depicting the land hereby rezoned from R1-AA to MPUD, Exhibit "C", Master Development Plan, Exhibit "D", Elevations, Exhibit "E", and Traffic Impact Analysis. The following identification numbers are included for this zoning amendment: 8110-00-00-0041, 8110-00-00-0080, and 8110-00-00-0070.

Section 3. Recording. The Applicant shall record and shall be responsible for all costs incurred in recording, this Ordinance and all exhibits hereto in the Public Records of Volusia County, Florida.

Section 4. Conflicts. Any and all Ordinances or parts of Ordinances in conflict herewith are hereby repealed.

Section 5. Severability. If any provision of this Ordinance or the application thereof to any person or circumstance is held invalid, such invalidity shall not affect any other provision or application of this Ordinance which can be given effect without the invalid provision or application.

Section 6. Effective Date. This Ordinance shall take effect immediately upon its final adoption by the City Commission.

**PASSED AND ADOPTED BY THE CITY COMMISSION OF THE CITY OF
DELTONA, FLORIDA THIS _____ DAY OF _____, 2026.**

First Reading: _____

Advertised: _____

Second Reading: _____

BY: _____

Santiago Aliva, Jr., MAYOR

ATTEST:

Joyce Raftery, CMC, MMC, CITY CLERK

Approved as to form and legality
for use and reliance of the City of
Deltona, Florida

TG Law PLLC, CITY ATTORNEY

| Name | Yes | No |
|---------------|-----|----|
| Avila-Vazquez | | |
| Colwell | | |
| Heriot | | |
| Howington | | |
| Nabicht | | |
| Santiago | | |
| Avila | | |

**THIS INSTRUMENT PREPARED BY
AND AFTER RECORDING RETURN TO:**

Gemma Torcivia
TG Law PLLC
City Attorney
City of Deltona
2345 Providence Boulevard
Deltona, Florida 32725

Exhibit “A” to Ordinance No. 01-2026

DEVELOPMENT AGREEMENT

for the project known as New Hope Mixed-Use Planned Unit Development (MPUD) located at 2830, 2846 and 2855 Lake Helen Osteen Rd., Deltona, FL 32738 (hereinafter referred to as the “Subject Properties”).

THIS DEVELOPMENT AGREEMENT (hereinafter referred to as the “Agreement”) is entered into and made as of the ____ day of _____, 2026, by and between the CITY OF DELTONA, a Florida municipal corporation, with a mailing address of 2345 Providence Boulevard, Deltona, Florida 32725, (hereinafter referred to as the “City”), and New Hope Baptist Church of Deltona, Inc., (hereinafter referred to as the “Owner”), and Tacolcy Economic Development Corporation, Inc., (hereinafter referred to as the “Developer”).

W I T N E S S E T H

WHEREAS, the Owner warrants that it holds legal title to the lands located in Volusia County, Florida, and within the corporate limits of the City of Deltona, said lands being more particularly described in **Exhibit “B”**, legal description for the Subject Properties, attached hereto and by this reference made a part hereof; and that the holders of any and all liens and encumbrances affecting such properties will subordinate their interests to this Agreement; and

WHEREAS, the Owner has clear title of the Subject Properties, and the Developer is currently under contract to purchase the Subject Properties and intends to develop such properties as a MPUD; and

WHEREAS, the Developer desires to facilitate the orderly development of the Subject Properties in compliance with the laws and regulations of the City and of other governmental authorities, and the Developer desires to ensure that its development is compatible with other properties in the area and planned traffic patterns; and

WHEREAS, the development permitted or proposed under this Agreement is consistent with the City's Comprehensive Plan, concurrency management system, and all land development regulations and this Agreement does not replace, supersede, or grant variances to those regulations; and

WHEREAS, it is the purpose of this Agreement to clearly set forth the understanding and agreement of the parties concerning the matters contained herein; and

WHEREAS, the Developer have sought the City's approval to develop the Subject Properties, and the City approved Ordinance No. 01-2026, through rezoning the Subject Properties to a form of Planned Unit Development (PUD), as defined under the City's Land Development Code on Section 110-319. The PUD shall consist of this Agreement as the Written Agreement of the PUD and an **Exhibit "C"**, Master Development Plan (MDP), attached hereto and by this reference made a part hereof as the Preliminary Plan, subject to the covenants, restrictions, and easements offered by the Developer and contained herein, (hereinafter the "Master Development Plan" or "MDP"). Where more detailed criteria for City required submittals exceed the criteria required for a Master Development Plan, the more detailed criteria apply.

NOW THEREFORE, in consideration of the mutual covenants and agreements contained herein, and other good and valuable considerations, the receipt and sufficiency of which is hereby acknowledged, the parties hereto agree as follows:

1. **Recitals and Definitions.** The recitals herein contained are true and correct and are incorporated herein by reference. All capitalized terms not otherwise defined herein shall be as defined or described in the City's Land Development Code as it may be amended from time to time, unless otherwise indicated.
2. **Ownership.** The legal and equitable owners of the Subject Properties is: New Hope Church of Deltona, Inc.
3. **Title Opinion/Certification.** The Developer will provide to the City, in advance of the City's execution and recordation of this Agreement, a title opinion from a licensed attorney in the state of Florida, or a certification by an abstractor or title company authorized to do business in the state of Florida, verifying marketable title to the Subject Properties to be in the name of the Owner and any and all liens, mortgages, and other encumbrances that are either satisfied or not satisfied or released of record.
4. **Subordination/Joinder.** Unless otherwise agreed to by the City and if applicable, all liens, mortgages, and other encumbrances that are not satisfied or released of record, must be subordinated to the terms of this Agreement or the lienholder may join in this Agreement. It shall be the responsibility of the

Developer to promptly obtain said subordination or joinder, in form and substance that is acceptable to the City Attorney, prior to the execution and recordation of this Agreement.

5. **Duration.** The duration of this Agreement is binding and runs with the land in perpetuity, unless amended or terminated earlier pursuant to the provisions of this Agreement. If a Final Site Plan for either phase/lot, a building permit for vertical construction of either phase/lot, or a plat has not been approved within two (2) years from the rezone approval by the City it shall have the effect of automatically voiding the development and the land shall revert to the same zoning classification which existed immediately preceding the approval of the Planned Unit Development (PUD). A PUD may receive one (1) extension issued by the Director or designee of Planning and Development Services, for good cause that is valid for three (3) years. Good cause may include factors such as market conditions, financing delays, infrastructure or utility coordination, or other circumstances beyond the applicant's control. Upon expiration of the extension, and if no vertical construction or plat has been approved as stated above, the PUD shall be null and void.
6. **Development of the Subject Properties.** Development of the Subject Properties shall be subject to performance standards listed in this Agreement. Where a land use listed below differs from a defined use in the City of Deltona's Code of Ordinances, the use listed in this Agreement shall prevail.
 - A. The New Hope Mixed-Use Planned Unit Development is consistent with the Comprehensive Plan, specific to these Subject Properties.
 - B. Permitted principal uses allowable on the Subject Properties:
 1. Residential – Multi-family residential dwellings not to exceed 96 units collectively used for affordable housing as defined by the U.S. Department of Housing and Urban Development (HUD).
 2. Houses of worship.
 3. School, parochial or private.
 4. Daycare.
 5. Meeting space/rooms.
 6. Parks or recreation areas publicly or privately owned.
 - C. Permitted accessory uses allowable on the Subject Properties:
 1. Garages (residential accessory only).
 2. Private active and passive recreational facilities.

3. Dumpsters, trash compactors, mail kiosks, maintenance buildings, and other similar uses.
4. Clubhouse and associated amenities.
5. Rental Office.
6. Home occupations, per LDC Section 110-807, as it is amended from time to time.

D. Prohibited principal uses, if any:

1. Mobile/manufactured homes defined by the United States Department of Housing and Urban Development
2. Any use not listed as a permitted use.

E. Development Standards for Overall PUD

- | | |
|-------------------------------------|-----------------------|
| 1. Minimum Open Space: | 25% common open space |
| 2. Maximum Impervious Surface Area: | 60% |
| 3. Minimum lot size: | 1 acre |
| 4. Minimum lot width: | 300 feet |

F. Development Standards for Residential Area

1. Proposed maximum density: 15 units per acre.
2. Maximum lot coverage: 30%
3. No single multi-family building shall exceed 48 units.
4. Minimum landscaping requirements shall be per the City's Land Development Code (LDC) Section 110-808, utilizing the multifamily standards.
5. Landscape Buffers: a minimum 25-foot landscape buffer shall be provided along Lake Helen Osteen Road; a minimum 20-foot landscape buffer shall be provided along all other perimeter property lines where a required wetland buffer is not otherwise located, except that a limited encroachment of the parking lot into the northern boundary of the required landscape buffer shall be permitted southwest of the existing church, as depicted on the MDP attached hereto. No landscape buffers will be required between residential and church or school use areas that are located internal to the overall Property.

Note: Stormwater management facilities shall not be located within designated buffer yards.

6. Wetland buffer: A minimum 25-foot upland buffer is required adjacent to any wetlands on the property, per the City's LDC Section 98-53.
7. Maximum building height and length:
 - Maximum height: 3 stories, not to exceed 45 feet.
 - Maximum length: No buildings shall exceed 170 feet.
8. Minimum floor area per dwelling unit:
 1. Studio, efficiency, one-bedroom: 651 square feet
 2. Two-bedroom: 870 square feet
 3. Three-bedroom: 1,041 square feet
9. Building setbacks:
 1. Front yard: 35 ft.
 2. Side yard (north and south): 25 feet
 3. Rear yard: 50 feet
10. Perimeter Setbacks: Perimeter setbacks apply only along the exterior property lines of the Planned Unit Development (PUD). All principal and accessory structure shall comply with the perimeter setbacks listed in this Agreement for the applicable development area.
11. Building Separation and Interior Setbacks: A minimum 25-foot building separation shall be required between any two principal buildings within the interior of the PUD. This standard serves as the interior setback requirement for the project.
 1. The 25-foot building separation is not cumulative with perimeter property line setbacks.
 2. Only one 25-foot distance is required between principal buildings.
 3. This requirement does not apply to accessory structures unless otherwise required by the City's Land Development Code.
12. Minimum parking standards are per Sections. 110-828 and 110-829 of the City's Land Development Code, as it is amended from time to time. In the event shared parking is proposed between the residential

and church portions of the Property, a parking study shall be provided during final site plan review to support an requested modification. In addition, designated visitor spaces or overflow parking shall be generally provided as depicted on the MDP based upon the multi-family standards in Section 110-828 of the City's Land Development Code. Parking maintenance, including striping shall be the responsibility of the Owner/Developer, or an entity designated by the Owner/Developer. Landscaping, design, and other elements of the overflow parking shall be addressed during the site plan review process consistent with the Land Development Code. Finally, no unpaved area shall be used to park, store or otherwise accommodate any vehicle, car, truck, trailer, boat, recreational vehicle or other equipment. No boat, unregistered vehicle, trailer, recreational vehicle or other shall be parked/stored in a driveway or any parking place.

G. Development Standards for Church/School Area:

1. Maximum FAR: 0.30
2. Maximum lot coverage: 30%.
3. Minimum landscaping requirements shall be per the City's Land Development Code.
4. Landscape Buffers: a minimum 25-foot landscape buffer shall be provided along Lake Helen Osteen Road; a minimum 20-foot landscape buffer shall be provided along all other perimeter property lines. No landscape buffers will be required between residential and church or school use areas that are located internal to the overall Property.
5. Maximum building height and length:
 1. Maximum height: 35 feet
 2. Maximum length: 260 feet
6. Building setbacks:
 1. Front yard: 90 feet
 2. Side yard (north and south): 15 feet
 3. Rear yard: 25 feet
7. Perimeter Setbacks: All principal and accessory structures shall meet or exceed a 20-foot setback from the perimeter property line.

8. Interior Setbacks: All principal and accessory structures shall meet or exceed a 10-foot setback from any interior street, drive, or off-street parking area.
9. Minimum building separation distance: Principal structures shall be located at least 25 feet from one another, subject to the interior setback requirements provided above.

H. **Lighting Standards.** Minimum lighting standards for the Subject Property shall comply with the applicable provisions of the City's Land Development Code. A separate Illumination Plan shall be submitted as part of the Final Site Plan application.

1. Streetlights shall be incorporated throughout the development to enhance appeal and safety.
2. Under no circumstances shall any Owner, Developer, residents, or other entity remove, disable or otherwise cause streetlights to become inoperable.
3. Streetlight maintenance shall be the responsibility of the Owner or designated Property Owner's Association.

Light Pole Height Standards and Exceptions:

4. Standard Light Pole Height. The maximum height for light poles throughout the project shall be 35 feet, consistent with the City's Land Development Code.
- I. Architectural controls and development on the Subject Properties shall follow a common architectural theme as listed in this Agreement by harmoniously coordinating the general appearance of all buildings and accessory structures.
1. Exterior walls shall be constructed of finished materials such as stucco, natural brick or stone, finished concrete, wood or concrete fiberboard or other similar materials on all sides.
 2. Ground level utility boxes, air conditioning condensers, pool pumps and similar mechanical apparatuses shall be screened from the public rights-of-way by architectural screening consistent with the structure or landscaping of sufficient density and maturity at planting to provide opaque screening. Waste dumpsters servicing the community shall be enclosed within a gated enclosure, the exterior of which shall be consistent with the architecture of the project.
 3. **Temporary/Permanent Signage** – All signs shall be consistent with Chapter 102 of the City's Land Development Code, as it may be

amended from time to time. The entrances to New Hope PUD are planned to be at Lake Helen Osteen Road, as depicted on the Master Development Plan. Subdivision entrance signs may be erected at each entrance generally in the locations shown on the MDP. The entrance signs shall be free-standing monument signs of no more than six-feet in height with an 18-inch base. The copy area shall feature no more than 75 square feet per side and will be maintained by a Property Owners' Association (POA). The easement to maintain the sign will be deeded in favor of the Property Owner/ POA. The signs shall not contain any electronic messaging. Foundation landscaping will be a required element of the signs. The entrance signs shall be permitted separately and must be approved by the Director of Community Development or designee. An elevation of the sign, including color renditions, landscaping and other design elements shall be part of the Final Site Plan and/or plat submittal to the Development Review Committee (DRC).

4. **Centralized Mail Delivery:** A centralized mail kiosk will be provided as shown on the MDP or as otherwise located during Final Site Plan and/or subdivision review and approval by the City. These facilities will include parking and will be maintained by the POA in accordance with the USPS requirements as applicable.
 5. **Architectural Elevation Submissions.** Architectural elevation drawings shall be required as part of all Preliminary Plat, Plat, and/or Final Site Plan applications, and must demonstrate adherence to the unified architectural theme and shall comply with the requirements of Chapter 111 of the City's Land Development Code, as may be amended from time to time.
- J. **Utility provision and dedication:** The Developer shall connect to the City of Deltona's central utility systems, when available, or to Volusia County's central utility systems, where applicable, at their sole cost and expense. Utility fees shall be paid to Deltona Water or Volusia County, respectively, before any building permit is issued. Central utility systems are to be designed, permitted, and constructed to the respective service provider specifications and dedicated to the respective service provider upon final inspection, clearance, and acceptance by the service provider.
- K. **Waste Disposal:** One (1) standard compactor shall be provided to service the development. Individual solid waste disposal pads and collection points shall be provided for every 60 residential units. The compactor shall be screened in accordance with Sec. 110-808(j) of the City Land Development

Code. All other collection points shall be strategically located within fully enclosed garage type structures. An acceptable design shall be reviewed and approved at the time of Final Site Plan. Any trash collection activities within the MPUD shall comply with the exclusive waste disposal franchise granted to Waste Pro, or any subsequent hauler as may be designated by the City in the future. No trash compactor or collection point shall be at the perimeter of the property adjacent to adjoining single-family neighbors.

- L. **Stormwater and environmental:** Per parcel stormwater systems or master stormwater systems shall be owned and maintained by an established Property Owners Association in private ownership and shall not be dedicated to or become the responsibility of the City of Deltona. All environmental permitting, mitigation, and/or soil and erosion control for the properties shall conform to all federal, state, and local permits/requirements, shall be the sole responsibility of the Property Owners Association, and shall be maintained in good condition/standing with the applicable permitting authorities. Best Management Practices and conformance to National Pollutant Discharge Elimination System (NPDES) criteria are required. The lift stations shall be elevated, equipped with a generator, and have sufficient space for fuel storage.
- M. **Transportation, site access, and traffic devices:** The Developer is responsible for all transportation improvements within the Subject Properties and any off-site transportation requirements, as a result of the proposed development, for site function, that maintains or improves the level of service for area roadways, and ensures the public health, safety, and welfare for the community as determined by the Traffic Impact Analysis and required by the Land Development Code. All permits shall be obtained from appropriate permitting agencies prior to development, and the City shall determine the appropriate level of service per the City Comprehensive Plan and current traffic counts.
- N. **Development Phases:** The Subject Properties may be developed in one (1) or more phases. If the MPUD is developed in phases a Preliminary Plat will be required. If the project is developed in phases a separate Final Site Plan for review and approval shall be consistent with this Agreement. The Final Site Plan for the phases of construction shall allow the applicant to provide for flexibility for providing amendments to the plan that may be done without the necessity of requiring a separate site plan application and review, providing the following are provided:
 - 1. Evidence that such amendment does not cause an increase in stormwater retention, and

2. The said amendments are consistent with the limitations and requirements provided by this Developer Agreement. During any construction phasing, Developer shall be required to maintain the undeveloped portions of the property so as not to cause any harm to any surrounding properties. Land clearing and grading for all construction phases shall be permitted in the first construction phase provided all tree preservation areas, if any, are maintained.
 3. If the development occurs in phases, enhanced landscaping and an open public space shall be provided and maintained on the undeveloped lot until the second phase begins. Enhanced landscaping refers to site design that goes above and beyond the minimum standard landscaping code requirements.
7. **Public Facilities/Land Dedication.** Facilities or tracts that either are or shall become public facilities/tracts that will serve the development and/or are on the Subject Properties will be determined at platting.
8. **Development Permits/Fees.** The Developer is responsible for obtaining, permitting, and the payment of all fees for facilities and services for the Subject Properties. Any site permits shall be kept current with the respective permitting agency and shall ensure the protection of the public health, safety, and welfare of the community and the development. All impact fees are applicable, and no impact fee credits shall be awarded through this Agreement; unless a cessation exists through a City moratorium that is Citywide. Proportionate fair share site improvements shall not be used in lieu of impact fees.
9. **Obligations.** Should the Developer fail to undertake and complete its obligations as described in this Agreement to the City's specifications, then the City shall give the Developer 30 days written notice to commence and 90 days to complete said required obligation. If the Developer fails to complete the obligations within the 90-day period, then the City, without further notice to the Developer, or its successors in interest, may, without prejudice to any other rights or remedies it may have, place liens and take enforcement action on the Subject Properties. A lien of such assessments shall be superior to all others, and all existing lienholders and mortgagees, by their execution of the subordination or joinder documents, agree to subordinate their liens or mortgages to the City's said liens or assessments. Notice to the Developer and its successors in interest shall be deemed to have been given upon the mailing of notice to the address or addresses set forth in Paragraph (20) hereof.

10. **Site Plan/Plat Approval. Exhibit “C”**, the Master Development Plan, is the Preliminary Plan of the PUD and this Agreement. The Master Development Plan shall not replace, supersede, or absolve the Developer from approvals for any Final Site Plan, Preliminary Plat, and/or Final Plat and their respective regulations. Where more detailed criteria for City required submittals exceed the criteria required for a Master Development Plan, the more detailed criteria apply.
11. **Indemnification.** The Developer shall indemnify, defend, and hold the City harmless from any and against all claims, demands, disputes, damages, costs, expenses, (to include attorneys' fees whether or not litigation is necessary and if necessary, both at trial and on appeal), incurred by the City as a result, directly or indirectly, of the use or development of the Subject Properties, except those claims or liabilities caused by or arising from the negligence or intentional acts of the City, or its employees or agents. It is specifically understood that the City is not guaranteeing the appropriateness, efficiency, quality or legality of the use or development of the Subject Properties, including but not limited to, drainage or water/sewer plans, fire safety, or quality of construction, whether or not inspected, approved, or permitted by the City.
12. **Compliance.** The Owner and Developer agree that they, and their successors and assigns, will abide by the provisions of this Agreement, the City's Comprehensive Plan and the City's Code of Ordinances, including but not limited to, the site plan regulations of the City as amended from time to time, which are incorporated herein by reference and such subsequent amendments hereto as may be applicable. Further, all required improvements, including landscaping, shall be continuously maintained by the Owner/Developer or Developer, or their successors and assigns, in accordance with the City's Code of Ordinances. The City may, without prejudice to any other legal or equitable right or remedy it may have, withhold permits, Certificates of Occupancy or site plan/plat approvals to the Subject Properties, should the Owner/Developer fail to comply with the terms of this Agreement. In the event of a conflict between this Development Agreement and the City's Land Development Code, the more restrictive regulations shall govern the development of the Subject Properties.
13. **Obligations for Improvements.** Any surface improvement as described and required hereunder included, but not limited to such as signalization, walls, stormwater management facilities, medians, and utilities, or any other surface improvement shall be performed, prior to the issuance of the first Certificate of Occupancy on that portion of the Subject Properties that the surface improvement(s) relates or is otherwise scheduled in this Agreement. Should the Developer fail to undertake and complete its obligations as described in this

Agreement and to the City's specifications, then the City shall give the Developer 30 days written notice to commence and 90 days to complete said required obligation at the sole expense of the Developer. If the Developer fails to complete the obligations within the 90 day period, then the City, without further notice to the Developer and their successors and assigns in interest, may but shall not be required to, perform such obligations at the expense of the Developer or their successors and assigns in interest, without prejudice to any other rights or remedies the City may have under this Agreement. Further, the City is hereby authorized to immediately recover the actual and verified cost of completing the obligations required under this Agreement and any legal fees from the Developer in an action at law for damages, as well as record a lien against the Subject Properties in that amount. The lien of such assessments shall be superior to all others, and all existing lienholders and mortgagees, by their execution of the subordination or joinder documents, agree to subordinate their liens or mortgages to the City's said liens or assessments. Notice to the Developer and their successors and assigns in interest shall be deemed to have been given upon the mailing of notice as provided in paragraph (24) of this Agreement.

14. **Concurrency and Vested Rights.** The Developer acknowledges and agrees that prior to the issuance of any development orders for the Properties, the Developer must have received and be in possession of a valid unexpired certificate of capacity/concurrency management system approval consistent with the City's Land Development Code. The capacity certificate/approval verifies the availability of infrastructure and service capacity sufficient to permit the proposed development of the Subject Properties without causing a reduction in the levels of service adopted in the City's Comprehensive Plan. The certificate of capacity/approval shall be effective for a term, as defined in the City's Code of Ordinances. Neither this Agreement nor the approved Master Development Plan shall create or result in a vested right or rights to develop the Subject Properties, as cited in Section 86-34 of the City's Land Development Code.
15. **Environmental and Tree Preservation.** The Developer is responsible for obtaining all site related permits and approval prior to any development activity on or for the Subject Properties. This may involve mitigation for habitat of threatened or endangered flora and fauna or for species identified for proportion (i.e. tree preservation). This Agreement does not vest or exempt the Developer from any permitting and mitigation obligations needed to develop a Subject Properties. In addition, tree replacement and/or wetland mitigation fees, as applicable, shall be paid in full prior to issuance of building permits. If the property contains gopher tortoise habitats, then the site will need to be

surveyed and, if deemed necessary, tortoises relocated. Any relocation of tortoises needs to be consistent with applicable permitting agencies. A minimum of 25' of upland buffer shall be maintained adjacent to all wetland areas.

16. **Homeowners Association or Property Owners Association.** The charter and by-laws of Property Owners Association ("POA") for the Subject Properties and any deed restrictions related thereto shall be furnished to the City for approval by the City Attorney prior to the recording thereof in the Public Records of Volusia County, Florida. Such recording shall take place before a Certificate of Occupancy is issued for the first development project on land covered by this Agreement. The POA shall at a minimum be responsible for maintaining the common open space, any common utility systems, such as for irrigation and site lighting, and project signage. The Developer shall be responsible for establishing the POA and recording said information in the Public Records of Volusia County, Florida. The City is not responsible for the enforcement of any agreements or deed restrictions entered into between property owners or occupiers of the Subject Properties. If maintenance for the Subject Properties is not maintained following issuance of a Certificate of Occupancy, the City has Code Enforcement services.
17. **Enforcement.** Both parties may seek specific performance of this Agreement and/or bring an action for damages in a court within Volusia County, Florida, if this Agreement is breached by either party. In the event that enforcement of this Agreement by the City becomes necessary, and the City is successful in such enforcement, the Developer shall be responsible for the payment of all of the City's costs and expenses, including attorney fees, whether or not litigation is necessary and, if necessary, both at trial and on appeal. Such costs, expenses and fees shall also be a lien upon the Subject Properties superior to all others. Should this Agreement require the payment of any monies to the City, the recording of this Agreement shall constitute a lien upon the Subject Properties for said monies, until said are paid, in addition to such other obligations as this Agreement may impose upon the Subject Properties and the Developer. Interest on unpaid overdue sums shall accrue at the rate of the lesser of eighteen percent (18%) compounded annually or at the maximum rate allowed by law.
18. **Utility Easements.** For any easement not established on a plat for the Subject Properties, the Developer shall provide to the City such easements and other legal documentation, in form mutually acceptable to the City Attorney and the Developer, as the City may deem reasonably necessary or appropriate for the installation and maintenance of the utility and other services, including but not

limited to, sanitary sewer, potable water, and reclaimed water services, electric, cable, gas, fire protection and telecommunications.

19. **Periodic Review.** The City reserves the right to review the Subject Properties subject in relation to this Agreement periodically to determine if there has been demonstrated good faith compliance with the terms of this Agreement. If the City finds that on the basis of substantial competent evidence that there has been a failure to comply with the terms of this Agreement, the City may not issue development orders or permits until compliance with this Agreement has been established.
20. **Notices.** Where notice is herein required to be given, it shall be by certified mail return receipt requested, hand delivery or nationally recognized courier, such as Federal Express or UPS. E-mail delivery of documents shall not replace or be in lieu of the aforementioned process. Said notice shall be sent to the following, as applicable:

DEVELOPER'S REPRESENTATIVES:

DEVELOPER

Tacolcy Economic Development Corp., Inc.
Attn: Carol Gardner
5900 NW 7th Ave., Suite 102
Miami, FL 33127

With copy to:

Mark A. Watts, Esq.
Cobb Cole
231 N. Woodland Blvd.
DeLand, FL 32720

CITY'S REPRESENTATIVES:

City Manager
City of Deltona
2345 Providence Boulevard
Deltona, Florida 32725

With copy to:

Planning & Development Services
City of Deltona
2345 Providence Boulevard
Deltona, Florida 32725

Should any party identified above change, it shall be said party's obligation to notify the remaining parties of the change in a fashion as is required for notices herein. It shall be the Owner/Developer's or Developer obligation to identify its lender(s) to all parties in a fashion as is required for notices herein.

21. **Compliance with the Law.** The failure of this Agreement to address a particular permit, condition, term, or restriction shall not relieve the Developer of the Subject Properties from the necessity of complying with the law governing said permitting requirements, conditions, terms, or restrictions.
22. **Captions.** The captions used herein are for convenience only and shall not be relied upon in construing this Agreement.

23. **Binding Effect.** This Agreement shall run with the land, shall be binding upon and inure to the benefit of the Developer and their successors and assigns in interest, and the City and their successor and assigns in interest. This Agreement shall become effective upon its execution and recordation with the Public Records of Volusia County, Florida. This Agreement does not, and is not intended to, prevent or impede the City from exercising its legislative authority as the same may affect the Subject Properties.
24. **Subsequently Enacted State or Federal Law.** If either state or federal law is enacted after the effective date of this Agreement that is applicable to and precludes the parties' compliance with the terms of this Agreement, this Agreement and correlating zoning amendment shall be modified or revoked, as is necessary, to comply with the relevant state or federal law.
25. **Severability.** If any part of this Development Agreement is found invalid or unenforceable in any court, such invalidity or unenforceability shall not affect the other parts of this Development Agreement, if the rights and obligations of the parties contained herein are not materially prejudiced and if the intentions of the parties can be affected. To that end, this Development Agreement is declared severable.
26. **Covenant Running with the Land.** This Agreement shall run with the Subject Properties and inure to and be for the benefit of the parties hereto and their respective successors and assigns and any person, firm, corporation, or entity who may become the successor in interest to the Subject Properties or any portion thereof.
27. **Recordation of Agreement.** The parties hereto agree that an executed original of this Agreement shall be recorded by the City, at the Developer's expense, in the Public Records of Volusia County, Florida.
28. **Applicable Law/Venue.** This Agreement and the provisions contained herein shall be construed, controlled, and interpreted according to the laws of the State of Florida. Venue of any litigation relating to this Agreement shall be in the courts of Volusia County, Florida.
29. **Time of the Essence.** Time is hereby declared of the essence to the lawful performance of the duties and obligations contained in this Agreement. The Owner/Developer shall execute this Agreement within 30 business days of City Commission adoption of Ordinance No. 01-2026; and agrees to pay the cost of recording this document in the Public Records of Volusia County, Florida. Failure to execute this Agreement within 30 business days of this Ordinance adoption may result in the City not issuing development orders or permits until execution and recordation of this Agreement has occurred.

30. **Agreement; Amendment.** This Agreement constitutes the entire agreement between the parties, and supersedes all previous discussions, understandings and agreements, with respect to the subject matter hereof; provided, however, that it is agreed that this Agreement is supplemental to the City's Comprehensive Plan and does not in any way rescind or modify any provisions of the City's Comprehensive Plan. Amendments to and waivers of the provisions of this Agreement shall be made by the parties only in writing by formal amendment.
31. **Effective Date.** The Effective Date of this Agreement shall be the day this Agreement is recorded in the Public Records of Volusia County, Florida.

[Remainder of the page intentionally left blank]

IN WITNESS WHEREOF, the Owner, the Developer and the City have executed this Agreement.

**NEW HOPE BAPTIST CHURCH OF
DELTONA, INC. (Owner)**

By:

Signature of Witness # 1

Signature

Print or type name

Print or type name

AS:

Signature of Witness # 1

Signature

Print or type name

Print or type name

As:

Mailing Address:

STATE OF FLORIDA

COUNTY OF _____

The foregoing instrument was acknowledged before me by means of ☐ physical presence or ☐ online notarization, this _____ day of _____, 2026, by _____, and _____, of _____, who is/are personally known to me or who has/have produced _____ as identification and who did not (did) take an oath.

(NOTARY SEAL)

Signature of Notary

Print or type name

**TACOLCY ECONOMIC
DEVELOPMENT CORPORATION, INC.
(Developer)**

By:

Signature of Witness # 1

Signature

Print or type name

Print or type name

AS:

Signature of Witness # 1

Signature

Print or type name

Print or type name

As:

Mailing Address:

**STATE OF FLORIDA
COUNTY OF _____**

The foregoing instrument was acknowledged before me by means of ☐ physical presence
or ☐ online notarization, this _____ day of _____, 2026, by
_____, and _____, of
_____, who is/are personally known to me or who has/have produced
_____ as identification and who did not (did) take
an oath.

(NOTARY SEAL)

Signature of Notary

Print or type name

CITY OF DELTONA:

By: _____

Date: _____

ATTEST:

Date: _____

Mailing Address:

City of Deltona
2345 Providence Boulevard
Deltona, Florida 32725

STATE OF FLORIDA

COUNTY OF _____

The foregoing instrument was acknowledged before me by means of ☐ physical presence or ☐ online notarization, this ____ day of _____, 202__, by _____, and _____, who are personally known to me and acknowledge executing the same freely and voluntarily under authority vested in them by the City of Deltona.

Signature of Notary

(NOTARY SEAL)

Print or type name

Approved as to form and legality for use and
reliance by the City of Deltona, Florida

Gemma Torcivia
City Attorney

EXHIBIT "B"
LEGAL DESCRIPTION

DESCRIPTION PER ORB 4041 PG. 402

THE SOUTH 264 FEET OF THE NORTH 792 FEET OF THE SOUTHWEST $\frac{1}{4}$ OF THE NORTHEAST $\frac{1}{4}$, EAST OF ROAD, SECTION 10, TOWNSHIP 18 SOUTH, RANGE 31 EAST, VOLUSIA COUNTY, FLORIDA.

AND

DESCRIPTION: PER OR 6785 PG 1227

The South 264 feet of the North 792 feet of the Southwest $\frac{1}{4}$ of the Northeast $\frac{1}{4}$ West of Road, Section 10, Township 18 South, Range 31 East, Volusia County, Florida.

AND

DESCRIPTION: PER OR 7585 PG 4982

The South 528 feet of the Southwest $\frac{1}{4}$ of the Northeast $\frac{1}{4}$, except the South 68 feet of the West 180 feet thereof; and the North 132 feet of the Southeast $\frac{1}{4}$, except the North 32 feet of the West 180 feet thereof, Section 10, Township 18 South, Range 31 East, lying West of Lake Helen-Osteen Road.

EXCEPT the following described property:

That portion of the South 105 feet of the Southwest $\frac{1}{4}$ of the Northeast $\frac{1}{4}$ of Section 10, Township 18 South, Range 31 East; Volusia County, Florida; lying West of "Lake Helen-Osteen Road", except the West 180 feet thereof.

AND EXCEPT that portion of the North 132 feet of the Southeast $\frac{1}{4}$ of Section 10, Township 18 South, Range 31 East, Volusia County, Florida, lying West of "Lake Helen-Osteen Road", except the North 32 feet of the West 180 feet thereof.

Containing approximately 14.43 total acres.

Exhibit B

LEGAL DESCRIPTION NEW HOPE PUD

DESCRIPTION PER ORB 4041 PG. 402

THE SOUTH 264 FEET OF THE NORTH 792 FEET OF THE SOUTHWEST $\frac{1}{4}$ OF THE NORTHEAST $\frac{1}{4}$, EAST OF ROAD, SECTION 10, TOWNSHIP 18 SOUTH, RANGE 31 EAST, VOLUSIA COUNTY, FLORIDA.

AND

DESCRIPTION: PER OR 6785 PG 1227

The South 264 feet of the North 792 feet of the Southwest $\frac{1}{4}$ of the Northeast $\frac{1}{4}$ West of Road, Section 10, Township 18 South, Range 31 East, Volusia County, Florida.

AND

DESCRIPTION: PER OR 7585 PG 4982

The South 528 feet of the Southwest $\frac{1}{4}$ of the Northeast $\frac{1}{4}$, except the South 68 feet of the West 180 feet thereof; and the North 132 feet of the Southeast $\frac{1}{4}$, except the North 32 feet of the West 180 feet thereof, Section 10, Township 18 South, Range 31 East, lying West of Lake Helen-Osteen Road.

EXCEPT the following described property:

That portion of the South 105 feet of the Southwest $\frac{1}{4}$ of the Northeast $\frac{1}{4}$ of Section 10, Township 18 South, Range 31 East; Volusia County, Florida; lying West of "Lake Helen-Osteen Road", except the West 180 feet thereof.

AND EXCEPT that portion of the North 132 feet of the Southeast $\frac{1}{4}$ of Section 10, Township 18 South, Range 31 East, Volusia County, Florida, lying West of "Lake Helen-Osteen Road", except the North 32 feet of the West 180 feet thereof.

Containing approximately 14.43 total acres.

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EXHIBIT C

PROJECT LOCATION



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4955 SW 75TH Avenue
Miami, Florida 33155
T 786.879.8882
F 786.350.0151
www.modisarchitects.com

New Hope Church & Residence

04/29/2025

Deltona, FLORIDA

Zoning & Project Data

| Residential Data | | | | |
|----------------------|---------------|------------|-------------|----------|
| Description | | Required | Proposed | |
| Lot | | | | |
| Parcel ID | | | | |
| 8111000000080 | 83,199.60 sf | 1.91 Acres | | |
| 8110000000041 | 196,020.00 sf | 4.50 Acres | | |
| Lot Area Summary | | | | |
| Gross Lot Area: | 279,220 sf | 6.41 Acres | | |
| Zoning District | | | | |
| Proposed Residential | 279,220 sf | | | PUD |
| Density | 6.41 Acres | | | |
| Density | 6.41 Acres | | 77 Units | 96 Units |
| Building Height | | | 12.00 DU/AC | 0 |
| Building Height | | | | 40'-0" |
| Building Setbacks | | | | 0 |
| Front Setback (East) | | 25'-0" | | 41'-0" |
| Side Setback (North) | | 25'-0" | | 25'-0" |
| Side Setback (South) | | 25'-0" | | 25'-0" |
| Rear Setback (West) | | 25'-0" | | 56'-0" |

Building Data

| Building Area A | | | |
|-----------------|--|--------------|---------------------|
| | Total Sq Ft. does not include Balcony Sq Ft. | | |
| Levels | Leasable Area | Non-Leasable | Total Bldg Gross SF |
| Level 1 | 6,894 sf | 1,253 sf | 8,147 sf |
| Level 2 | 6,864 sf | 1,094 sf | 7,958 sf |
| Level 3 | 6,864 sf | 1,094 sf | 7,958 sf |
| | | | |
| Total | 20,592 sf | 3,441 sf | 24,033 sf |
| | | | 96,132 sf |

Unit Data

[illegible]

Parking Data

| Residential Parking Requirement | | | | | |
|---------------------------------|----------|-----------|---------------|------------|------------|
| | | | | Required | Provided |
| Unit A (1 BD) | 24 Units | 25.00% | 1.5 SP/UD | 36 spaces | |
| Unit B (2 BD) | 48 Units | 50.00% | 2.0 SP/UD | 96 spaces | |
| Unit C (3 BD) | 24 Units | 25.00% | 2.0 SP/UD | 48 spaces | |
| Total Units | 96 Units | 100.00% | 1 sp/10 units | 10 spaces | |
| Visitors | | | | | |
| | | | | | |
| | | Sub Total | | 190 spaces | |
| | | | | | |
| Parking Provided | | | | | |
| | Standard | HC | Parallel | | |
| | 206 | 7 | | | |
| Surface | | | | | |
| | | | | 190 spaces | 213 spaces |

New Hope Church & Residence

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Miami, Florida 33155
T. 786.879.8882
F. 786.350.1515

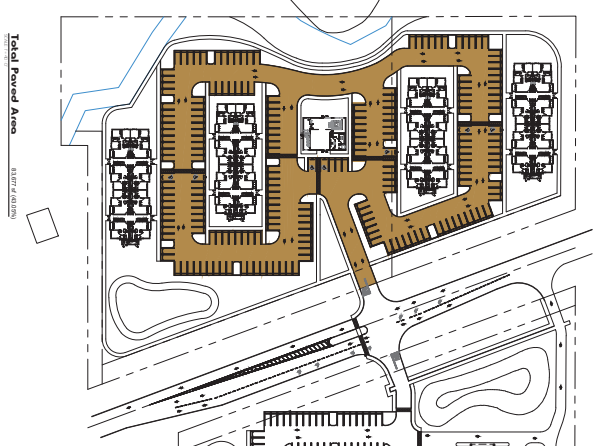
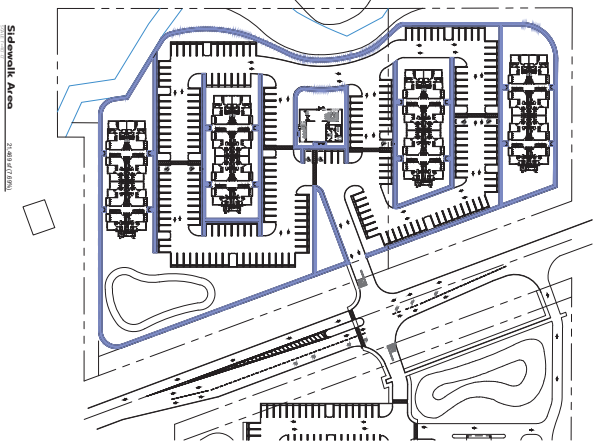
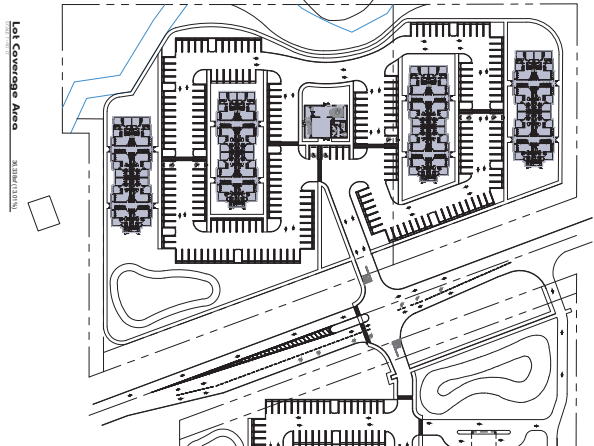
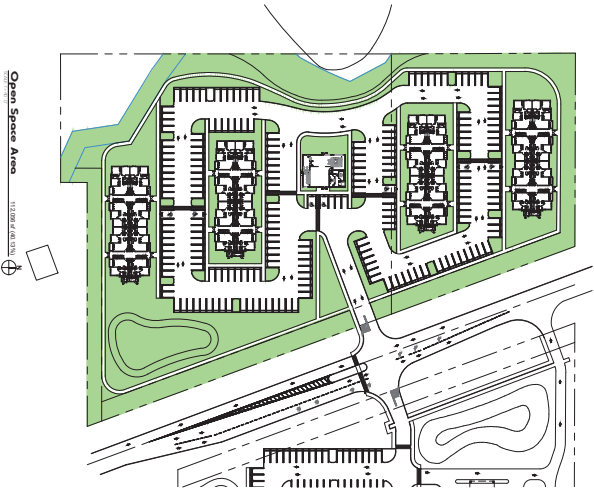
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CONCEPTUAL DESIGN

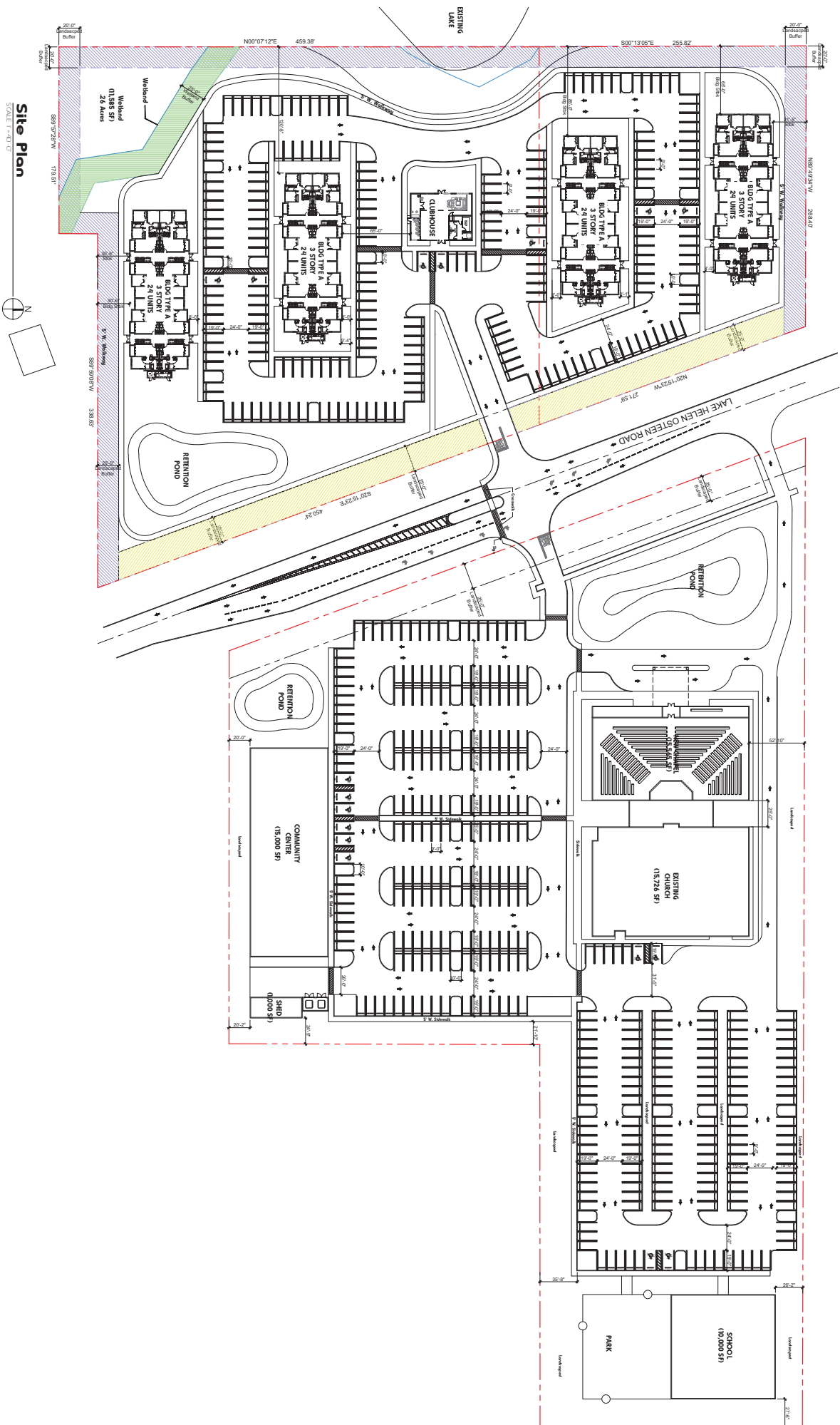
Current Scheme

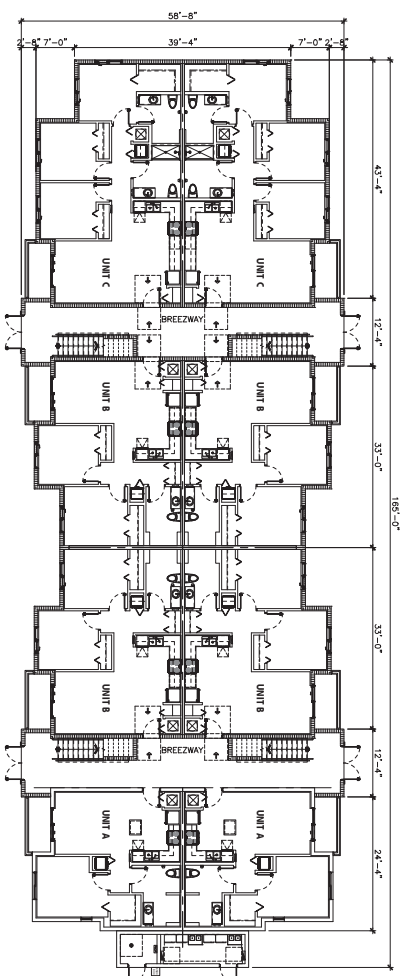
Residential Data Plan

#22043
04/29/2025
SCALE: 1"=40'



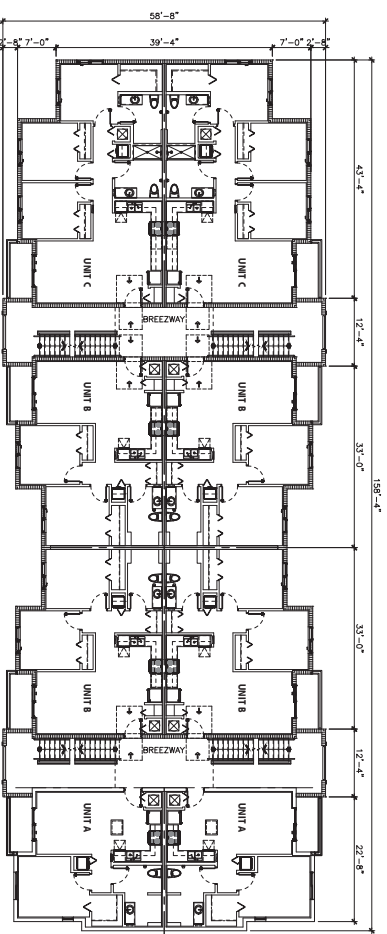
| Description | | Residential Data | | Required | Proposed |
|----------------------|---------------|------------------|--|-----------|------------|
| Lot | | | | | |
| Parcel ID | | | | | |
| 81100000030 | 83,199.60 sf | 1.91 Acres | | | |
| 81100000041 | 196,020.00 sf | 4.50 Acres | | | |
| Lot Area Summary | | | | | |
| Gross Lot Area | 279,220 sf | 6.41 Acres | | | |
| Zoning District | | | | | |
| Proposed Residential | 279,220 sf | | | District | |
| | 6.41 Acres | | | PUD | |
| Density | | | | | |
| Density | 6.41 Acres | 77 Units | | | 96 Units |
| | | 12.00 DU/AC | | | 0 |
| Building Height | | | | | |
| Building Height: | | | | 40'-0" | 0 |
| Building Setbacks | | | | | |
| Front Setback (East) | | 25'-0" | | | 41'-0" |
| Side Setback (North) | | 25'-0" | | | 25'-0" |
| Side Setback (South) | | 25'-0" | | | 25'-0" |
| Rear Setback (West) | | 25'-0" | | | 56'-0" |
| General Requirements | | | | | |
| Flour Area Ratio | | | | | 96,132 sf |
| | | | | | 34.43% |
| Lot Coverage | | | | N/A | 36,338 sf |
| | | | | | 13.01% |
| Landscape Open Space | | | | 69,805 sf | 112,066 sf |
| | | | | 25% | 40.13% |
| Total Paved Area | | | | N/A | 83,677 sf |
| | | | | | 43.05% |
| Sidewalk Area | | | | N/A | 21,489 sf |
| | | | | | 7.69% |





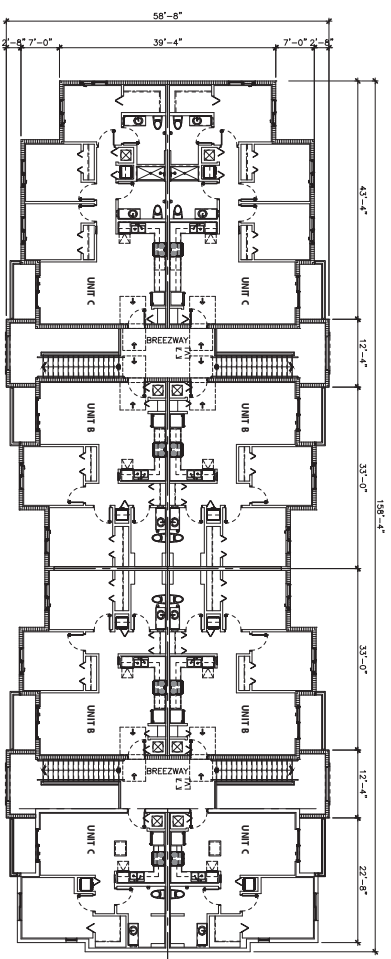
01 Building Type-A - Ground Level

SCALE: 3/32" = 1'-0"



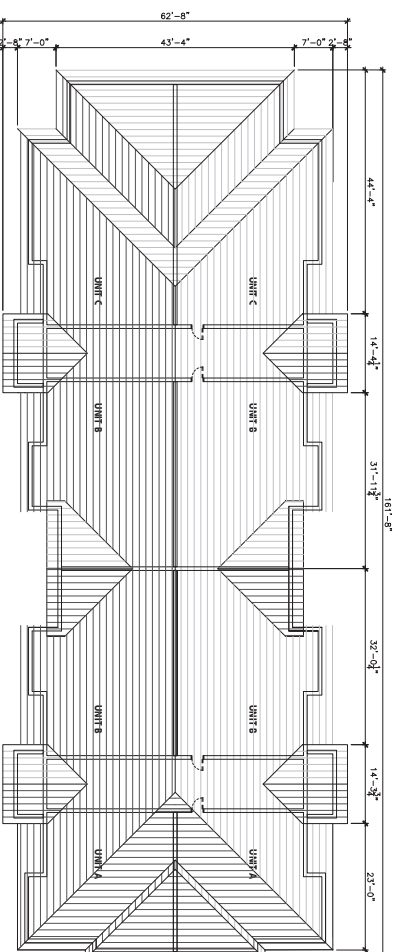
02 Building Type-A - Floor Plan - Level 2

SCALE: 3/32" = 1'-0"



03 Building Type-A -Floor Plan - Level 3

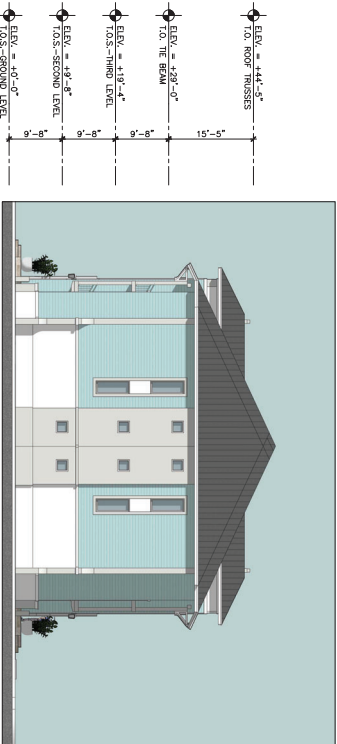
SCALE: 3/32"=1'-0"



04 Building Type-A -Floor Plan - Roof Level

SCALE: 3/32"=1'-0"

Exhibit D





01 Proposed Front Elevation Building Type-8

SCALE: 3/32"=1'-0"



02 Proposed Side Elevation Building Type-8

SCALE: 3/32"=1'-0"

Exhibit E



■ TRAFFIC IMPACT ANALYSIS

NEW HOPE PUD

DELTONA, FLORIDA

MARCH 2024

PREPARED BY:

WALSH TRAFFIC ENGINEERING, LLC

285 PALMETTO SPRINGS STREET

DEBARY, FLORIDA 32713

PHONE – 386.668.0062

TRAFFIC IMPACT ANALYSIS



NEW HOPE PUD

DELTONA, FLORIDA

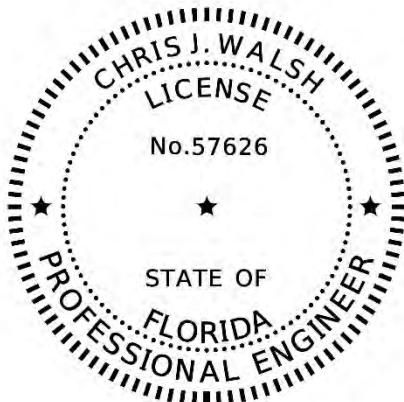
MARCH 2024

PREPARED BY:

CHRIS J. WALSH, P.E.
WALSH TRAFFIC ENGINEERING, LLC
285 PALMETTO SPRINGS STREET
DEBARY, FLORIDA 32713
PHONE – 386.668.0062
PROJECT #: 10068

PREPARED FOR:

TACOLCY ECONOMIC DEVELOPMENT CORPORATION, INC.
5900 NW 7TH AVENUE, SUITE 102
MIAMI, FLORIDA 33127



THIS DOCUMENT HAS BEEN DIGITALLY SIGNED AND SEALED BY:

ON THE DATE ADJACENT TO THE SEAL

PRINTED COPIES OF THIS DOCUMENT ARE NOT CONSIDERED SIGNED AND SEALED AND THE SIGNATURE MUST BE VERIFIED ON ANY ELECTRONIC COPIES

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INTRODUCTION

Walsh Traffic Engineering, LLC (Walsh Traffic) was retained to conduct a traffic impact analysis for the proposed New Hope PUD located on Lake Helen Osteen Road, south of Haulover Boulevard in Deltona, Florida (see **Figure 1**). The subject property straddles both sides of Lake Helen Osteen Road. The property on the west side is vacant. The property on the east side includes a 15,726 square-foot building that serves as a church and can accommodate up to 648 seats. Additionally, this building is used as a daycare facility and is licensed/certified for up to 85 students, operating from 6:30 AM to 6:00 PM with child drop offs/pick-ups occurring continuously throughout the day. The development is proposed to include the following:

West side of Lake Helen Osteen Road

- 120-dwelling unit multi-family development

East side of Lake Helen Osteen Road

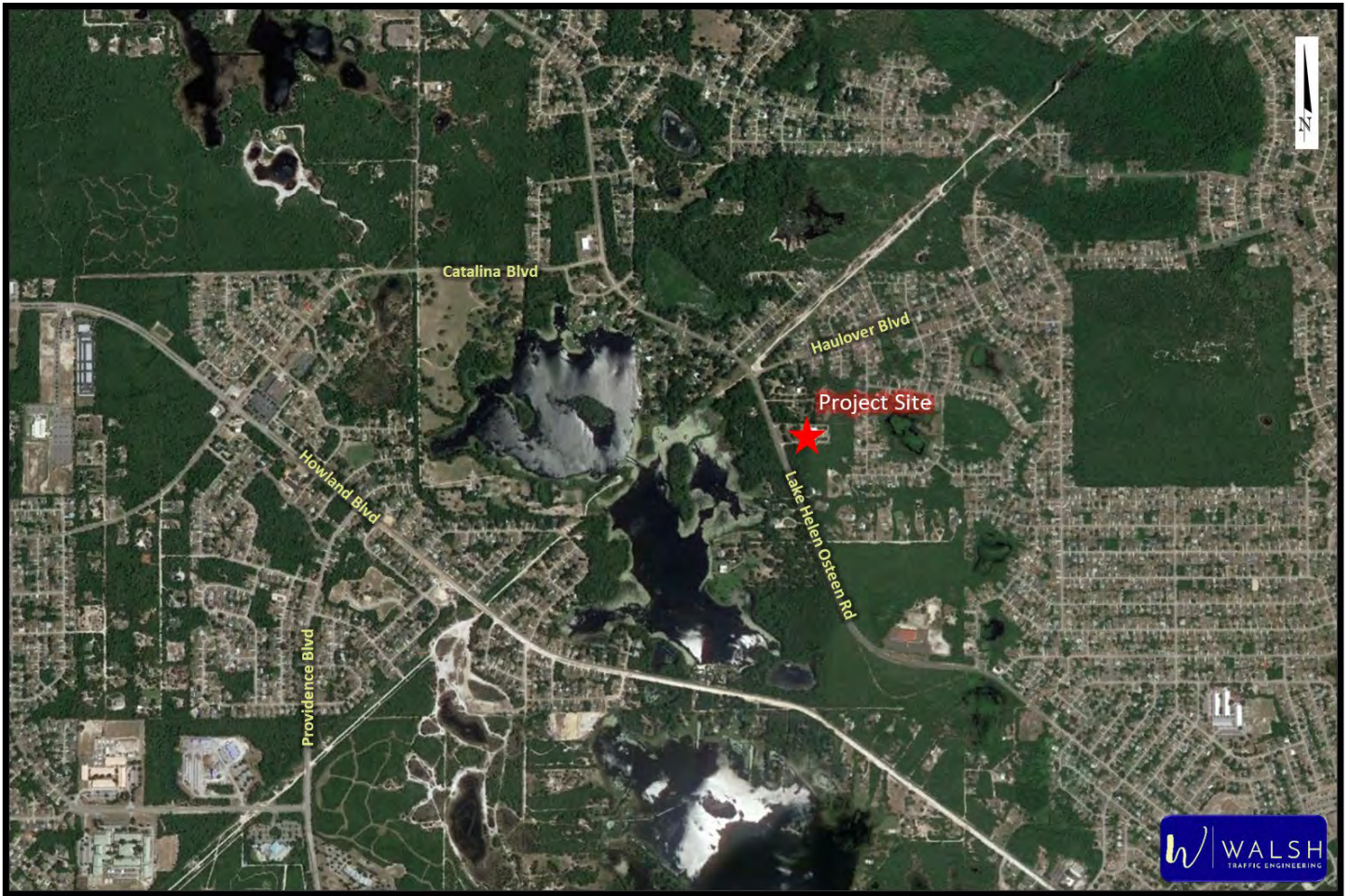
- 10,000 square-foot daycare building for 115 students
- 15,000 square-foot community center building
- 31,291 square-foot church (expansion of the existing church)

A copy of the preliminary development plan is included in **Appendix A**. Additionally, the development is proposed to have a build out date of 2029. This study, which evaluates the overall impact of the development on the adjacent roadway network, was prepared for the City of Deltona's transportation concurrency requirements and Volusia County's TIA requirements for the driveway connection permit. The study was conducted in accordance with the approved methodology as included in **Appendix B**.

Access

Access to the development (on the east side) is currently provided via two driveways with the northern driveway (exit only) located approximately 650 feet south of Haulover Boulevard and the southern driveway (entrance only) located approximately 900 feet south of Haulover Boulevard. Both driveways will be maintained for the eastern portion of the development, however the southern driveway will be converted to bi-directional. The multi-family development on the west side will have a single driveway that aligns with the southern driveway.

Figure 1 - Site Location Map



Study Area

Based on the River to Sea TPO TIA Guidelines and as included in the approved methodology, the study area includes those roadways where the project impact consumes 3% or more of a roadway's two-way peak-hour generalized service volume. Additionally, the study area includes any critical/near critical roadway segments located within three miles. The study roadway segments and intersections are summarized below:

Study Roadway Segments

- Lake Helen Osteen Road – from Howland Blvd to Elkcam Blvd
- Lake Helen Osteen Road – from Elkcam Blvd to Project
- Lake Helen Osteen Road – from Project to Haulover Blvd
- Lake Helen Osteen Road – from Haulover Blvd to Catalina Blvd
- Catalina Boulevard – from Howland Blvd to Lake Helen Osteen Rd
- Howland Boulevard – from Catalina Blvd to Wolf Pack Run
- Howland Boulevard – from Wolf Pack Run to I-4

Study Intersections

- Lake Helen Osteen Rd at Elkcam Blvd
- Lake Helen Osteen Rd at Project Driveways
- Lake Helen Osteen Rd at Catalina Blvd
- Catalina Blvd at Howland Blvd

EXISTING CONDITIONS

Existing Volumes

For purposes of this study, AM and PM peak-period turning movement counts, from 7:00 AM to 9:00 AM and 4:00 PM to 6:00 PM, were conducted at the study intersections. *Figure 2* and *Figure 3* summarize the existing AM and PM peak-hour turning movement volumes at the study intersections. Based on FDOT's Peak Season Factor Category Report for Volusia County, a seasonal factor of 1.02 for January 18th (the date of the turning movement counts) was applied to the turning movement counts. Printouts of the traffic counts are provided in *Appendix C*.

Existing Roadway Segment Conditions

The existing PM peak-hour two-way volumes on the roadway segments were obtained from Volusia County where available. Since data was not available on Catalina Boulevard, the PM peak-hour two-way volumes were based on the average approach/departure volumes from the PM peak-hour turning movement counts at the Howland Boulevard/Catalina Boulevard and Lake Helen Osteen Road/Catalina Boulevard intersections. The resulting volumes were then compared against the generalized service volume for each study roadway segment. The generalized peak-hour two-way service volume for each roadway segment was obtained from Volusia County's 2022 Average Annual Daily Traffic & Historical Counts based on the adopted level of service standards. *Table 1* shows the adopted level of service and generalized service volume under the adopted level of service for each study roadway segment. As shown in *Table 1*, the existing PM peak-hour two-way volumes for all of the study roadway segments are below the generalized service volume with the exception of the volumes on Providence Boulevard from Fort Smith Boulevard to Elkcam Boulevard. This indicates that all roadway segments currently have acceptable operating conditions with the exception of the study segment of Providence Boulevard.

Figure 2 - Existing AM Peak-Hour Volumes (Year 2024)

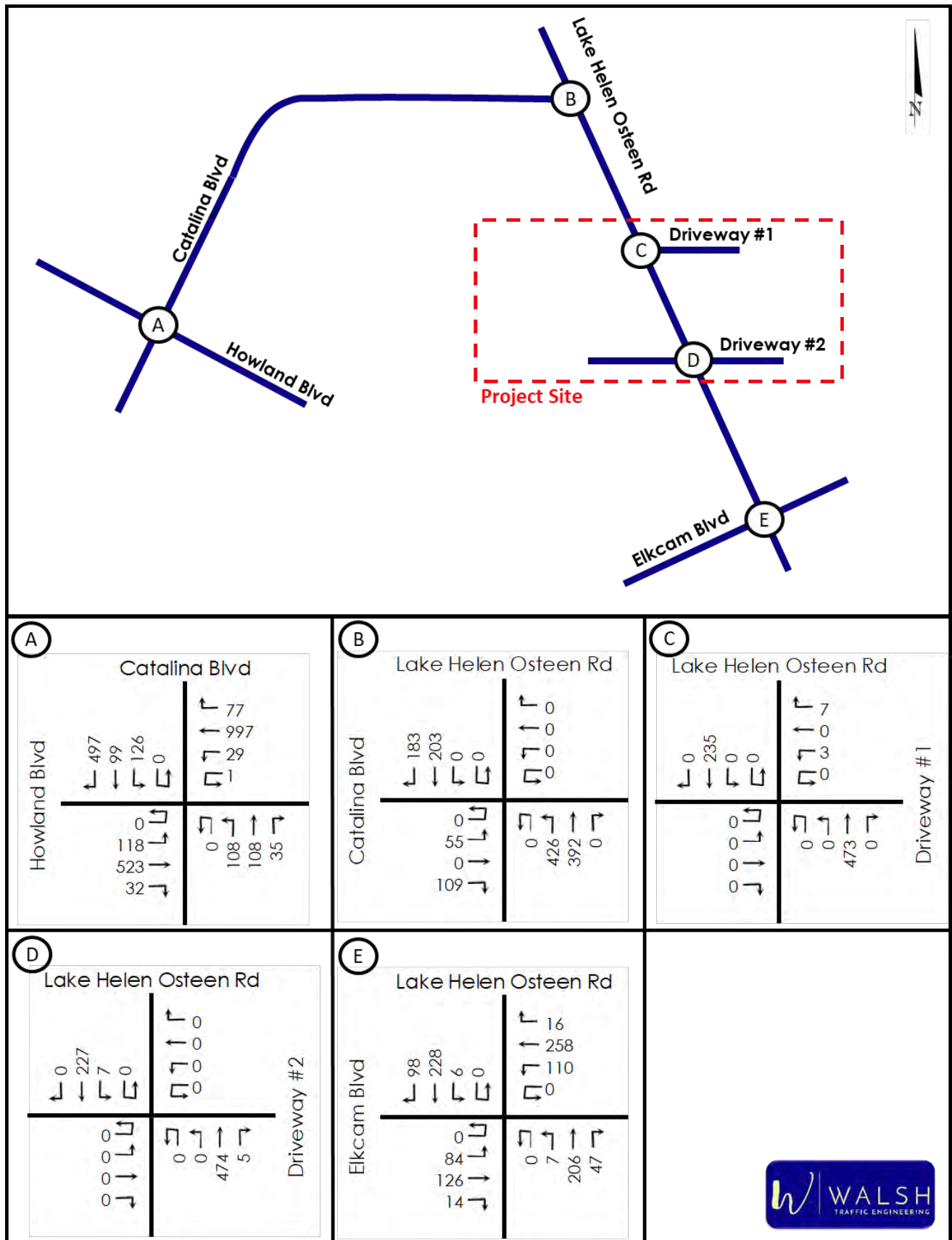


Figure 3 - Existing PM Peak-Hour Volumes (Year 2024)

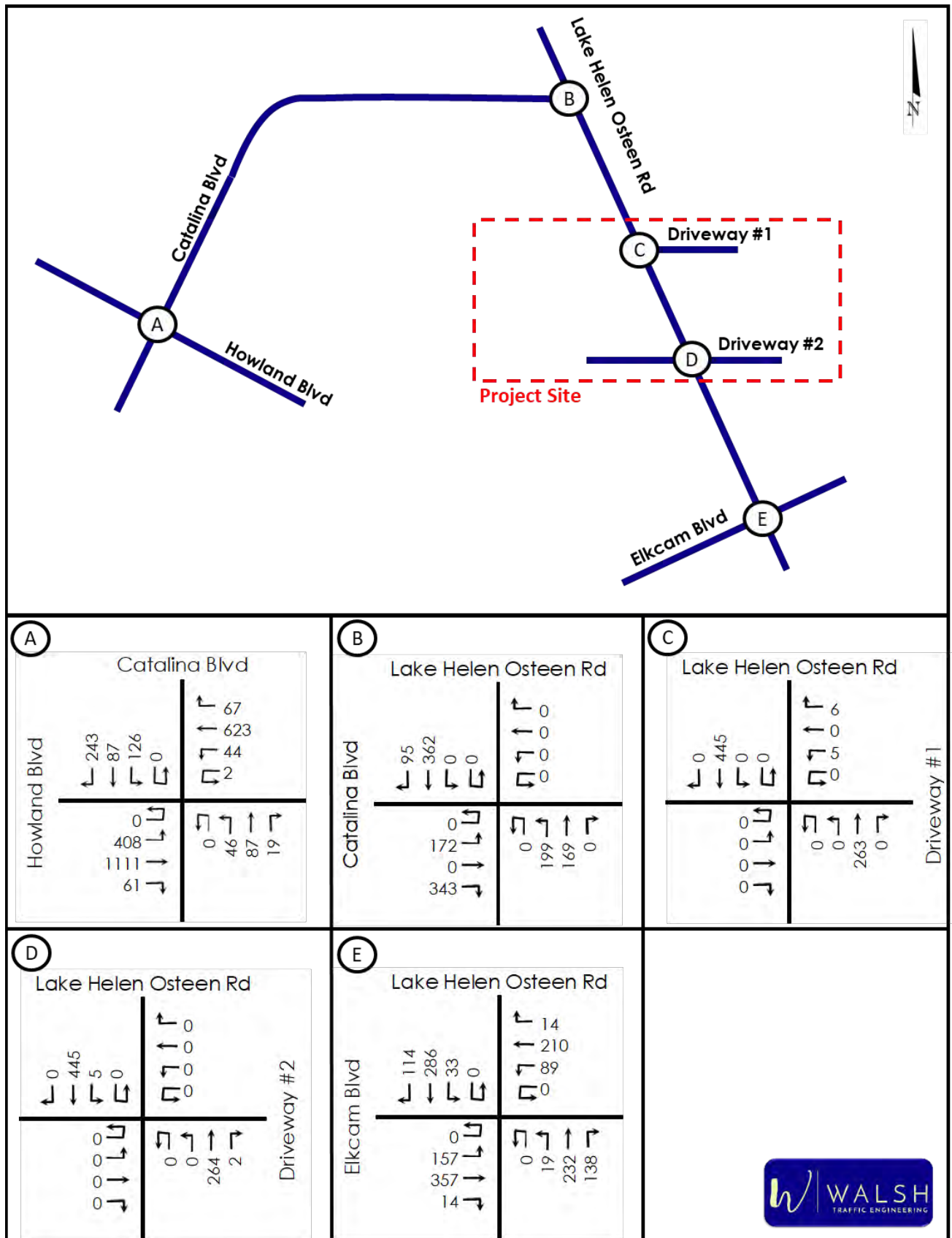


Table 1 - Existing Roadway Segment Operating Conditions (PM Peak Hour)

| Roadway Segment | # of Lanes | Adopted LOS | Service Volume | Existing Volume | | | |
|--------------------------------------|------------|-------------|----------------|-----------------|------|--------|-------------------------|
| | | | | Existing Volume | Year | Source | Volume Exceeds Svc Vol? |
| Lake Helen Osteen Road | | | | | | | |
| Howland Blvd to Elkcaml Blvd | 2 | E | 1,020 | 770 | 2022 | VC | no |
| Elkcaml Blvd to Project | 2 | E | 1,230 | 865 | 2022 | VC | no |
| Project to Haulover Blvd | 2 | E | 1,230 | 865 | 2022 | VC | no |
| Haulover Blvd to Catalina Blvd | 2 | E | 1,230 | 1,170 | 2022 | VC | no |
| Catalina Boulevard | | | | | | | |
| Howland Blvd to Lake Helen Osteen Rd | 2 | E | 1,230 | 1,018 | 2024 | TMC | no |
| Howland Boulevard | | | | | | | |
| Catalina Blvd to Wolf Pack Run | 4 | E | 3,410 | 2,125 | 2022 | VC | no |
| Wolf Pack Run to I-4 | 4 | E | 3,410 | 2,410 | 2022 | VC | no |
| Providence Boulevard | | | | | | | |
| Fort Smith Blvd to Elkcaml Blvd | 2 | E | 1,020 | 1,075 | 2022 | VC | yes |

Note: VC = Volusia County 2022 Counts, TMC = Turning Movement Counts

Existing Intersection Conditions

The AM and PM peak-hour existing operating conditions of the study intersections were evaluated using *Highway Capacity Manual (HCM)*, 6th Edition methodologies with the Synchro 11 software. The existing AM and PM peak-hour turning movement volumes, existing roadway geometry, and existing signal timings (where applicable) were utilized in the analyses. **Table 2** summarizes the results of the intersection operational analyses. All movements at the unsignalized driveway intersections on Lake Helen Osteen Road currently operate well at LOS B or better.

As for the signalized intersections, all three study locations currently have overall acceptable levels of service (LOS) of D or better. The only noted existing deficiency is the southbound right-turn movement at the Howland Boulevard/Catalina Boulevard intersection. This deficiency can be addressed through the optimization of signal timings (signal timing optimization analysis is provided in the buildout conditions analysis). Printouts of the operational analyses are provided in **Appendix D**.

Table 2 - Existing Intersection Operating Conditions (Year 2024)

| | | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | | Overall |
|--|-----------------|-----------|------|------|------|-----------|-------|---|------|------------|------|---|------|------------|-------|-------|------|---------|
| | | L/U | T | R | App | L/U | T | R | App | L/U | T | R | App | L/U | T | R | App | Intxn |
| Howland Blvd at Catalina Blvd - Signalized | | | | | | | | | | | | | | | | | | |
| AM Peak | Delay (sec/veh) | 32.6 | 29.0 | - | 29.6 | 24.4 | 47.7 | - | 47.0 | 32.1 | 28.7 | - | 30.1 | 41.3 | 38.7 | 129.2 | 99.4 | 54.2 |
| | LOS | C | C | - | C | C | D | - | D | C | C | - | C | D | D | F | F | D |
| | V/C | 0.61 | 0.4 | - | - | 0.09 | 0.82 | - | - | 0.33 | 0.22 | - | - | 0.35 | 0.21 | 1.12 | - | - |
| | Queue (ft) | 63 | - | - | - | 15 | - | - | - | 68 | - | - | - | 93 | - | 588 | - | - |
| | Storage (ft) | 315 | - | - | - | 225 | - | - | - | 135 | - | - | - | 190 | - | 375 | - | - |
| PM Peak | Delay (sec/veh) | 29.1 | 24.9 | - | 25.9 | 21.7 | 30.4 | - | 29.9 | 39.1 | 36.0 | - | 36.9 | 48.7 | 45.1 | 55.8 | 51.3 | 31.1 |
| | LOS | C | C | - | C | C | C | - | C | D | D | - | D | D | D | E | D | C |
| | V/C | 0.83 | 0.66 | - | - | 0.2 | 0.52 | - | - | 0.2 | 0.25 | - | - | 0.51 | 0.31 | 0.83 | - | - |
| | Queue (ft) | 188 | - | - | - | 20 | - | - | - | 30 | - | - | - | 95 | - | 160 | - | - |
| | Storage (ft) | 315 | - | - | - | 225 | - | - | - | 135 | - | - | - | 190 | - | 375 | - | - |
| Lake Helen Osteen Rd at Catalina Blvd - Signalized | | | | | | | | | | | | | | | | | | |
| AM Peak | Delay (sec/veh) | 22.7 | - | 27.7 | 26.0 | - | - | - | - | 12.9 | 4.5 | - | 8.9 | - | 20.0 | - | 20.0 | 14.1 |
| | LOS | C | - | C | C | - | - | - | - | B | A | - | A | - | C | - | C | B |
| | V/C | 0.3 | - | 0.69 | - | - | - | - | - | 0.79 | 0.36 | - | - | - | 0.81 | - | - | - |
| | Queue (ft) | 18 | - | - | - | - | - | - | - | 58 | - | - | - | - | - | - | - | - |
| | Storage (ft) | 145 | - | - | - | - | - | - | - | 215 | - | - | - | - | - | - | - | - |
| PM Peak | Delay (sec/veh) | 20.0 | - | 37.4 | 31.6 | - | - | - | - | 15.6 | 7.9 | - | - | - | 26.5 | - | 26.5 | 24.5 |
| | LOS | B | - | B | C | - | - | - | - | B | A | - | - | - | C | - | C | C |
| | V/C | 0.39 | - | 0.88 | - | - | - | - | - | 0.59 | 0.18 | - | - | - | 0.85 | - | - | - |
| | Queue (ft) | 55 | - | - | - | - | - | - | - | 40 | - | - | - | - | - | - | - | - |
| | Storage (ft) | 145 | - | - | - | - | - | - | - | 215 | - | - | - | - | - | - | - | - |
| | | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | | Overall |
| | | L | T | R | App | L | T | R | App | L/U | T | R | App | L | T | R | App | Intxn |
| Lake Helen Osteen Rd at Driveway #1 - 1-Way STOP Control | | | | | | | | | | | | | | | | | | |
| AM Peak | Delay (sec/veh) | - | - | - | - | - | 13.1 | - | 13.1 | - | - | - | - | - | - | - | - | - |
| | LOS | - | - | - | - | - | B | - | B | - | - | - | - | - | - | - | - | - |
| | V/C | - | - | - | - | - | 0.026 | - | - | - | - | - | - | - | - | - | - | - |
| | Queue (ft) | - | - | - | - | - | 3 | - | - | - | - | - | - | - | - | - | - | - |
| | Storage (ft) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| PM Peak | Delay (sec/veh) | - | - | - | - | - | 12.8 | - | 12.8 | - | - | - | - | - | - | - | - | - |
| | LOS | - | - | - | - | - | B | - | B | - | - | - | - | - | - | - | - | - |
| | V/C | - | - | - | - | - | 0.027 | - | - | - | - | - | - | - | - | - | - | - |
| | Queue (ft) | - | - | - | - | - | 3 | - | - | - | - | - | - | - | - | - | - | - |
| | Storage (ft) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Lake Helen Osteen Rd at Driveway #2 - 1-Way STOP Control | | | | | | | | | | | | | | | | | | |
| AM Peak | Delay (sec/veh) | - | - | - | - | - | - | - | - | - | - | - | - | - | 8.6 | - | 0.3 | - |
| | LOS | - | - | - | - | - | - | - | - | - | - | - | - | - | A | - | - | - |
| | V/C | - | - | - | - | - | - | - | - | - | - | - | - | - | 0.008 | - | - | - |
| | Queue (ft) | - | - | - | - | - | - | - | - | - | - | - | - | - | 0 | - | - | - |
| | Storage (ft) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| PM Peak | Delay (sec/veh) | - | - | - | - | - | - | - | - | - | - | - | - | - | 7.9 | - | 0.1 | - |
| | LOS | - | - | - | - | - | - | - | - | - | - | - | - | - | A | - | - | - |
| | V/C | - | - | - | - | - | - | - | - | - | - | - | - | - | 0.005 | - | - | - |
| | Queue (ft) | - | - | - | - | - | - | - | - | - | - | - | - | - | 0 | - | - | - |
| | Storage (ft) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Lake Helen Osteen Rd at Elkcam Blvd - Signalized | | | | | | | | | | | | | | | | | | |
| AM Peak | Delay (sec/veh) | 22.0 | 25.9 | - | 24.5 | 20.9 | 30.1 | - | 27.5 | 19.8 | 27.8 | - | 27.7 | 20.4 | 24.1 | - | 24.0 | 26.2 |
| | LOS | C | C | - | C | C | C | - | C | B | C | - | C | C | C | - | C | C |
| | V/C | 0.33 | 0.45 | - | - | 0.31 | 0.79 | - | - | 0.02 | 0.8 | - | - | 0.04 | 0.6 | - | - | - |
| | Queue (ft) | 28 | - | - | - | 35 | - | - | - | 3 | - | - | - | 3 | - | - | - | - |
| | Storage (ft) | 140 | - | - | - | 60 | - | - | - | 115 | - | - | - | 60 | - | - | - | - |
| PM Peak | Delay (sec/veh) | 24.2 | 42.6 | - | 37.1 | 26.5 | 32.3 | - | 30.6 | 23.2 | 32.8 | - | 32.0 | 23.5 | 32.8 | - | 32.3 | 33.5 |
| | LOS | C | D | - | D | C | C | - | C | C | C | - | C | C | C | - | C | C |
| | V/C | 0.46 | 0.87 | - | - | 0.41 | 0.63 | - | - | 0.17 | 0.85 | - | - | 0.11 | 0.83 | - | - | - |
| | Queue (ft) | 63 | - | - | - | 38 | - | - | - | 13 | - | - | - | 8 | - | - | - | - |
| | Storage (ft) | 140 | - | - | - | 60 | - | - | - | 115 | - | - | - | 60 | - | - | - | - |

FUTURE CONDITIONS

As previously conveyed, the proposed development will have a buildout date of 2029. Therefore, future background volumes and project trips were calculated and combined to arrive at the future total PM peak-hour segment volumes and the AM and PM peak-hour turning movement counts.

Future Background Conditions

ROADWAY SEGMENTS

Future background traffic is the non-project-related traffic projected to utilize the study roadways and intersections. For the purposes of this analysis, the future background traffic was estimated in accordance with Volusia County's Segment Growth Rates and Vested Trips Instruction Policy. For purposes of this process historical traffic counts for the study roadway segments, where available, were obtained. It should be noted that neither the City of Deltona nor Volusia County have vested trip information available for the study roadways/intersections. The resulting growth rate calculations are summarized in *Appendix E* along with the historical annual volumes and historical trend worksheets. *Table 3* below shows the resulting future background PM peak-hour two-way volumes on the study roadway segments. Additionally, *Table 3* below demonstrates that the resulting future background PM peak-hour two-way volumes are projected to be below the generalized service volumes with the exception of those volumes on Lake Helen Osteen Road from Haulover Canal to Catalina Boulevard and on Providence Boulevard from Fort Smith Boulevard to Elkcarn Boulevard. Therefore, both of these roadway segments need to be widened to four lanes to accommodate future background traffic.

Table 3 - Future Background PM Peak-Hour Volumes (Year 2029) for Roadway Segments

| Roadway Segment | Existing Pk Hr Volume | Applied Annual Growth Rate | Existing Year | Buildout Year | Based on Growth Rate | Vested Trips | Applied Volume Growth | Total Background Volume | Service Volume | Bckgrnd Volume Exceeds Svc Vol? |
|--------------------------------------|-----------------------|----------------------------|---------------|---------------|----------------------|--------------|-----------------------|-------------------------|----------------|---------------------------------|
| Lake Helen Osteen Road | | | | | | | | | | |
| Howland Blvd to Elkcarn Blvd | 770 | 3.5% | 2022 | 2029 | 189 | 0 | 189 | 959 | 1,020 | no |
| Elkcarn Blvd to Project | 865 | 1.0% | 2022 | 2029 | 61 | 0 | 61 | 926 | 1,230 | no |
| Project to Haulover Blvd | 865 | 1.0% | 2022 | 2029 | 61 | 0 | 61 | 926 | 1,230 | no |
| Haulover Blvd to Catalina Blvd | 1,170 | 1.0% | 2022 | 2029 | 82 | 0 | 82 | 1,252 | 1,230 | yes |
| Catalina Boulevard | | | | | | | | | | |
| Howland Blvd to Lake Helen Osteen Rd | 1,018 | 1.0% | 2024 | 2029 | 51 | 0 | 51 | 1,069 | 1,230 | no |
| Howland Boulevard | | | | | | | | | | |
| Catalina Blvd to Wolf Pack Run | 2,125 | 1.0% | 2022 | 2029 | 149 | 0 | 149 | 2,274 | 3,410 | no |
| Wolf Pack Run to I-4 | 2,410 | 1.0% | 2022 | 2029 | 169 | 0 | 169 | 2,579 | 3,410 | no |
| Providence Boulevard | | | | | | | | | | |
| Fort Smith Blvd to Elkcarn Blvd | 1,075 | 1.0% | 2022 | 2029 | 75 | 0 | 75 | 1,150 | 1,020 | yes |

INTERSECTIONS

With regards to the future background turning movements, the annual growth rates as established through Volusia County's Segment Growth Rates and Vested Trips Instruction Policy and summarized in *Appendix E*, were applied to existing turning movement volumes. The resulting future background AM and PM peak-hour turning movement volumes are provided in *Figure 4* and *Figure 5*. Turning movement worksheets are provided in *Appendix F*.

Figure 4 - Future Background AM Peak-Hour Volumes (Year 2029)

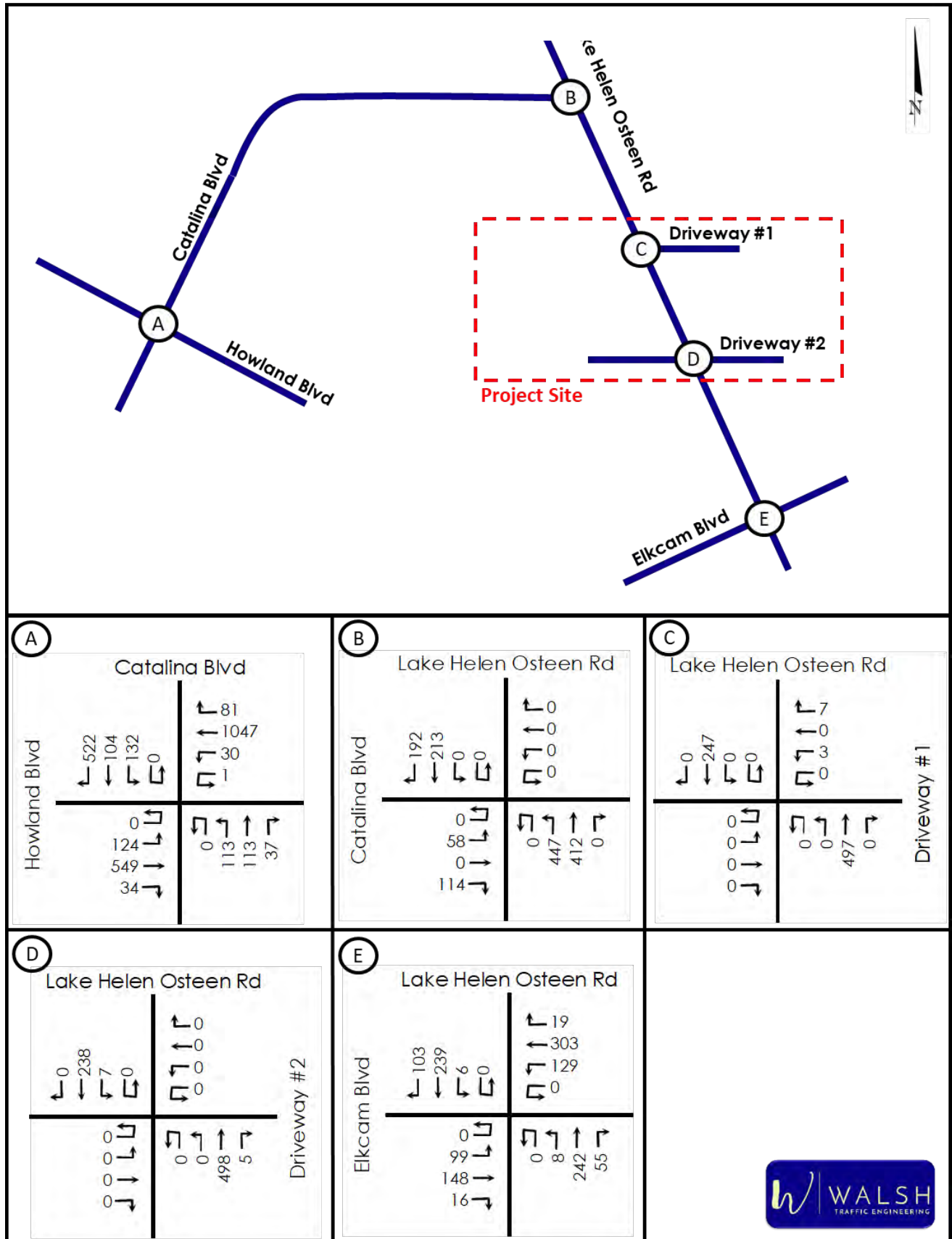
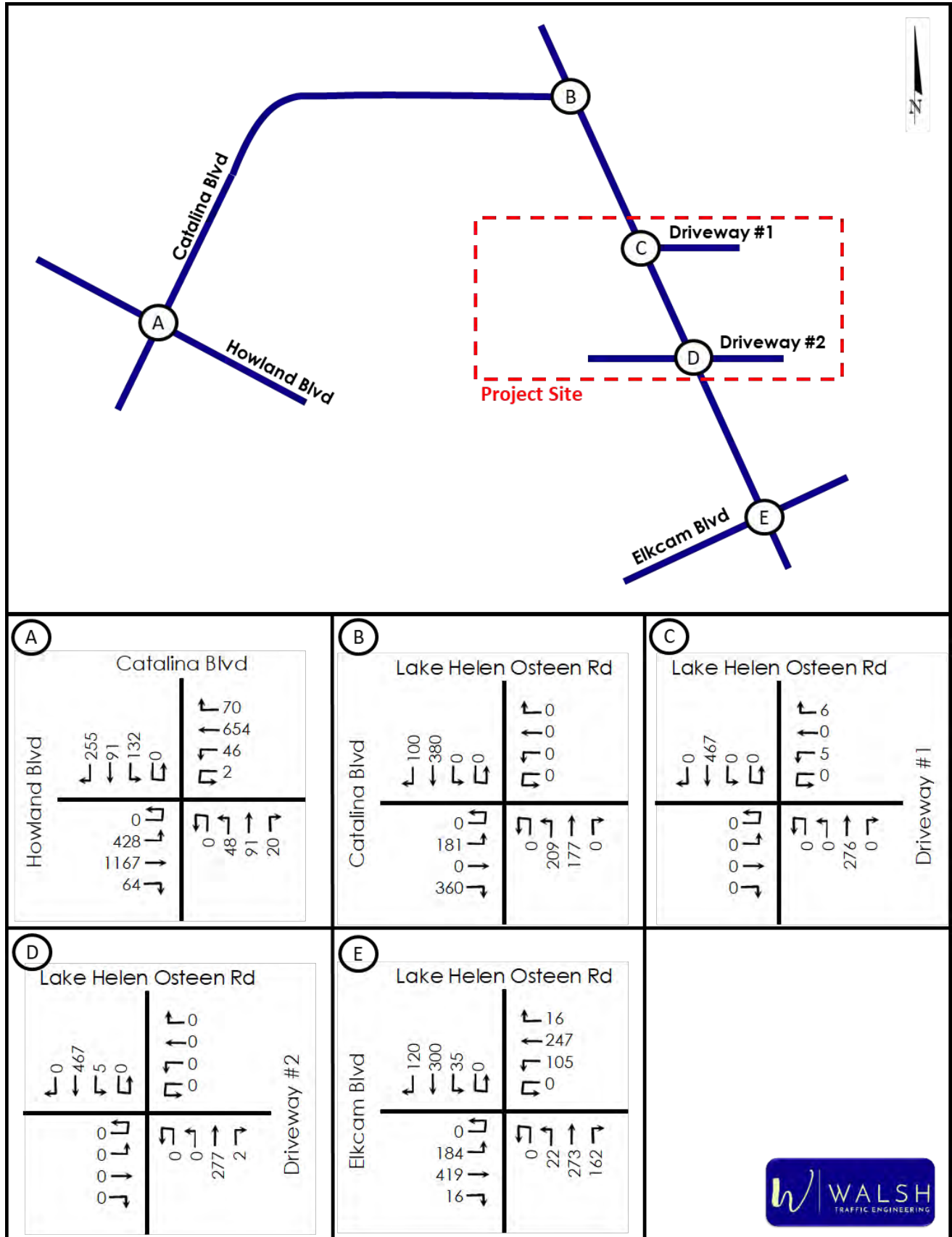


Figure 5 - Future Background PM Peak-Hour Volumes (Year 2029)



Project Trips

TRIP GENERATION

The total daily, AM peak-hour, and PM peak-hour trip generation proposed development is provided below based on trip generation equations/rates provided in the Institute of Transportation Engineer's (ITE) *Trip Generation Manual, 11th Edition*. As summarized below in **Table 4**, and as included in the approved methodology, the proposed development is projected to generate 1,763 total daily trips, 193 total AM peak-hour trips (97 in, 96 out), and 212 total PM peak-hour trips (101 in, 111 out).

Table 4 – Total Trip Generation Summary for Proposed Development

| Land Use | ITE Land Use Code | Intensity | Daily | | |
|-----------------------------------|-------------------|--------------|-------------|-----|-------|
| | | | Total Trips | | |
| | | | In | Out | Total |
| Multi-Family (Low-Rise) | 220 | 120 DU | 422 | 423 | 845 |
| Church | 560 | 31.29 KSF | 119 | 119 | 238 |
| Day Care Center | 565 | 115 Students | 228 | 229 | 457 |
| General Office (Community Center) | 710 | 15.0 KSF | 111 | 112 | 223 |
| Total | | | 880 | 883 | 1,763 |

| Land Use | ITE Land Use Code | Intensity | AM Peak Hour | | |
|-----------------------------------|-------------------|--------------|--------------|-----|-------|
| | | | Total Trips | | |
| | | | In | Out | Total |
| Multi-Family (Low-Rise) | 220 | 120 DU | 14 | 46 | 60 |
| Church | 560 | 31.29 KSF | 6 | 4 | 10 |
| Day Care Center | 565 | 115 Students | 48 | 42 | 90 |
| General Office (Community Center) | 710 | 15.0 KSF | 29 | 4 | 33 |
| Total | | | 97 | 96 | 193 |

| Land Use | ITE Land Use Code | Intensity | PM Peak Hour | | |
|-----------------------------------|-------------------|--------------|--------------|-----|-------|
| | | | Total Trips | | |
| | | | In | Out | Total |
| Multi-Family (Low-Rise) | 220 | 120 DU | 45 | 27 | 72 |
| Church | 560 | 31.29 KSF | 7 | 8 | 15 |
| Day Care Center | 565 | 115 Students | 43 | 48 | 91 |
| General Office (Community Center) | 710 | 15.0 KSF | 6 | 28 | 34 |
| Total | | | 101 | 111 | 212 |

ITE provides a PM peak-hour pass-by rate of 44% for the daycare facility. The pass-by trips were thus calculated and the resulting new external trips identified. Pass-by trips were compared against 14% of the future background traffic on the adjacent section of Lake Helen Osteen Road and, per the River to Sea TPO's TIA Guidelines, determined to be acceptable. As summarized in **Table 5** below, and as included in the approved methodology, the proposed development is projected to generate 193 new external AM peak-hour trips (97 in, 96 out) and 172 new external PM peak-hour trips (82 in, 90 out).

Table 5 – New External Trip Generation Summary for Proposed Development

| Land Use | ITE Land Use Code | Intensity | AM Peak Hour | | | | | | | | | |
|-----------------------------------|-------------------|--------------|--------------|-----|-------|---------------|----|-----|------------------------|----|-----|-------|
| | | | Total Trips | | | Pass-By Trips | | | Net New External Trips | | | |
| | | | In | Out | Total | % | In | Out | Total | In | Out | Total |
| Multi-Family (Low-Rise) | 220 | 120 DU | 14 | 46 | 60 | 0.0% | 0 | 0 | 0 | 14 | 46 | 60 |
| Church | 560 | 31.29 KSF | 6 | 4 | 10 | 0.0% | 0 | 0 | 0 | 6 | 4 | 10 |
| Day Care Center | 565 | 115 Students | 48 | 42 | 90 | 0.0% | 0 | 0 | 0 | 48 | 42 | 90 |
| General Office (Community Center) | 710 | 15.0 KSF | 29 | 4 | 33 | 0.0% | 0 | 0 | 0 | 29 | 4 | 33 |
| Total | | | 97 | 96 | 193 | 0.0% | 0 | 0 | 0 | 97 | 96 | 193 |

| Land Use | ITE Land Use Code | Intensity | PM Peak Hour | | | | | | | | | |
|-----------------------------------|-------------------|--------------|--------------|-----|-------|---------------|----|-----|------------------------|----|-----|-------|
| | | | Total Trips | | | Pass-By Trips | | | Net New External Trips | | | |
| | | | In | Out | Total | % | In | Out | Total | In | Out | Total |
| Multi-Family (Low-Rise) | 220 | 120 DU | 45 | 27 | 72 | 0.0% | 0 | 0 | 0 | 45 | 27 | 72 |
| Church | 560 | 31.29 KSF | 7 | 8 | 15 | 0.0% | 0 | 0 | 0 | 7 | 8 | 15 |
| Day Care Center | 565 | 115 Students | 43 | 48 | 91 | 44.0% | 19 | 21 | 40 | 24 | 27 | 51 |
| General Office (Community Center) | 710 | 15.0 KSF | 6 | 28 | 34 | 0.0% | 0 | 0 | 0 | 6 | 28 | 34 |
| Total | | | 101 | 111 | 212 | 18.9% | 19 | 21 | 40 | 82 | 90 | 172 |

Trip generation was then calculated for the existing development on the eastern portion of the subject property. It is important to note that the existing building currently serves as both a church and a day-care facility. For purposes of calculating trip generation, trips were first calculated based on the 85-student daycare facility. Based on the proposed development, a 10,000 square-foot daycare accommodates 115 students. This equates to approximately 87 square feet required per student. Applying this same ratio to the 85 students, it is estimated that approximately 7,395 square feet of the existing building serves as daycare during the weekdays. Thus, the remaining 8,300 square feet of the existing building is used as a church. As summarized on the following page in **Table 6**, and as included in the approved methodology, the existing development therefore generates 1,195 total daily trips, 69 total AM peak-hour trips (37 in, 32 out) and 71 total PM peak-hour trips (34 in, 37 out).

Similar to the proposed development, pass-by trips were calculated for the existing daycare facility and the resulting new external trips identified. As summarized in **Table 7** on the following page, and as included in the approved methodology, the proposed development is projected to generate 69 new external AM peak-hour trips (37 in, 32 out) and 42 new external PM peak-hour trips (20 in, 22 out).

Table 6 – Total Trip Generation Summary for Existing Development

| Land Use | ITE Land Use Code | Intensity | Daily | | |
|-----------------|-------------------|-------------|-------------|-----|-------|
| | | | Total Trips | | |
| | | | In | Out | Total |
| Church | 560 | 8.30 KSF | 32 | 32 | 63 |
| Day Care Center | 565 | 85 Students | 175 | 175 | 350 |
| Total | | | 207 | 207 | 413 |

| Land Use | ITE Land Use Code | Intensity | AM Peak Hour | | |
|-----------------|-------------------|-------------|--------------|-----|-------|
| | | | Total Trips | | |
| | | | In | Out | Total |
| Church | 560 | 8.30 KSF | 2 | 1 | 3 |
| Day Care Center | 565 | 85 Students | 35 | 31 | 66 |
| Total | | | 37 | 32 | 69 |

| Land Use | ITE Land Use Code | Intensity | PM Peak Hour | | |
|-----------------|-------------------|-------------|--------------|-----|-------|
| | | | Total Trips | | |
| | | | In | Out | Total |
| Church | 560 | 8.30 KSF | 2 | 2 | 4 |
| Day Care Center | 565 | 85 Students | 32 | 35 | 67 |
| Total | | | 34 | 37 | 71 |

Table 7 – New External Trip Generation Summary (Existing Development)

| Land Use | ITE Land Use Code | Intensity | AM Peak Hour | | | | | | | | | |
|-----------------|-------------------|-------------|--------------|-----|-------|---------------|----|-----|------------------------|----|-----|-------|
| | | | Total Trips | | | Pass-By Trips | | | Net New External Trips | | | |
| | | | In | Out | Total | % | In | Out | Total | In | Out | Total |
| Church | 560 | 8.30 KSF | 2 | 1 | 3 | 0.0% | 0 | 0 | 0 | 2 | 1 | 3 |
| Day Care Center | 565 | 85 Students | 35 | 31 | 66 | 0.0% | 0 | 0 | 0 | 35 | 31 | 66 |
| Total | | | 37 | 32 | 69 | 0.0% | 0 | 0 | 0 | 37 | 32 | 69 |

| Land Use | ITE Land Use Code | Intensity | PM Peak Hour | | | | | | | | | |
|-----------------|-------------------|-------------|--------------|-----|-------|---------------|----|-----|-------|------------------------|-----|-------|
| | | | Total Trips | | | Pass-By Trips | | | | Net New External Trips | | |
| | | | In | Out | Total | % | In | Out | Total | In | Out | Total |
| Church | 560 | 8.30 KSF | 2 | 2 | 4 | 0.0% | 0 | 0 | 0 | 2 | 2 | 4 |
| Day Care Center | 565 | 85 Students | 32 | 35 | 67 | 44.0% | 14 | 15 | 29 | 18 | 20 | 38 |
| Total | | | 34 | 37 | 71 | 40.8% | 14 | 15 | 29 | 20 | 22 | 42 |

Recognizing that the existing development is vested, the difference between the existing and proposed development was then calculated. As summarized below in **Table 8**, and as included in the approved methodology, the proposed development modification will increase the AM peak-hour external trips by 124 trips (60 in, 64 out) and the new external PM peak-hour trips by 130 (62 in, 68 out).

Table 8 – New External Trip Generation Increase of Proposed Development

| Land Use | AM Peak Hour | | |
|--|--------------|-----|-------|
| | Total Trips | | |
| | In | Out | Total |
| Proposed Development | 97 | 96 | 193 |
| Existing Development | 37 | 32 | 69 |
| Additonal Trips from Proposed Development | 60 | 64 | 124 |

| Land Use | PM Peak Hour | | |
|--|--------------|-----|-------|
| | Total Trips | | |
| | In | Out | Total |
| Proposed Development | 82 | 90 | 172 |
| Existing Development | 20 | 22 | 42 |
| Additonal Trips from Proposed Development | 62 | 68 | 130 |

TRIP DISTRIBUTION

The trip distribution pattern defines the primary corridors that will be traveled by the traffic generated by the project. The trip distribution for the new external trips, as included in the approved methodology, is shown in *Figure 6*.

Figure 6 – New External Trip Distribution



TRIP ASSIGNMENT

The new external trip generation increase in AM and PM peak-hour project trips from *Table 10* were then assigned to the study roadways and non-access intersections based on the trip distribution. *Figure 7* and *Figure 8* show the AM and PM peak-hour new external trips, assigned to the non-access study intersections.

For the access-related intersections, the turning projections were developed by first removing exiting trips turning into and out of the development. Then, the total new external trips and pass-by trips from Table 5 were assigned to the driveways. When assigning exiting trips from the eastern portion of the development, approximately 50% of the daycare exiting trips destined to the north on Lake Helen Osteen Road and 33% of the daycare exiting trips destined to the south on Lake Helen Osteen Road were assigned to Driveway #1 (northern driveway). All other exiting trips were assigned to Driveway #2. AM and PM peak-hour turning movement projections at the access-related intersections are summarized in *Figure 9* and *Figure 10*.

Figure 7 - AM Peak-Hour Project Trips at Non-Access Intersections (New External)

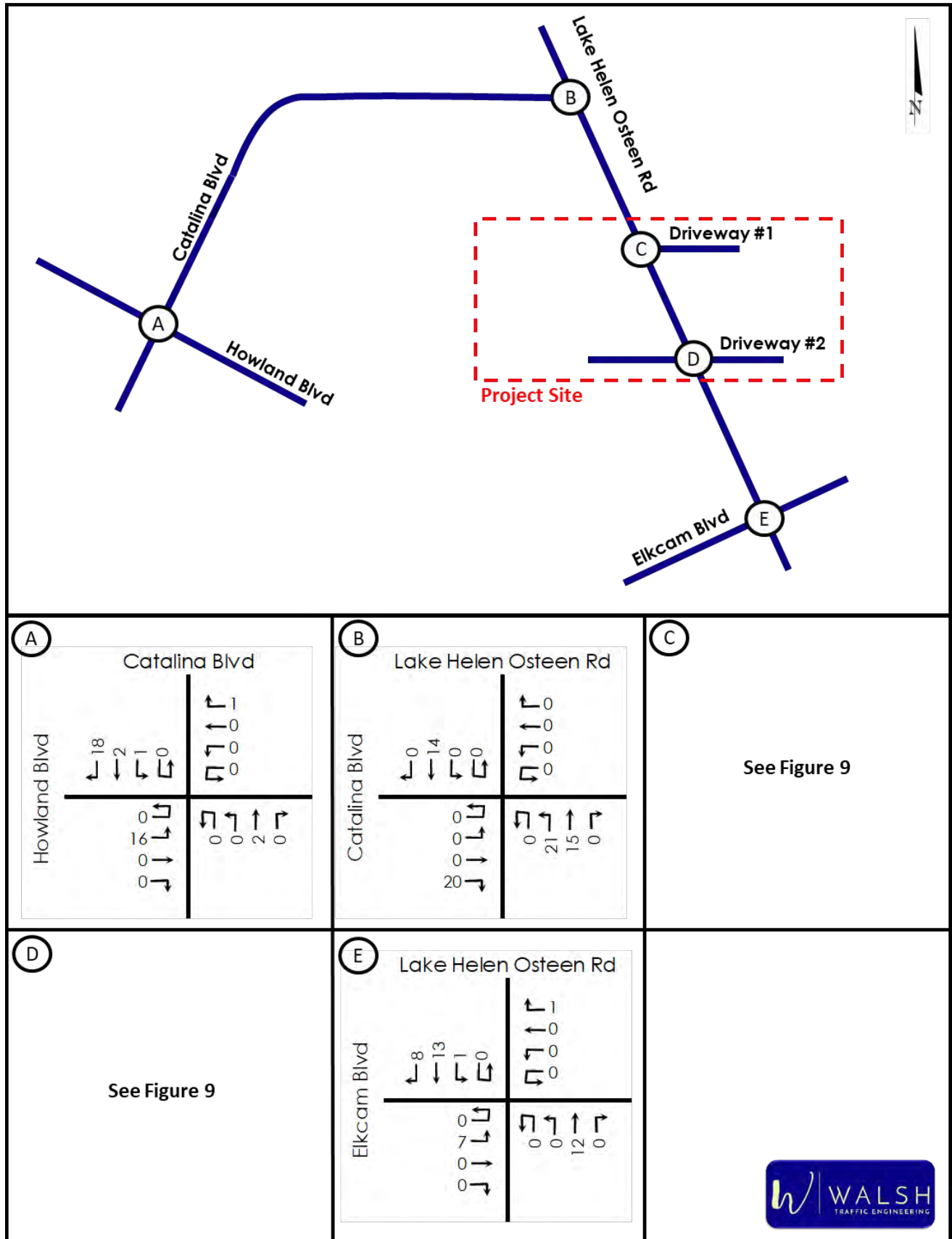


Figure 8 - PM Peak-Hour Project Trips at Non-Access Intersections (New External)

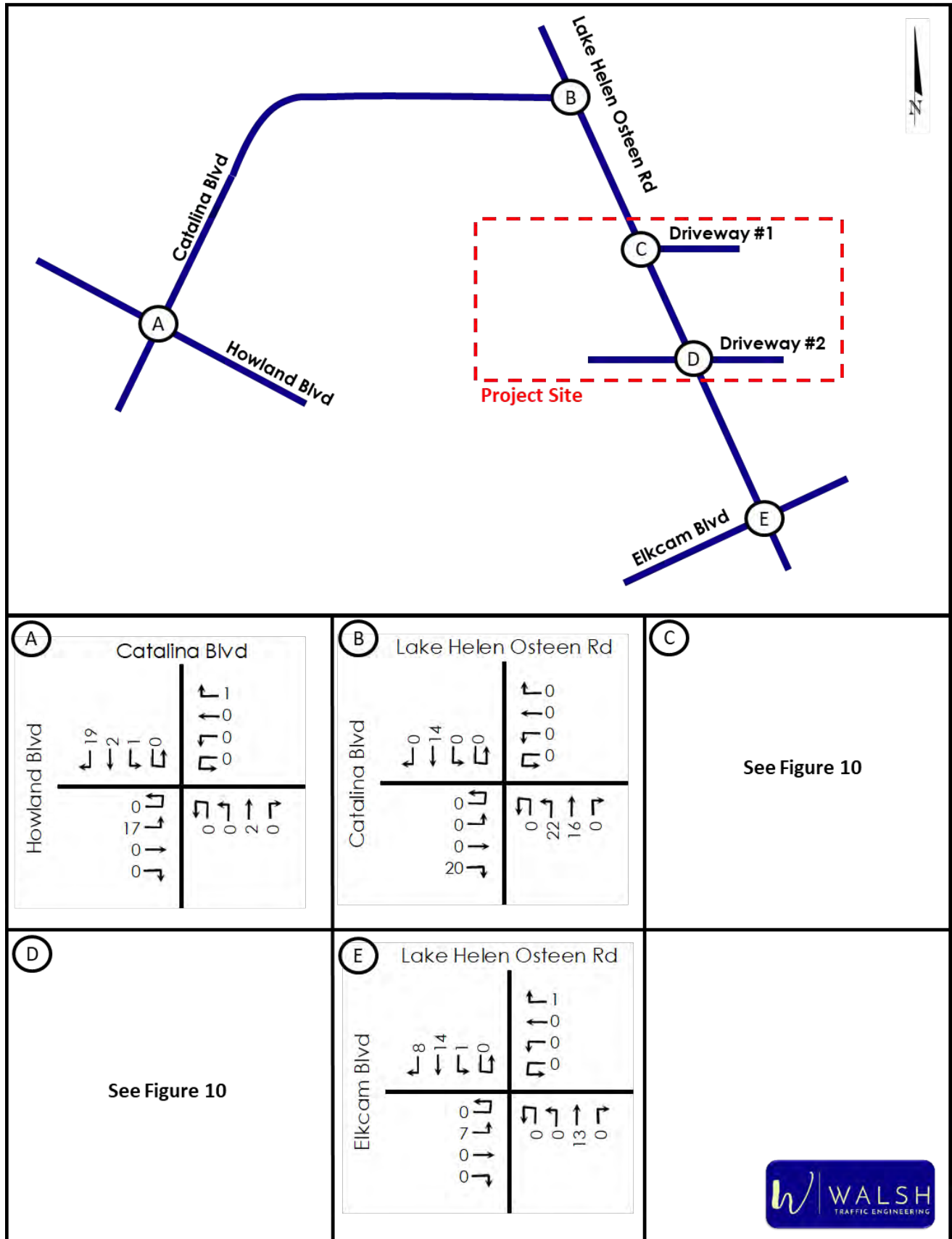


Figure 9 - AM Peak-Hour Project Trips at Access Intersections

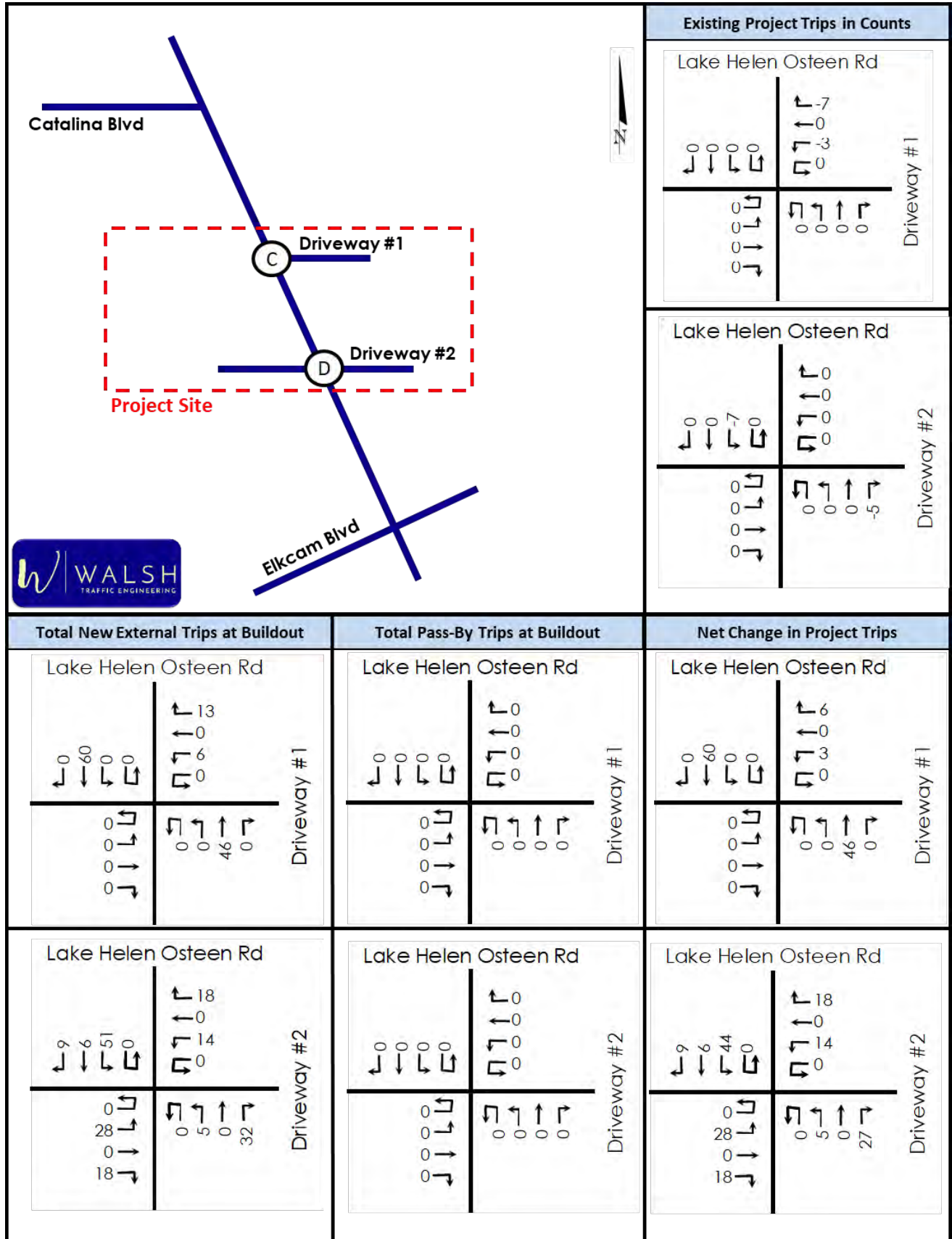
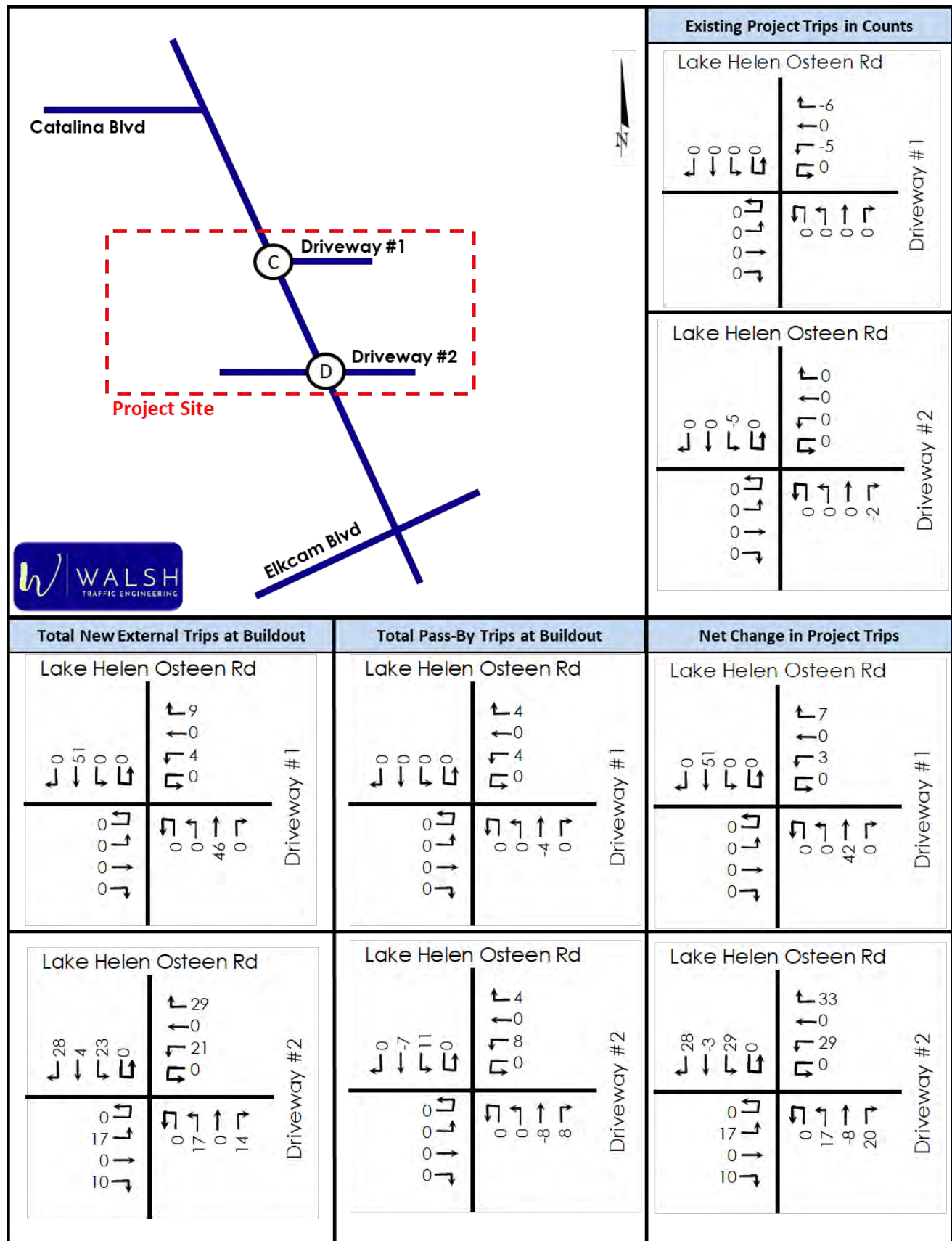


Figure 10 - PM Peak-Hour Project Trips at Access Intersections



Future Buildout Conditions

ROADWAY SEGMENTS

The total projected PM peak-hour two-way segment volumes for the study roadway segments were calculated by adding the new external trip increase for the project to the future background volume projections. The PM peak-hour operating conditions of the study roadway segments were then analyzed by comparing total projected PM peak-hour two-way segment volumes to each roadway segment's generalized service volume. **Table 9** summarizes the total PM peak-hour two-way volumes in year 2029 on the roadway segments at build out of the development. Consistent with the future background conditions analysis, the buildout PM peak-hour two-way volumes are projected to be below the generalized service volumes with the exception of those volumes on Lake Helen Osteen Road from Haulover Canal to Catalina Boulevard and on Providence Boulevard from Fort Smith Boulevard to Elkcam Boulevard. Therefore, consistent with the future background analyses, both of these roadway segments need to be widened to four lanes to accommodate traffic at buildout of the development.

Table 9 - Year 2029 Roadway Segment Operating Conditions (PM Peak Hour)

| Roadway Segment | # of Lanes | Adopted LOS | Total Background Volume | Project Trips | | Total Buildout Volume | Service Volume | Buildout Volume Exceeds Svc Vol? |
|--------------------------------------|------------|-------------|-------------------------|---------------|--------|-----------------------|----------------|----------------------------------|
| | | | | % Assign. | Volume | | | |
| Lake Helen Osteen Road | | | | | | | | |
| Howland Blvd to Elkcam Blvd | 2 | E | 959 | 20.3% | 26 | 985 | 1,020 | no |
| Elkcam Blvd to Project | 2 | E | 926 | 38.8% | 50 | 976 | 1,230 | no |
| Project to Haulover Blvd | 2 | E | 926 | 61.2% | 80 | 1,006 | 1,230 | no |
| Haulover Blvd to Catalina Blvd | 2 | E | 1,252 | 55.6% | 72 | 1,324 | 1,230 | yes |
| Catalina Boulevard | | | | | | | | |
| Howland Blvd to Lake Helen Osteen Rd | 2 | E | 1,069 | 32.7% | 43 | 1,112 | 1,230 | no |
| Howland Boulevard | | | | | | | | |
| Catalina Blvd to Wolf Pack Run | 4 | E | 2,274 | 27.4% | 36 | 2,310 | 3,410 | no |
| Wolf Pack Run to I-4 | 4 | E | 2,579 | 27.1% | 35 | 2,614 | 3,410 | no |
| Providence Boulevard | | | | | | | | |
| Fort Smith Blvd to Elkcam Blvd | 2 | E | 1,150 | 6.3% | 8 | 1,158 | 1,020 | yes |

It is important to note that all improvements identified are the same improvements as those needed to address the future background deficiencies. Per Florida Statutes 163.3180(5)(h)4:

A “transportation deficiency” means a facility or facilities on which the adopted level of service standard is exceeded by the existing, committed, and vested trips, plus additional projected background trips from any source other than the development project under review...

Further, it is conveyed under F.S. 163.3180(5)(h)2b:

If any road is determined to be transportation deficient without the project traffic under review, the costs of correcting that deficiency shall be removed from the project's proportionate-share calculation and the necessary transportation improvements to correct that deficiency shall be considered to be in place for purposes of the proportionate-share calculation. The improvement necessary to correct the transportation deficiency is the funding responsibility of the entity that has maintenance responsibility for the facility. The development's proportionate share shall be calculated only for the needed transportation improvements that are greater than the identified deficiency.

Therefore, because the needed improvements for buildout are the same as those needed to mitigate deficiencies that are projected without the project, the development is not responsible to mitigate impacts to these roadway segments.

INTERSECTIONS

For purposes of analyzing the study intersections at buildout of the development, AM and PM peak-hour turning movement projections were calculated by adding the future background volume projections and the project trips. The resulting total AM and PM peak-hour turning movement projections at buildout of the development are summarized in **Figures 11** and **12** on the following pages.

The AM and PM peak-hour operating conditions for the study intersections were analyzed at build out of the proposed development in year 2029 using the projected turning movements, existing roadway geometry, and existing signal timings (where applicable). **Table 10** summarizes the results of the future buildout intersection operational analyses in 2029. All movements at the unsignalized driveway intersections on Lake Helen Osteen Road are projected to operate acceptably at LOS C or better.

As for the signalized intersections, all three study locations are projected to have overall acceptable levels of service (LOS) of E or better. Consistent with the existing conditions analysis, the only noted projected deficiency is the southbound right-turn movement at the Howland Boulevard/Catalina Boulevard intersection. With the optimization of signal timings, the same improvement needed to address the existing deficiency, this intersection and all movements are projected to operate acceptably. Printouts of the operational analyses are provided in **Appendix G**.

Similar to the roadway segment improvements, because the needed intersection improvement for buildout is the same as that needed to mitigate a deficiency that currently exists without the project, per Florida Statutes 163.3180 the development is not responsible to mitigate impacts to these roadway segments.

Figure 11 – Buildout (Year 2029) AM Peak-Hour Volumes

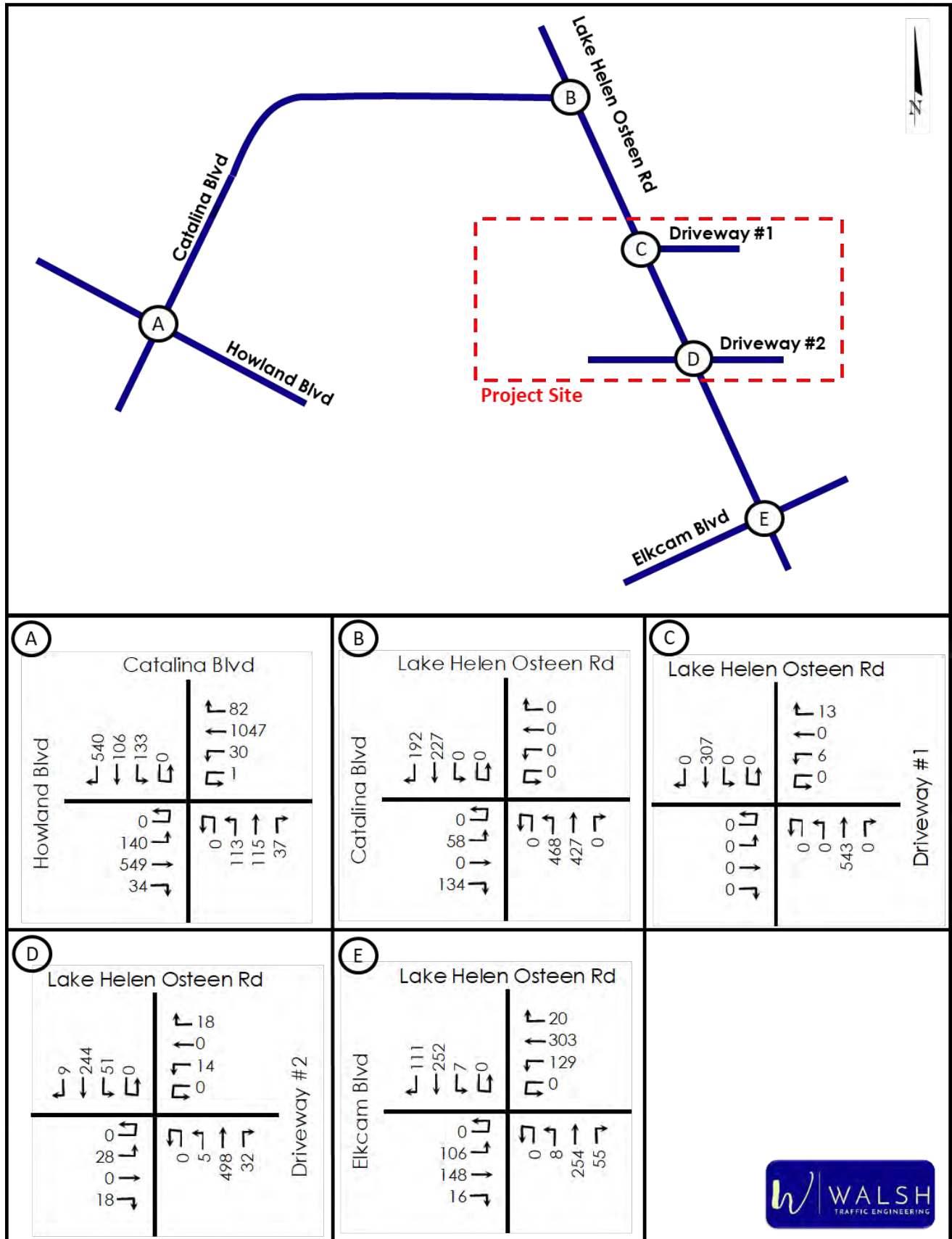


Figure 12 - Buildout (Year 2029) PM Peak-Hour Volumes

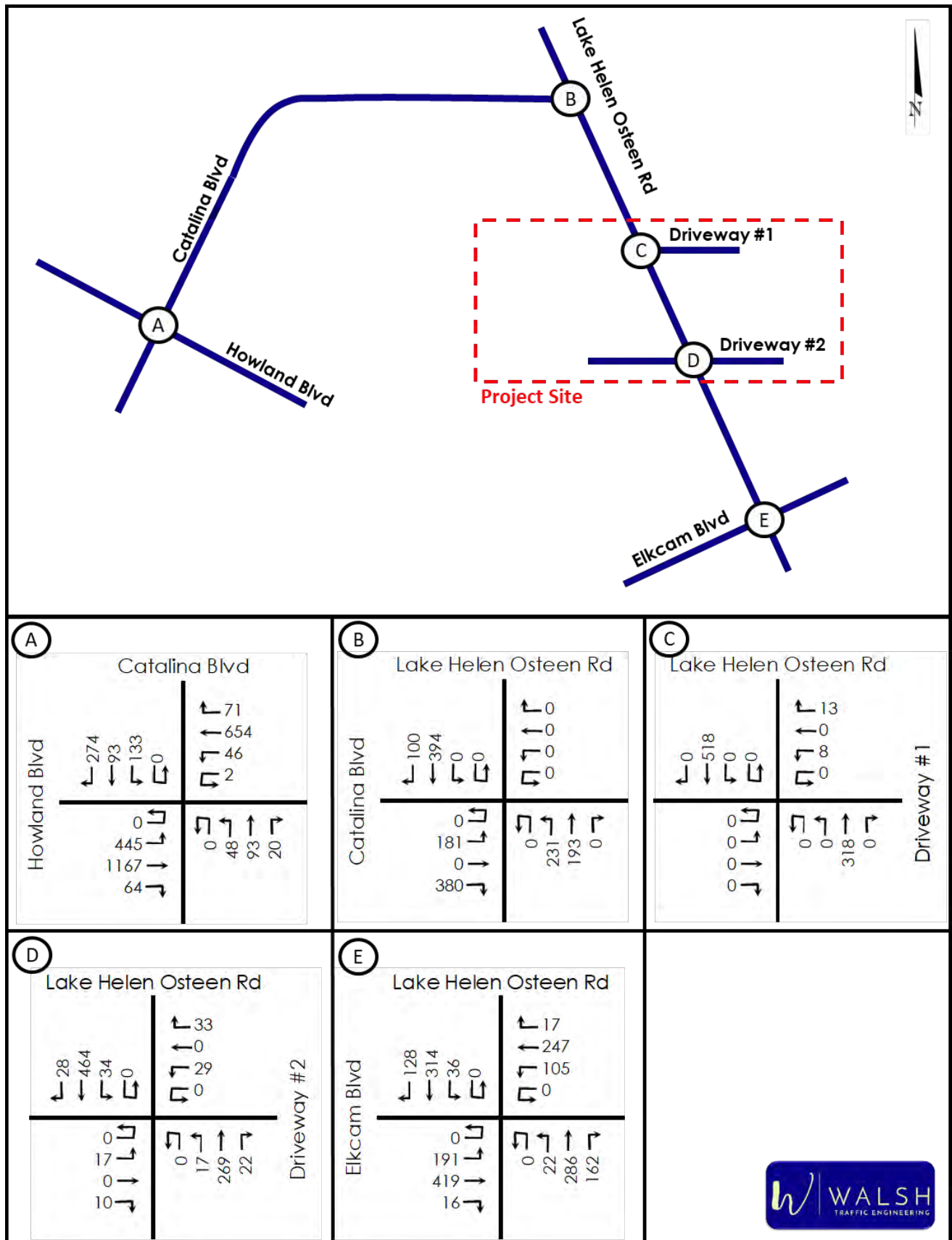


Table 10 – Future Buildout Intersection Operating Conditions (Year 2029)

| | | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | | Overall |
|--|-----------------|-----------|-------|------|------|-----------|-------|---|------|------------|-------|---|------|------------|-------|-------|-------|---------|
| | | L/U | T | R | App | L/U | T | R | App | L/U | T | R | App | L/U | T | R | App | Intxn |
| Howland Blvd at Catalina Blvd - Signalized | | | | | | | | | | | | | | | | | | |
| AM Peak | Delay (sec/veh) | 37.3 | 29.6 | - | 31.1 | 25.2 | 55.1 | - | 54.2 | 32.3 | 28.8 | - | 30.3 | 41.8 | 39.1 | 171.4 | 128.5 | 65.1 |
| | LOS | D | C | - | C | C | E | - | D | C | C | - | C | D | D | F | F | E |
| | V/C | 0.73 | 0.42 | - | - | 0.1 | 0.88 | - | - | 0.35 | 0.23 | - | - | 0.37 | 0.23 | 1.23 | - | - |
| | Queue (ft) | 78 | - | - | - | 15 | - | - | - | 70 | - | - | - | 100 | - | 710 | - | - |
| | Storage (ft) | 315 | - | - | - | 225 | - | - | - | 135 | - | - | - | 190 | - | 375 | - | - |
| PM Peak | Delay (sec/veh) | 45.4 | 27.9 | - | 32.5 | 24.7 | 35.0 | - | 34.3 | 39.3 | 36.5 | - | 37.3 | 49.1 | 45.4 | 57.6 | 52.6 | 36.2 |
| | LOS | D | C | - | C | C | C | - | C | D | D | - | D | D | D | E | D | D |
| | V/C | 0.93 | 0.7 | - | - | 0.23 | 0.57 | - | - | 0.2 | 0.25 | - | - | 0.5 | 0.3 | 0.86 | - | - |
| | Queue (ft) | 268 | - | - | - | 23 | - | - | - | 33 | - | - | - | 105 | - | 195 | - | - |
| | Storage (ft) | 315 | - | - | - | 225 | - | - | - | 135 | - | - | - | 190 | - | 375 | - | - |
| Lake Helen Osteen Rd at Catalina Blvd - Signalized | | | | | | | | | | | | | | | | | | |
| AM Peak | Delay (sec/veh) | 24.3 | - | 30.2 | 28.4 | - | - | - | - | 20.2 | 5.0 | - | 12.9 | - | 23.4 | - | 23.4 | 17.8 |
| | LOS | C | - | C | C | - | - | - | - | B | A | - | A | - | C | - | C | B |
| | V/C | 0.28 | - | 0.73 | - | - | - | - | - | 0.88 | 0.39 | - | - | - | 0.84 | - | - | - |
| | Queue (ft) | 20 | - | - | - | - | - | - | - | 98 | - | - | - | - | - | - | - | - |
| | Storage (ft) | 145 | - | - | - | - | - | - | - | 215 | - | - | - | - | - | - | - | - |
| PM Peak | Delay (sec/veh) | 21.9 | - | 53.1 | 43.0 | - | - | - | - | 18.2 | 8.6 | - | 13.8 | - | 33.7 | - | 33.7 | 31.5 |
| | LOS | C | - | D | D | - | - | - | - | B | A | - | B | - | C | - | C | C |
| | V/C | 0.4 | - | 0.94 | - | - | - | - | - | 0.7 | 0.2 | - | - | - | 0.89 | - | - | - |
| | Queue (ft) | 65 | - | - | - | - | - | - | - | 55 | - | - | - | - | - | - | - | - |
| | Storage (ft) | 145 | - | - | - | - | - | - | - | 215 | - | - | - | - | - | - | - | - |
| | | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | | Overall |
| | | L | T | R | App | L | T | R | App | L/U | T | R | App | L | T | R | App | Intxn |
| Lake Helen Osteen Rd at Driveway #1 - 1-Way STOP Control | | | | | | | | | | | | | | | | | | |
| AM Peak | Delay (sec/veh) | - | - | - | - | - | 15.0 | - | 15.0 | - | - | - | - | - | - | - | - | - |
| | LOS | - | - | - | - | - | C | - | C | - | - | - | - | - | - | - | - | - |
| | V/C | - | - | - | - | - | 0.58 | - | - | - | - | - | - | - | - | - | - | - |
| | Queue (ft) | - | - | - | - | - | 5 | - | - | - | - | - | - | - | - | - | - | - |
| | Storage (ft) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| PM Peak | Delay (sec/veh) | - | - | - | - | - | 13.9 | - | 13.9 | - | - | - | - | - | - | - | - | - |
| | LOS | - | - | - | - | - | B | - | B | - | - | - | - | - | - | - | - | - |
| | V/C | - | - | - | - | - | 0.057 | - | - | - | - | - | - | - | - | - | - | - |
| | Queue (ft) | - | - | - | - | - | 5 | - | - | - | - | - | - | - | - | - | - | - |
| | Storage (ft) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Lake Helen Osteen Rd at Driveway #2 - 1-Way STOP Control | | | | | | | | | | | | | | | | | | |
| AM Peak | Delay (sec/veh) | - | 22.0 | - | 22.0 | - | 19.3 | - | 19.3 | - | 7.9 | - | 0.1 | - | 9.0 | - | 1.5 | - |
| | LOS | - | C | - | C | - | C | - | C | - | A | - | - | - | A | - | - | - |
| | V/C | - | 0.24 | - | - | - | 0.13 | - | - | - | 0.005 | - | - | - | 0.063 | - | - | - |
| | Queue (ft) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| | Storage (ft) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| PM Peak | Delay (sec/veh) | - | 21.0 | - | 21.0 | - | 18.7 | - | 18.7 | - | 8.6 | - | 0.5 | - | 8.0 | - | 0.5 | - |
| | LOS | - | C | - | C | - | C | - | C | - | A | - | - | - | A | - | - | - |
| | V/C | - | 0.121 | - | - | - | 0.214 | - | - | - | 0.019 | - | - | - | 0.032 | - | - | - |
| | Queue (ft) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| | Storage (ft) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Lake Helen Osteen Rd at Elkcam Blvd - Signalized | | | | | | | | | | | | | | | | | | |
| AM Peak | Delay (sec/veh) | 23.6 | 27.6 | - | 26.0 | 21.8 | 35.3 | - | 31.4 | 22.1 | 27.1 | - | 26.9 | 21.4 | 30.6 | - | 30.5 | 29.1 |
| | LOS | C | C | - | C | C | D | - | C | C | C | - | C | C | C | - | C | C |
| | V/C | 0.42 | 0.46 | - | - | 0.35 | 0.84 | - | - | 0.05 | 0.68 | - | - | 0.03 | 0.83 | - | - | - |
| | Queue (ft) | 38 | - | - | - | 45 | - | - | - | 3 | - | - | - | 3 | - | - | - | - |
| | Storage (ft) | 140 | - | - | - | 60 | - | - | - | 115 | - | - | - | 60 | - | - | - | - |
| PM Peak | Delay (sec/veh) | 27.9 | 66.2 | - | 54.5 | 31.4 | 39.5 | - | 37.2 | 25.6 | 43.1 | - | 42.3 | 26.1 | 38.4 | - | 37.4 | 44.1 |
| | LOS | C | E | - | D | C | D | - | D | C | D | - | D | C | D | - | D | D |
| | V/C | 0.57 | 0.96 | - | - | 0.54 | 0.71 | - | - | 0.13 | 0.89 | - | - | 0.22 | 0.84 | - | - | - |
| | Queue (ft) | 90 | - | - | - | 53 | - | - | - | 15 | - | - | - | 10 | - | - | - | - |
| | Storage (ft) | 140 | - | - | - | 60 | - | - | - | 115 | - | - | - | 60 | - | - | - | - |

Project Driveway Turn-Lane Analysis

Driveway #1 on Lake Helen Osteen Road is and will remain exit only. Therefore, this driveway was not evaluated for turn lanes on Lake Helen Osteen Road into the site. However, Driveway #2 on Lake Helen Osteen Road was evaluated for the need for a northbound and/or southbound right-turn lane based on Section 72-619 of the Volusia County Land Development Code recognizing that Lake Osteen Road is a Volusia County roadway. Based on Volusia County's LDC, a right-turn lane is warranted for roadways with posted speed limits of 35 miles per hour or where the right-turn volume is projected to exceed 100 vehicles per hour. The northbound right-turn volume is projected to be 32 vehicles in the AM peak hour and 22 vehicles in the PM peak hour. Thus, from a traffic volume perspective, the northbound right-turn volume is well below the County's volume threshold for warranting a right-turn lane. However, given that the northbound right-turn lane serves the day care center as well as the church, a northbound right-turn lane of 320 feet is recommended based on the County's LDC given the 45-mph posted speed limit. The 320-foot turn-lane length includes a 50-foot taper.

The southbound right-turn volume is projected to be 9 vehicles in the AM peak hour and 28 vehicles in the PM peak hour. Thus, from a traffic volume perspective, the northbound right-turn volume is well below the County's volume threshold for warranting a right-turn lane. Although the posted speed limit is 45 mph, a waiver of the requirements for a southbound right-turn lane is requested given that the right-turn volumes are only projected to reach, at most, 30% of the County's volume threshold requirements.

Lake Helen Osteen Road at Driveway #2 was also evaluated for the need for northbound and southbound left-turn lanes on Lake Helen Osteen Road based on Section 72-619 of the Volusia County Land Development Code. Based on the County's LDC, a left-turn lane is warranted for roadways where the left-turn volume is projected to exceed 25 vehicles per hour. The northbound left-turn volume is projected to be five (5) vehicles in the AM peak hour and 17 vehicles in the PM peak hour. Thus, a northbound left-turn lane is not warranted.

The southbound left-turn volume is projected to exceed the 25 vehicle per hour threshold. Thus, a southbound right-turn lane of 370 feet is recommended based on a 50-foot queue (the 95th percentile queue is less than two vehicles) plus a deceleration distance of 320 feet based on the County's LDC given the 45-mph posted speed limit. The 370-foot turn-lane length includes a 50-foot taper.

Internal Site Queue Analysis for Daycare Operations

Based on **Table 4**, the proposed daycare will have 48 inbound AM peak-hour trips and 42 inbound PM peak-hour trips. There will be an additional 35 AM and 13 PM peak-hour non-daycare trips destined to parking spaces in the eastern portion of the development. These additional trips were not included in the queue analysis as they are expected to pull directly into the parking spaces.

The daycare will be located at the easternmost portion of the property. The existing entry driveway extends approximately 400' to the eastern end of the existing church. Then an additional 300' of parking aisle leads to the front of the daycare facility. This combined 700' can accommodate 28 vehicles. It is estimated that 25% of drop offs will occur with motorists parking and walking their children into the facility. Thus, these motorists will not be involved in the drop-off queues. If half of the peak-hour entering vehicles to be queued arrive in a 15-minute increment, that would equate to 18 queued vehicles ($48 \times 75\%$ to be queued $\times 50\%$ in 15-minute increment) in the AM peak hour and 17 queue vehicles ($43 \times 75\% \times 50\%$) in the PM peak hour. Without even considering a staggering-of-the-vehicles, 18 vehicles equate to a 450-foot queue and 17 vehicles to a 425-foot queue. Thus, the back of the worst-case queue would be contained on-site approximately 250' east of Lake Helen Osteen Road.

Alternative Mode Analysis

Per the River to Sea TPO TIA Guidelines, an evaluation relating to transit, pedestrian, and bicycle facilities is provided below.

Transit – Votran does not provide fixed-route transit service in close proximity to the development. The nearest fixed-route service is nearly two miles away at the Howland Boulevard/Elkcam Boulevard intersection (routes 21/22).

Pedestrian Facilities – Currently, sidewalks are not provided on either side of Lake Helen Osteen Road. However, a 5' walkway will be provided around the western portion of the development with pedestrian connections to the various buildings. Internal pedestrian connectivity will be provided in the eastern portion along with the provision of a sidewalk that runs parallel with Lake Helen Osteen Road within the development. This sidewalk will provide the opportunity for adjacent properties to provide sidewalk connectivity along the east side of Lake Helen Osteen Road. It is also proposed to provide a midblock crosswalk with a refuge island across Lake Helen Osteen Road on the south side of the south driveway intersection.

Bicycle Facilities – There are no bicycle facilities provided along Lake Helen Osteen Road.

Crash Analysis

A five-year crash analysis (January 1, 2019 to December 31, 2023) was conducted on Lake Helen Osteen Road immediately adjacent to the proposed development. Based on the University of Florida's Signal Four Analytics, there was only one rear-end crash (property damage only) on Lake Helen Osteen Road (see Signal Four Analytics screenshot of analysis in *Appendix I*). No other crashes were identified. Thus, there is no existing crash trend on Lake Helen Osteen Road adjacent to the development. Further, the development is not projected to trigger any new roadway segment/intersection deficiencies. Therefore, no additional crash analyses were required per the approved methodology.

CONCLUSIONS

A traffic impact analysis was prepared for the proposed New Hope PUD located on Lake Helen Osteen Road, south of Haulover Boulevard in Deltona, Florida. Below is a summary of the findings of the study:

- Based on the existing conditions analyses, all study roadway segments currently operate at an acceptable level of service (LOS) with the exception of the volumes on Providence Boulevard from Fort Smith Boulevard to Elkcarn Boulevard.
- Based on the future background conditions analyses, all study roadway segments are projected to operate acceptably with the exception Lake Helen Osteen Road from Haulover Canal to Catalina Boulevard and Providence Boulevard from Fort Smith Boulevard to Elkcarn Boulevard. Both of these roadway segments need to be widened to four lanes to accommodate future background traffic.
- Based on the future buildout conditions analyses, consistent with the future background analyses, all study roadway segments are projected to operate acceptably with the exception Lake Helen Osteen Road from Haulover Canal to Catalina Boulevard and Providence Boulevard from Fort Smith Boulevard to Elkcarn Boulevard. Both of these roadway segments need to be widened to four lanes to accommodate future background traffic. These improvements identified are the same improvements as those needed to address the future background deficiencies. Therefore, per Florida Statutes 163.3180, because the needed improvements for buildout are the same as those needed to mitigate deficiencies that are projected without the project, the development is not responsible to mitigate impacts to these roadway segments.
- Based on the existing conditions intersection analyses, all movements at the unsignalized driveway intersections on Lake Helen Osteen Road currently operate well at LOS B or better. As for the signalized intersections, all three study locations currently have overall acceptable levels of service (LOS) of D or better. The only noted existing deficiency is the southbound right-turn movement at the Howland Boulevard/Catalina Boulevard intersection which can be addressed through the optimization of signal timings.
- Based on the future buildout intersection analyses, all movements at the unsignalized driveway intersections on Lake Helen Osteen Road are projected to operate acceptably at LOS C or better. As for the signalized intersections, all three study locations are projected to have overall acceptable levels of service (LOS) of E or better. Consistent with the existing conditions analysis, the only noted projected deficiency is the southbound right-turn movement at the Howland Boulevard/Catalina Boulevard intersection. With the optimization of signal timings, the same improvement needed to address the existing deficiency, this intersection and all movements are

projected to operate acceptably. Because the needed intersection improvement for buildout is the same as that needed to mitigate a deficiency that currently exists without the project, per Florida Statutes 163.3180 the development is not responsible to mitigate impacts to these roadway segments.

- Driveway #1 on Lake Helen Osteen Road is and will remain exit only.
- Relative to Driveway #2 on Lake Helen Osteen Road
 - A northbound right-turn lane of 320 feet is recommended.
 - A southbound right-turn lane is not recommended.
 - A northbound left-turn lane is not warranted.
 - A southbound right-turn lane of 370 feet is recommended
- The daycare will be located at the easternmost portion of the property. The back of the worst-case projected queue will be contained on-site approximately 250' east of Lake Helen Osteen Road. Based on the buildout conditions (year 2026) intersection analyses:
- A 5' walkway will be provided around the western portion of the development with pedestrian connections to the various buildings. Internal pedestrian connectivity will be provided in the eastern portion along with the provision of a sidewalk that runs parallel with Lake Helen Osteen Road within the development. This sidewalk will provide the opportunity for adjacent properties to provide sidewalk connectivity along the east side of Lake Helen Osteen Road. It is also proposed to provide a midblock crosswalk with a refuge island across Lake Helen Osteen Road on the south side of the south driveway intersection.
- All movements at the STOP-controlled intersections are projected to operate acceptably.
- Based on a five-year crash analysis there is no existing crash trend on Lake Helen Osteen Road adjacent to the development.

Appendix A

Preliminary Development Plan



| Residential Data | | | | |
|-----------------------|---------------|------------|-------------|------------|
| Description | | | Required | Proposed |
| Lot | | | | |
| Parcel ID | | | | |
| | | | | |
| 811000000080 | 83,199.60 sf | 1.91 Acres | | |
| 811000000041 | 196,020.00 sf | 4.50 Acres | | |
| Lot Area Summary | | | | |
| Gross Lot Area: | 279,220 sf | 6.41 Acres | | |
| | | | | |
| Zonning District | | | | |
| | | | District | |
| Proposed Residential | 279,220 sf | | | PUD |
| | 6.41 Acres | | | |
| Density | | | | |
| Density | 6.41 Acres | | 77 Units | 120 Units |
| | | | 12.00 Du/AC | 0 |
| Building Height | | | | |
| Building Height: | | | | 40'-0" |
| | | | | 0 |
| Building Setbacks | | | | |
| Front Setback (East) | | | 25'-0" | 41'-0" |
| Side Setback (North) | | | 25'-0" | 25'-0" |
| Side Setback (South) | | | 25'-0" | 25'-0" |
| Rear Setback (West) | | | 25'-0" | 56'-0" |
| General Requirements | | | | |
| Floor Area Ratio | | | | 121,486 sf |
| | | | | 43.51% |
| Lot Coverage | | | N/A | 45,500 sf |
| | | | | 16.30% |
| Landscape Open Space: | | | 69,805 sf | 91,783 sf |
| | | | 25 % | 32.87% |
| Total Paved Area | | | N/A | 120,214 sf |
| | | | | 43.05% |
| Sidewalk Area | | | N/A | 21,723 sf |
| | | | | 7.78% |

| Building Area A | | | | | |
|--|---------------|--------------|-----------------|--|---------------------|
| Total Sq Ft. does not include Balcony Sq Ft. | | | | | |
| Levels | Leasable Area | Non-Leasable | | | Total Bldg Gross SF |
| Level 1 | 7,860 sf | 1,247 sf | | | 9,107 sf |
| Level 2 | 7,860 sf | 1,087 sf | | | 8,947 sf |
| Level 3 | 7,860 sf | 1,087 sf | | | 8,947 sf |
| | | | | | |
| Total | 23,580 sf | 3,421 sf | | | 27,001 sf |
| | | | Total of 2 Bldg | | 54,002 sf |
| | | | | | |
| Building Area B | | | | | |
| Total Sq Ft. does not include Balcony Sq Ft. | | | | | |
| Levels | Leasable Area | Non-Leasable | | | Total Bldg Gross SF |
| Level 1 | 9,564 sf | 1,778 sf | | | 11,342 sf |
| Level 2 | 9,564 sf | 1,636 sf | | | 11,200 sf |
| Level 3 | 9,564 sf | 1,636 sf | | | 11,200 sf |
| | | | | | |
| Total | 28,692 sf | 5,050 sf | | | 33,742 sf |
| | | | Total of 2 Bldg | | 67,484 sf |

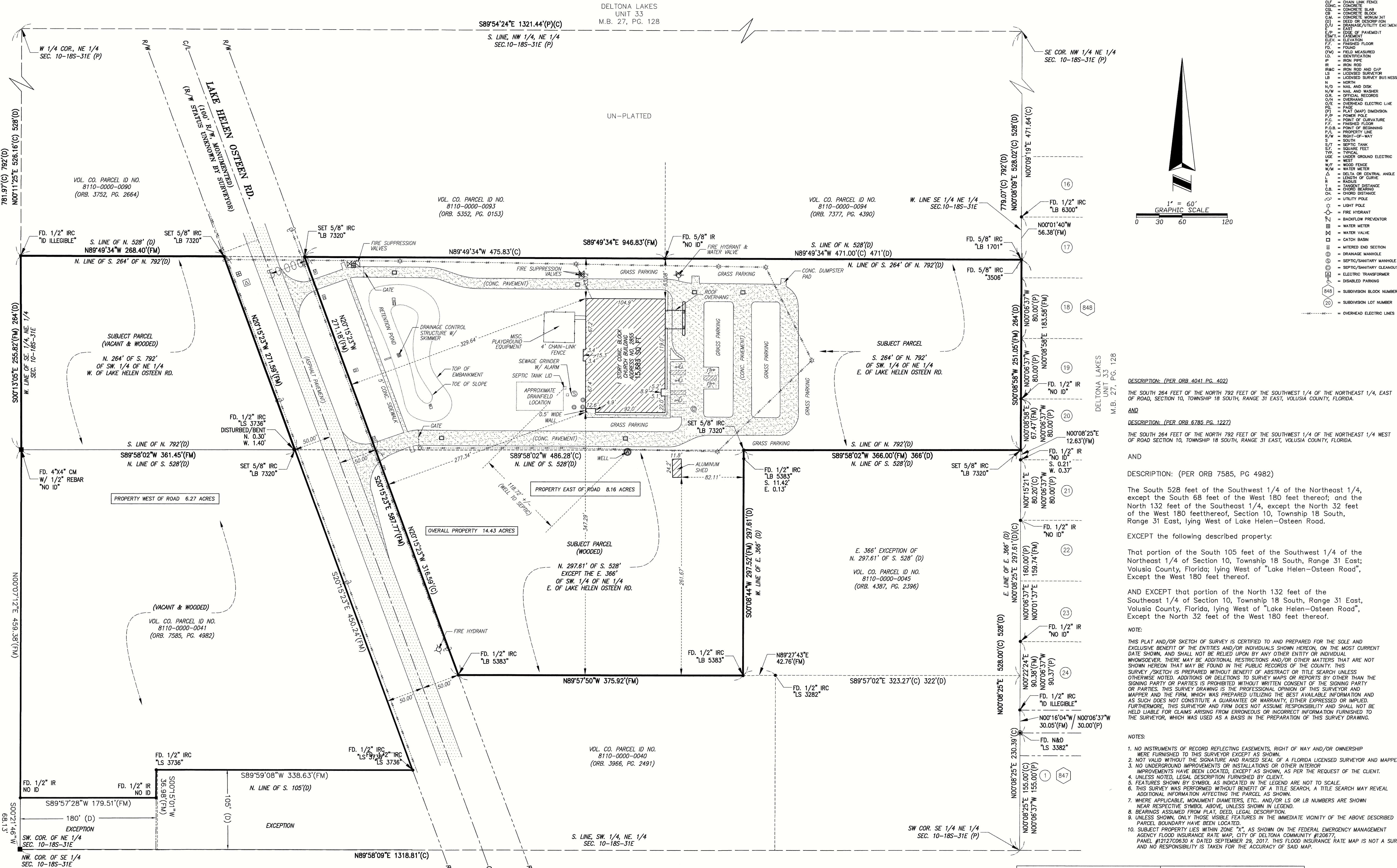
| Unit Area | | | | | | |
|-----------------|---------|--|---------------|---------------|--------------|-------------|
| | | | Unit A (1 BD) | Unit B (2 BD) | Uni C (3 BD) | Total Units |
| | | | 651 sf | 870 sf | 1,095 sf | |
| | | | | | | |
| | | | | | | |
| Type A | Level 1 | | | 4 Units | 4 Units | 8 Units |
| | Level 2 | | | 4 Units | 4 Units | 8 Units |
| | Level 3 | | | 4 Units | 4 Units | 8 Units |
| Sub Total | | | | 12 Units | 12 Units | 24 Units |
| Total of 2 Bldg | | | | 24 Units | 24 Units | 48 Units |
| | | | | | | |
| Type B | Level 1 | | 4 Units | 8 Units | | 12 Units |
| | Level 2 | | 4 Units | 8 Units | | 12 Units |
| | Level 3 | | 4 Units | 8 Units | | 12 Units |
| Sub Total | | | 12 Units | 24 Units | | 36 Units |
| Total of 2 Bldg | | | 24 Units | 48 Units | | 72 Units |
| | | | | | | |
| | | | | Total Units | | 120 Units |

| Residential Parking Requirement | | | | | | | |
|---------------------------------|------------|-------------------------------------|----------|-----------|---------------|------------|------------|
| | | | | | | Required | Provided |
| | | | | | | | |
| | | | | | | | |
| Unit A (1 BD) | 24 Units | 20.00% | | | 1.5 SP/DU | 36 spaces | |
| Unit B (2 BD) | 72 Units | 60.00% | | | 2.0 SP/DU | 144 spaces | |
| Uni C (3 BD) | 24 Units | 20.00% | | | 2.0 SP/DU | 48 spaces | |
| Total Units | 120 Units | 100.00% | | | | | |
| Visitors | | | | | 1 sp/10 units | 12 spaces | |
| | | | | | Sub Total | 240 spaces | |
| | | | | | | | |
| | | | | | | | |
| | | | | Sub Total | | 240 spaces | |
| | | | | | | | |
| Parking Provided | | | | | | | |
| | | | | | | | |
| Surface | Standard | HC | Parallel | | | | 240 spaces |
| | 233 | 7 | | | | | |
| | | | | | | 240 spaces | 240 spaces |
| | | | | | | | |
| | | | | | | | |
| Bicycle Requirements | | | | | | | |
| Parking Space | 240 spaces | 6 Plus 1 for each 20 Autos over 100 | | | | 10 spaces | 10 spaces |

SECTION 10, TOWNSHIP 18 SOUTH, RANGE 31 EAST
CITY OF DELTONA, VOLUSIA COUNTY, FLORIDA

DELTONA LAKES
UNIT 33
M.B. 27, PG. 128

UN-PLATTED



DESCRIPTION: (PER ORB 4041 PG. 402)
THE SOUTH 264 FEET OF THE NORTH 792 FEET OF THE SOUTHWEST 1/4 OF THE NORTHEAST 1/4, EAST OF ROAD, SECTION 10, TOWNSHIP 18 SOUTH, RANGE 31 EAST, VOLUSIA COUNTY, FLORIDA.

AND
DESCRIPTION: (PER ORB 6785 PG. 1227)
THE SOUTH 264 FEET OF THE NORTH 792 FEET OF THE SOUTHWEST 1/4 OF THE NORTHEAST 1/4 WEST OF ROAD SECTION 10, TOWNSHIP 18 SOUTH, RANGE 31 EAST, VOLUSIA COUNTY, FLORIDA.

AND
DESCRIPTION: (PER ORB 7585, PG 4982)
The South 528 feet of the Southwest 1/4 of the Northeast 1/4, except the South 68 feet of the West 180 feet thereof, and the North 132 feet of the Southeast 1/4, except the North 32 feet of the West 180 feet thereof, Section 10, Township 18 South, Range 31 East, lying West of Lake Helen-Osteen Road.

EXCEPT the following described property:
That portion of the South 105 feet of the Southwest 1/4 of the Northeast 1/4 of Section 10, Township 18 South, Range 31 East; Volusia County, Florida; lying West of "Lake Helen-Osteen Road", Except the West 180 feet thereof.

AND EXCEPT that portion of the North 132 feet of the Southeast 1/4 of Section 10, Township 18 South, Range 31 East, Volusia County, Florida, lying West of "Lake Helen-Osteen Road", Except the North 32 feet of the West 180 feet thereof.

NOTE:
THIS PLAT AND/OR SKETCH OF SURVEY IS CERTIFIED TO AND PREPARED FOR THE SOLE AND EXCLUSIVE BENEFIT OF THE ENTITIES AND/OR INDIVIDUALS SHOWN HEREON, ON THE MOST CURRENT DATE SHOWN, AND SHALL NOT BE RELIED UPON BY ANY OTHER ENTITY OR INDIVIDUAL. WHOSOEVER, THERE MAY BE ADDITIONAL RESTRICTIONS AND/OR OTHER MATTERS THAT ARE NOT SHOWN HEREON THAT MAY BE FOUND IN THE PUBLIC RECORDS OF THE COUNTY. THIS SURVEY/SKETCH IS PREPARED WITHOUT BENEFIT OF ABSTRACT OR TITLE SEARCH UNLESS OTHERWISE NOTED. ADDITIONS OR DELETIONS TO SURVEY MAPS OR REPORTS BY OTHER THAN THE SIGNING PARTY OR PARTIES IS PROHIBITED WITHOUT WRITTEN CONSENT OF THE SIGNING PARTY OR PARTIES. THIS SURVEY DRAWING IS THE PROFESSIONAL OPINION OF THIS SURVEYOR AND MAPPER AND THE FIRM, WHICH WAS PREPARED UTILIZING THE BEST AVAILABLE INFORMATION AND AS SUCH DOES NOT CONSTITUTE A GUARANTEE OR WARRANTY, EITHER EXPRESSED OR IMPLIED. FURTHERMORE, THIS SURVEYOR AND FIRM DOES NOT ASSUME RESPONSIBILITY AND SHALL NOT BE HELD LIABLE FOR CLAIMS ARISING FROM ERRONEOUS OR INCORRECT INFORMATION FURNISHED TO THE SURVEYOR, WHICH WAS USED AS A BASIS IN THE PREPARATION OF THIS SURVEY DRAWING.

NOTES:
1. NO INSTRUMENTS OF RECORD REFLECTING EASEMENTS, RIGHT OF WAY AND/OR OWNERSHIP WERE FURNISHED TO THIS SURVEYOR EXCEPT AS SHOWN.
2. NOT VALID WITHOUT THE SIGNATURE AND RAISED SEAL OF A FLORIDA LICENSED SURVEYOR AND MAPPER.
3. NO UNDERGROUND IMPROVEMENTS OR INSTALLATIONS OR OTHER INTERIOR IMPROVEMENTS HAVE BEEN LOCATED, EXCEPT AS SHOWN, AS PER THE REQUEST OF THE CLIENT.
4. UNLESS NOTED, LEGAL DESCRIPTION FURNISHED BY CLIENT.
5. FEATURES SHOWN BY SYMBOL AS INDICATED IN THE LEGEND ARE NOT TO SCALE.
6. THIS SURVEY WAS PERFORMED WITHOUT BENEFIT OF A TITLE SEARCH; A TITLE SEARCH MAY REVEAL ADDITIONAL INFORMATION AFFECTING THE PARCEL, AS SHOWN.
7. WHERE APPLICABLE, MONUMENT DIAMETERS, ETC., AND/OR LS OR LB NUMBERS ARE SHOWN NEAR RESPECTIVE SYMBOL ABOVE, UNLESS SHOWN IN LEGEND.
8. BEARINGS ASSUMED FROM PLAT, DEED, LEGAL DESCRIPTION.
9. UNLESS SHOWN, ONLY THOSE VISIBLE FEATURES IN THE IMMEDIATE VICINITY OF THE ABOVE DESCRIBED PARCEL BOUNDARY HAVE BEEN LOCATED.
10. SUBJECT PROPERTY LIES WITHIN ZONE "X", AS SHOWN ON THE FEDERAL EMERGENCY MANAGEMENT AGENCY FLOOD INSURANCE RATE MAP, CITY OF DELTONA COMMUNITY #120877, PANEL #12127C0830 K DATED SEPTEMBER 28, 2017. THIS FLOOD INSURANCE RATE MAP IS NOT A SURVEY AND NO RESPONSIBILITY IS TAKEN FOR THE ACCURACY OF SAID MAP.

ACREAGE CALCULATIONS
OVERALL PROPERTY 14.43 ACRES
PROPERTY WEST OF ROAD 6.27 ACRES
PROPERTY EAST OF ROAD 8.16 ACRES
EXISTING CHURCH BUILDING 15,683 SQ FT

EFIRD SURVEYING GROUP, INC.

475 S. BLUE LAKE AVENUE
DELAND, FLORIDA 32724
PHONE: (386) 740-4144 FAX: (386) 740-4155
WEBSITE: www.efirdsurveying.com
e-mail: larry@efirdsurveying.com
Certificate Of Authorization Licensed Business Number 7230

Boundary Survey

Survey Date: 8/26/19 Drawing Number: 19-0543 Scale: 1"=60' Drawn By: BE

NEW HOPE BAPTIST CHURCH
OF DELTONA, INC.

I HEREBY CERTIFY THIS SURVEY DRAWING TO BE CORRECT, TO THE BEST OF MY KNOWLEDGE AND BELIEF, AND COME'S IN FORM WITH THE STANDARDS OF PRACTICES SET FORTH BY THE FLORIDA BOARD OF PROFESSIONAL SURVEYORS AND MAPPERS IN CHAPTER 17, F.S. AS PERMANENT TO SECTION 472.027, FLORIDA STATUTES.
LARRY R. EFIRD, JR.
Professional Surveyor & Mapper No. 6823

Appendix B

Approved TIA Methodology





The following proposed development project has an **APPROVED TIA METHODOLOGY**:

Project: New Hope PUD

Date of Approval: February 9, 2024

Date of Expiration*: August 9, 2024

TIA Approval Required By*: February 9, 2025

Conditions:

The respective TIA can now be accepted for review by the county. TIAs must be completed per the River-to-Sea TPO TIA Guidelines, which can be found on the R2CTPO.org website.

Approval Signature: Omar Atallah

TIA SUBMISSION TO COUNTY:

Two steps are required:

- 1) Submit the following items through email to Omar Atallah (Oatallah@volusia.org) and William White (Wdwhite@volusia.org)
 - PDF copy of the complete TIA (TIA needs to include completed TIA checklist)
 - Response to Comments (if resubmitted)
- 2) Due size limitations and computer input file incompatibility issues, send the following directly to VCTE by Mail or Delivery:
 - CD or USB drive containing all computer input files

***REMINDERS:**

- TIA approval needs to be obtained within a year of the approved methodology based on the interpretation of the TPO TIA Guidelines, which state that an approved methodology is valid for up to 6 months and a TIA is valid for up to a year..
- The TIA submitted to support a development plan or use permit cannot be older than one year.
- Advisory: If the applicant waits to submit the TIA or TIA revisions, requested updates to vested trip data, growth rates, traffic count data, etc. are likely to occur. (Example: Applicant submits TIA, receives comments, but doesn't update the TIA and respond to comments until 10 months later.)

Questions about TIAs and TIA methodologies should be addressed to Omar Atallah at Oatallah@volusia.org

MEMORANDUM

To: Ms. Jessica Entwistle – Deltona Planning & Development Services
From: Mr. Chris J. Walsh, P.E.
Date: February 2, 2024
Subject: New Hope PUD – Response to City TIA Methodology Comments
Deltona, Florida

Walsh Traffic Engineering, LLC (Walsh Traffic) has received comments on the November 26, 2023 TIA methodology for the proposed New Hope PUD located on Lake Helen Osteen Road, south of Haulover Boulevard in Deltona, Florida. We offer the following responses:

1) Page 1:

a. For the existing land uses on the east side of Lake Helen Osteen Road, please provide the source for the information stated, for verification of the land use sizes.

Response: The site plan for the existing site shows 15,726 square feet. This is highly comparable to the property appraiser information which shows 15,748 square feet. As for the daycare, they are only licensed/certified to have a maximum of 85 students.

b. It is stated that the “Access to the development (on the east side) is currently provided via two full-access driveways with the northern driveway located approximately 650 feet south of Haulover Boulevard and the southern driveway located approximately 900 feet south of Haulover Boulevard”.

Based on street view of the existing driveways into the property, it is observed that these are entry only (southern driveway) and exit only (northern driveway) driveways. Is it proposed to make these full access driveways (each driveway provides both entry and exit ways) as part of the development? If it is not the case, suggest modifying the description to keep them as entrance and exit only driveways.

Response: It is proposed to convert the southern driveway to full access. The northern driveway will remain as exit only.

c. The southern driveway (entrance only driveway) which is located approximately 900 feet south of Haulover Boulevard has a substandard exclusive right turn lane. It is suggested to improve/provide an exclusive right turn lane in accordance with Volusia County and City of Deltona design requirements.

Response: As conveyed in the methodology, turn lanes at the project driveways will be addressed in the traffic impact analysis.

2) Table 1: To calculate the weekday/daily trip generation for Day Care Center (Land Use Code 565), suggest using the average rate instead of fitted curve since $R^2 < 0.75$ and sample size/number of studies are less than 20. (The R^2 value should be at least 0.75, if using the fitted curve, “because it indicates the recommended acceptable level of correlation between trips generated by a site and the value measured for an independent variable” (ITE Trip Generation Handbook, 3rd edition)).

Please update the trip generation values in the table accordingly.

Response: The daily trip generation for the Day Care Center has been updated as requested.

3) Table 2: For the PM peak hour trip generation calculation for Day Care Center, the pass-by trips should be 19 (In) which is 44% of 43 and 21 (out) which is 44% of 48, instead of 20 (In) and 20 (Out). Please update accordingly.

Response: The trip generation has been updated accordingly.

4) Table 3:

a. The total trips calculated for Church are incorrect. Using the land use code 560 and intensity of 8.30 KSF, using the average rate (because the intensity value is out of data range), the calculated trip ends are calculated to be 63 (total) with 32 (entering) and 31 (exiting).

b. For the Church land use, suggest using average rate for the AM and PM peak hour trip generation. Please modify/update the table accordingly.

Response: The requested modifications have been made.

5) Table 4: For the PM peak hour trip generation calculation for Day Care Center:

a. Why is the pass-by trip percentage 43.3% instead of 44%?

b. The pass-by trips should be 14 (In) which is 44% of 32 and 15 (out) which is 44% of 35, instead of 15 (In) and 14 (Out). Please update the table accordingly.

Response: The trip generation table has been updated based on these comments.

6) Trip Generation: It is assumed that one-fourth of the trips that were shown on Lake Helen Osteen Road between Elkcarn Boulevard and Howland Boulevard will now be diverted to use Elkcarn Boulevard and Howland Boulevard roadways instead. Please justify the detour of 5% on to Elkcarn Boulevard. Is it based on the existing roadway capacities or new modeling effort?

Response: The reassignment consideration has been removed.

7) Study Area: For the intersections to be studied, suggest including Lake Helen Osteen Road and Howland Boulevard intersection, since 17% of the project traffic will end up at the intersection.

Response: The methodology follows the River to Sea TPO's TIA Guidelines' defined significance process for determining the study area. The project impact on Lake Helen Osteen Road is below the three-percent impact threshold. Further, this intersection is not part of the County's critical/near critical list of roadways. The TIA Guidelines were established to provide consistency in the TIA process.

8) Analysis Periods:

Walsh Traffic Engineering

285 Palmetto Springs Street, DeBary, Florida 32713
www.walshtraffic.com

Phone: 386.668.0062



- a. **Please specify the times of data collection for turning movement counts,**
- b. **Please include a queuing analysis for turning movements at study intersections.**

Response: The methodology has been revised to incorporate the two items above.

9) Conceptual Design: Please provide parking requirements and parking spaces provided for the proposed land uses on the east side of Lake Helen Osteen Road.

Response: This is a site plan item that will be addressed within the engineering plans, not within the TIA.

Please let us know if you have any questions.

MEMORANDUM

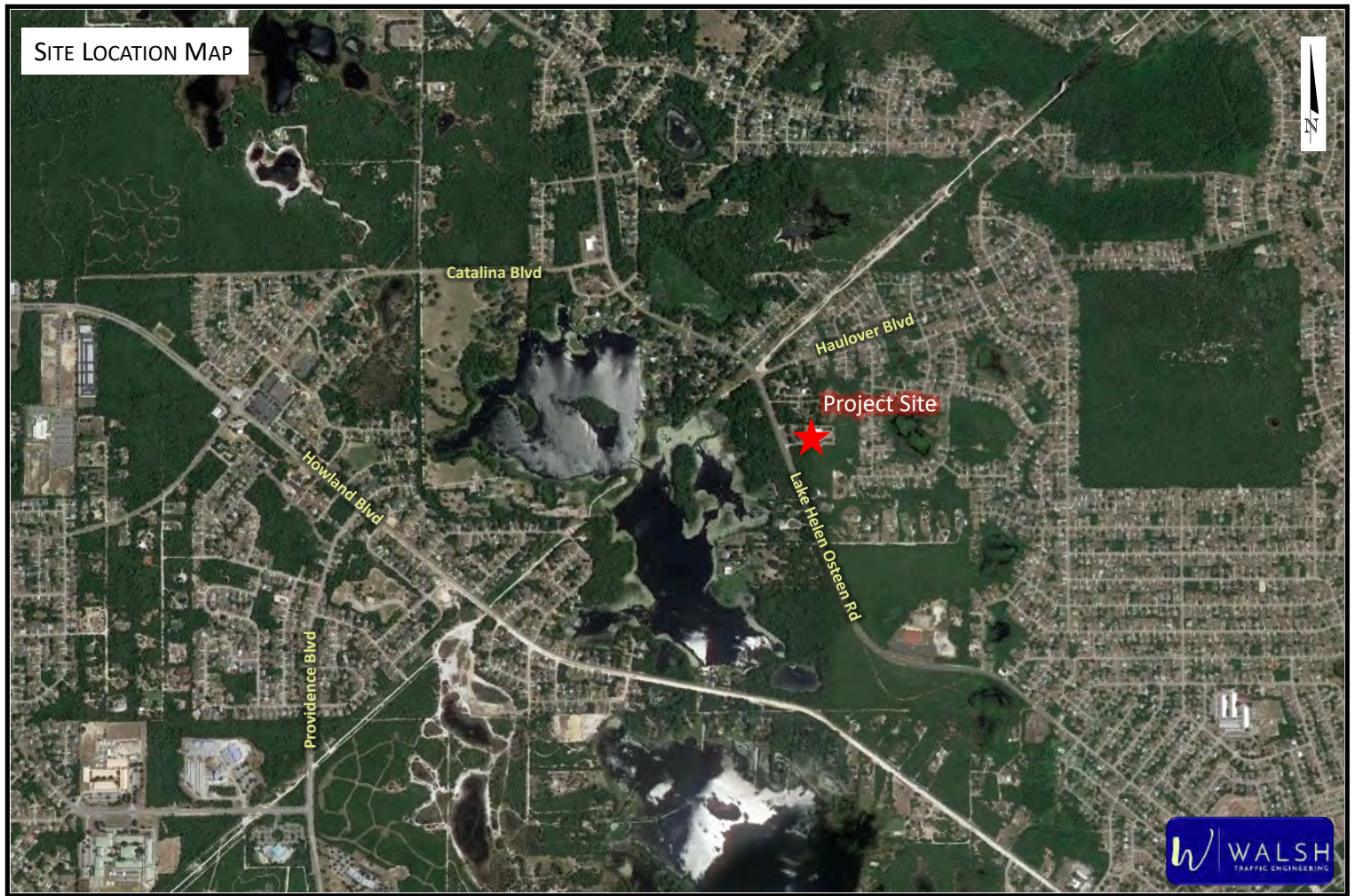
To: Ms. Jessica Entwistle – Deltona Planning & Development Services
From: Mr. Chris J. Walsh, P.E.
Date: February 2, 2024
Subject: New Hope PUD Traffic Impact Analysis Methodology (Revised)
Deltona, Florida

Walsh Traffic Engineering, LLC (Walsh Traffic) has been retained to conduct a traffic impact analysis (TIA) for a proposed New Hope PUD located on Lake Helen Osteen Road, south of Haulover Boulevard in Deltona, Florida (see **Site Location Map**). The subject property straddles both sides of Lake Helen Osteen Road. The property on the west side is vacant. The property on the east side includes a 15,726 square-foot building that serves as a church and can accommodate up to 648 seats. Additionally, this building is used as a daycare facility and is licensed/certified for up to 85 students, operating from 6:30 AM to 6:00 PM with child drop offs/pick-ups occurring continuously throughout the day.

The development is proposed to include the following:

- West side of Lake Helen Osteen Road
 - 120-dwelling unit multi-family development
- East side of Lake Helen Osteen Road
 - 10,000 square-foot daycare building for 115 students
 - 15,000 square-foot community center building
 - 31,291 square-foot church (expansion of the existing church)

Access to the development (on the east side) is currently provided via two driveways with the northern driveway (exit only) located approximately 650 feet south of Haulover Boulevard and the southern driveway (entrance only) located approximately 900 feet south of Haulover Boulevard. Both driveways will be maintained for the eastern portion of the development, however the southern driveway will be converted to bi-directional. The multi-family development on the west side will have a single driveway that aligns with the southern driveway. A copy of the preliminary development plan is attached. The development is proposed to be constructed by year 2029. This memorandum is intended to serve as the methodology for the TIA, prepared in accordance with the River to Sea TPO TIA Guidelines.



Trip Generation

The total daily, AM peak-hour and PM peak-hour trip generation potential for the proposed development is provided below based on trip generation equations/rates provided in the Institute of Transportation Engineer's (ITE) *Trip Generation Manual, 11th Edition*. As summarized below in **Table 1**, the proposed development is projected to generate 1,763 total daily trips, 193 total AM peak-hour trips (97 in, 96 out), and 212 total PM peak-hour trips (101 in, 111 out).

Table 1 – Total Trip Generation Summary (Proposed Development)

| Land Use | ITE Land Use Code | Intensity | Daily | | |
|-----------------------------------|-------------------|--------------|-------------|-----|-------|
| | | | Total Trips | | |
| | | | In | Out | Total |
| Multi-Family (Low-Rise) | 220 | 120 DU | 422 | 423 | 845 |
| Church | 560 | 31.29 KSF | 119 | 119 | 238 |
| Day Care Center | 565 | 115 Students | 228 | 229 | 457 |
| General Office (Community Center) | 710 | 15.0 KSF | 111 | 112 | 223 |
| Total | | | 880 | 883 | 1,763 |

| Land Use | ITE Land Use Code | Intensity | AM Peak Hour | | |
|-----------------------------------|-------------------|--------------|--------------|-----|-------|
| | | | Total Trips | | |
| | | | In | Out | Total |
| Multi-Family (Low-Rise) | 220 | 120 DU | 14 | 46 | 60 |
| Church | 560 | 31.29 KSF | 6 | 4 | 10 |
| Day Care Center | 565 | 115 Students | 48 | 42 | 90 |
| General Office (Community Center) | 710 | 15.0 KSF | 29 | 4 | 33 |
| Total | | | 97 | 96 | 193 |

| Land Use | ITE Land Use Code | Intensity | PM Peak Hour | | |
|-----------------------------------|-------------------|--------------|--------------|-----|-------|
| | | | Total Trips | | |
| | | | In | Out | Total |
| Multi-Family (Low-Rise) | 220 | 120 DU | 45 | 27 | 72 |
| Church | 560 | 31.29 KSF | 7 | 8 | 15 |
| Day Care Center | 565 | 115 Students | 43 | 48 | 91 |
| General Office (Community Center) | 710 | 15.0 KSF | 6 | 28 | 34 |
| Total | | | 101 | 111 | 212 |

ITE provides a PM peak-hour pass-by rate of 44% for the daycare facility (see attachment). The pass-by trips were thus calculated and the resulting new external trips identified. Within the TIA, pass-by trips will be limited to 14% of the future background traffic on the adjacent roadway per the River to Sea TPO's TIA Guidelines. As summarized in **Table 2** below, the proposed development is projected to generate 193 new external AM peak-hour trips (97 in, 96 out) and 172 new external PM peak-hour trips (82 in, 90 out).

Table 2 – New External Trip Generation Summary (Proposed Development)

| Land Use | ITE Land Use Code | Intensity | AM Peak Hour | | | | | | | | | |
|-----------------------------------|-------------------|--------------|--------------|-----|-------|---------------|----|-----|-------|------------------------|-----|-------|
| | | | Total Trips | | | Pass-By Trips | | | | Net New External Trips | | |
| | | | In | Out | Total | % | In | Out | Total | In | Out | Total |
| Multi-Family (Low-Rise) | 220 | 120 DU | 14 | 46 | 60 | 0.0% | 0 | 0 | 0 | 14 | 46 | 60 |
| Church | 560 | 31.29 KSF | 6 | 4 | 10 | 0.0% | 0 | 0 | 0 | 6 | 4 | 10 |
| Day Care Center | 565 | 115 Students | 48 | 42 | 90 | 0.0% | 0 | 0 | 0 | 48 | 42 | 90 |
| General Office (Community Center) | 710 | 15.0 KSF | 29 | 4 | 33 | 0.0% | 0 | 0 | 0 | 29 | 4 | 33 |
| Total | | | 97 | 96 | 193 | 0.0% | 0 | 0 | 0 | 97 | 96 | 193 |

| Land Use | ITE Land Use Code | Intensity | PM Peak Hour | | | | | | | | | |
|-----------------------------------|-------------------|--------------|--------------|-----|-------|---------------|----|-----|-------|------------------------|-----|-------|
| | | | Total Trips | | | Pass-By Trips | | | | Net New External Trips | | |
| | | | In | Out | Total | % | In | Out | Total | In | Out | Total |
| Multi-Family (Low-Rise) | 220 | 120 DU | 45 | 27 | 72 | 0.0% | 0 | 0 | 0 | 45 | 27 | 72 |
| Church | 560 | 31.29 KSF | 7 | 8 | 15 | 0.0% | 0 | 0 | 0 | 7 | 8 | 15 |
| Day Care Center | 565 | 115 Students | 43 | 48 | 91 | 44.0% | 19 | 21 | 40 | 24 | 27 | 51 |
| General Office (Community Center) | 710 | 15.0 KSF | 6 | 28 | 34 | 0.0% | 0 | 0 | 0 | 6 | 28 | 34 |
| Total | | | 101 | 111 | 212 | 18.9% | 19 | 21 | 40 | 82 | 90 | 172 |

Trip generation was then calculated for the existing development on the eastern portion of the subject property. It is important to note that the existing building currently serves as both a church and a day-care facility. For purposes of calculating trip generation, trips were first calculated based on the 85-student daycare facility. Based on the proposed development, a 10,000 square-foot daycare accommodates 115 students. This equates to approximately 87 square feet required per student. Applying this same ratio to the 85 students, it is estimated that approximately 7,395 square feet of the existing building serves as daycare during the weekdays. Thus, the remaining 8,300 square feet of the existing building is used as a church. As summarized on the following page in **Table 3**, the existing development therefore generates 1,195 total daily trips, 69 total AM peak-hour trips (37 in, 32 out) and 71 total PM peak-hour trips (34 in, 37 out).

Similar to the proposed development, pass-by trips were calculated for the existing daycare facility and the resulting new external trips identified. As summarized in **Table 4** on the following page, the proposed development is projected to generate 69 new external AM peak-hour trips (37 in, 32 out) and 42 new external PM peak-hour trips (20 in, 22 out).

Table 3 – Total Trip Generation Summary (Existing Development)

| Land Use | ITE Land Use Code | Intensity | Daily | | |
|-----------------|-------------------|-------------|-------------|-----|-------|
| | | | Total Trips | | |
| | | | In | Out | Total |
| Church | 560 | 8.30 KSF | 32 | 32 | 63 |
| Day Care Center | 565 | 85 Students | 175 | 175 | 350 |
| Total | | | 207 | 207 | 413 |

| Land Use | ITE Land Use Code | Intensity | AM Peak Hour | | |
|-----------------|-------------------|-------------|--------------|-----|-------|
| | | | Total Trips | | |
| | | | In | Out | Total |
| Church | 560 | 8.30 KSF | 2 | 1 | 3 |
| Day Care Center | 565 | 85 Students | 35 | 31 | 66 |
| Total | | | 37 | 32 | 69 |

| Land Use | ITE Land Use Code | Intensity | PM Peak Hour | | |
|-----------------|-------------------|-------------|--------------|-----|-------|
| | | | Total Trips | | |
| | | | In | Out | Total |
| Church | 560 | 8.30 KSF | 2 | 2 | 4 |
| Day Care Center | 565 | 85 Students | 32 | 35 | 67 |
| Total | | | 34 | 37 | 71 |

Table 4 – New External Trip Generation Summary (Existing Development)

| Land Use | ITE Land Use Code | Intensity | AM Peak Hour | | | | | | | | | |
|-----------------|-------------------|-------------|--------------|-----|-------|---------------|----|-----|-------|------------------------|-----|-------|
| | | | Total Trips | | | Pass-By Trips | | | | Net New External Trips | | |
| | | | In | Out | Total | % | In | Out | Total | In | Out | Total |
| Church | 560 | 8.30 KSF | 2 | 1 | 3 | 0.0% | 0 | 0 | 0 | 2 | 1 | 3 |
| Day Care Center | 565 | 85 Students | 35 | 31 | 66 | 0.0% | 0 | 0 | 0 | 35 | 31 | 66 |
| Total | | | 37 | 32 | 69 | 0.0% | 0 | 0 | 0 | 37 | 32 | 69 |

| Land Use | ITE Land Use Code | Intensity | PM Peak Hour | | | | | | | | | |
|-----------------|-------------------|-------------|--------------|-----|-------|---------------|----|-----|------------------------|----|-----|-------|
| | | | Total Trips | | | Pass-By Trips | | | Net New External Trips | | | |
| | | | In | Out | Total | % | In | Out | Total | In | Out | Total |
| Church | 560 | 8.30 KSF | 2 | 2 | 4 | 0.0% | 0 | 0 | 0 | 2 | 2 | 4 |
| Day Care Center | 565 | 85 Students | 32 | 35 | 67 | 44.0% | 14 | 15 | 29 | 18 | 20 | 38 |
| Total | | | 34 | 37 | 71 | 40.8% | 14 | 15 | 29 | 20 | 22 | 42 |

Recognizing that the existing development is vested, the difference between the existing and proposed development was then calculated. As summarized below in **Table 5**, the proposed development modification will increase the AM peak-hour external trips by 124 trips (60 in, 64 out) and the new external PM peak-hour trips by 130 (62 in, 68 out).

Table 5 – New External Trip Generation Increase of Proposed Development

| Land Use | AM Peak Hour | | |
|--|--------------|-----|-------|
| | Total Trips | | |
| | In | Out | Total |
| Proposed Development | 97 | 96 | 193 |
| Existing Development | 37 | 32 | 69 |
| Additonal Trips from Proposed Development | 60 | 64 | 124 |

| Land Use | PM Peak Hour | | |
|--|--------------|-----|-------|
| | Total Trips | | |
| | In | Out | Total |
| Proposed Development | 82 | 90 | 172 |
| Existing Development | 20 | 22 | 42 |
| Additonal Trips from Proposed Development | 62 | 68 | 130 |

Trip Distribution

A TIA was recently prepared by LTG, Inc. in April of 2023 for the proposed development in support of a future land use change and rezoning. The TIA included a model distribution for the development as attached. This model distribution is also proposed for this TIA as it looked reasonable based on engineering judgment. The proposed distribution is attached.

Pass-by trip distribution for day care center will be assessed separately taking into consideration the directional volume of traffic on Lake Helen Osteen Road and the ease of access from each direction of travel.

Study Area

Based on the River to Sea TPO TIA Guidelines, the study area is to include those roadways where the project impact consumes 3% or more of a roadway's two-way peak-hour generalized service volume. **Table 2** below summarizes the significance analysis, based on the net increase of external trips, for purposes of determining the study area. Additionally, the study area is to include any critical/near critical roadway segments located within three miles. The attached critical/near critical map as included in the April 2023 TIA shows the 3-mile radius. It is important to note that the County current critical/near critical map on the County website map is based on 2021 counts. However, the section of Howland Boulevard from Elkcam Boulevard to Providenced Boulevard was recently widened and is thus no longer critical.

Table 2 – Study Area Determination

| Roadway Segment | # of Lanes | Adopted LOS | Peak-Hr 2-Way Service Volume | Project Trips (2-Way) | | | | Critical/Near Critical? | Study Roadway Segment? |
|--|------------|-------------|------------------------------|-----------------------|---------------|---------------|--------------|-------------------------|------------------------|
| | | | | % Assign | Project Trips | % Significant | Significant? | | |
| Lake Helen Osteen Road | | | | | | | | | |
| Howland Blvd to Elkcam Blvd | 2 | E | 1,020 | 20.3% | 26 | 2.55% | no | YES | YES |
| Elkcam Blvd to Project | 2 | E | 1,230 | 38.8% | 50 | 4.07% | YES | YES | YES |
| Project to Haulover Blvd | 2 | E | 1,230 | 61.2% | 80 | 6.50% | YES | YES | YES |
| Haulover Blvd to Catalina Blvd | 2 | E | 1,230 | 55.6% | 72 | 5.85% | YES | no | YES |
| Catalina Blvd to Captain Dr | 2 | E | 1,020 | 22.8% | 30 | 2.94% | no | no | no |
| Catalina Boulevard | | | | | | | | | |
| Eustace Ave to Howland Blvd | 2 | E | 1,230 | 2.9% | 4 | 0.33% | no | no | no |
| Howland Blvd to Lake Helen Osteen Rd | 2 | E | 1,230 | 32.7% | 43 | 3.50% | YES | YES | YES |
| Elkcam Boulevard | | | | | | | | | |
| Howland Blvd to Lake Helen Osteen Rd | 2 | E | 1,230 | 11.9% | 15 | 1.22% | no | no | no |
| Lake Helen-Osteen Rd to Courtland Blvd | 2 | E | 1,230 | 1.5% | 2 | 0.16% | no | no | no |
| Howland Boulevard | | | | | | | | | |
| Providence Blvd to Catalina Blvd | 4 | E | 3,410 | 1.5% | 2 | 0.06% | no | no | no |
| Catalina Blvd to Wolf Pack Run | 4 | E | 3,410 | 27.4% | 36 | 1.06% | no | YES | YES |
| Wolf Pack Run to I-4 | 4 | E | 3,410 | 27.1% | 35 | 1.03% | no | YES | YES |
| Providence Boulevard | | | | | | | | | |
| Fort Smith Blvd to Elkcam Blvd | 2 | E | 1,020 | 6.3% | 8 | 0.78% | no | YES | YES |

The study roadways will include the following:

- Lake Helen Osteen Road – from Howland Blvd to Elkcam Blvd
- Lake Helen Osteen Road – from Elkcam Blvd to Project
- Lake Helen Osteen Road – from Project to Haulover Blvd
- Lake Helen Osteen Road – from Haulover Blvd to Catalina Blvd
- Catalina Boulevard – from Howland Blvd to Lake Helen Osteen Rd
- Howland Boulevard – from Catalina Blvd to Wolf Pack Run
- Howland Boulevard – from Wolf Pack Run to I-4
- Providence Boulevard – from Fort Smith Blvd to Elkcam Blvd

The study intersections include the following:

- Lake Helen Osteen Rd at Elkcam Blvd
- Lake Helen Osteen Rd at Project Driveways
- Lake Helen Osteen Rd at Catalina Blvd
- Catalina Blvd at Howland Blvd

The map on the following page shows the study roadway segments and intersections.

Existing turning movement counts will be obtained from 7:00 to 9:00 AM and 4:00 to 6:00 PM for each of the study intersections. The counts, which will be no older than one year, will also include trucks, bikes, and pedestrians.

Future Volume Traffic Projections

Future background traffic volumes will be estimated in accordance with Volusia County's *Segment Growth Rates and Vested Trips Instruction Policy* (see attachment). Because the existing development is in full operation, the net increase in new external project trips will then be added to the future background peak-hour volumes to develop the future total volume projections.

Analysis Periods

The study roadway segments and intersections will be analyzed under existing conditions and future build-out conditions. In the event a roadway segment or intersection is shown to have unacceptable operations at buildout of the development, future background conditions will also be conducted to determine if deficiencies are triggered by future background traffic volumes.

Roadway segments will be analyzed by comparing the PM peak-hour two-way volumes against each roadway's generalized service volume. In the event that the volumes exceed the generalized service volume, then a more detailed arterial/highway analysis may be conducted using HCM methodologies in accordance with the *FDOT Quality/Level of Service Handbook*. The operating conditions of the study intersections will be analyzed for AM and PM peak-hour conditions using *Synchro 11*, employing *HCM, 6th Edition* methodologies. A queueing summary for each study intersection will also be provided.

Planned Roadway Improvements

Improvements in the study area programmed for construction within the next three years by FDOT, Volusia County, or the City of Deltona will be included in the analyses as committed improvements. Based on information obtained, no improvements are committed for construction within the study area.

Crash Analysis

A five-year crash analysis with a crash summary and crash diagram will be provided for Lake Helen Osteen Road immediately adjacent to the proposed development as well as at each intersection where improvements are recommended under build-out conditions (due to the inclusion of project trips). The crash analysis will seek to identify any crash trends and whether or not any proposed improvements will result in degradation of an existing crash trend. In an effort to avoid unnecessarily burdening the developer, in the event no crash trends are identified, a screen shot of the signal four crash summary will be provided in place of a crash diagram/summary.

Alternative Mode Analysis

An alternative mode analysis will be conducted to evaluate present and programmed bike, pedestrian, and transit mobility options. Planned bicycle and pedestrian connections within the development will be documented. Votran will be notified of the proposed project and appropriate sections of the development review checklist on page 9, Table 2, of the Transit Development Design Guidelines, will be followed. Additionally, an assessment of pedestrian connectivity between the western and eastern portions of the development will be included in the study.

Project Driveway Evaluation

The project driveways on Lake Helen Osteen Road will be evaluated with regard to the need for a right-turn and left-turn lanes. This analysis will be conducted in accordance with requirements in Volusia County's Land Development Code. Should a turn lane be warranted, the study will identify the required turn-lane length in accordance with Volusia County criteria. As a part of this assessment, a queuing analysis will also be provided with regards to the operation of the day care center to better understand if there will be any concerns regarding potential queue spillback onto Lake Helen Osteen Road.

Mitigation

Where roadway segment or intersection deficiencies are identified, appropriate improvements will be identified for existing, future background, and future total build-out conditions. Following, the applicant and the development team will coordinate with the City, and other agencies where applicable, to determine the development's mitigation responsibility. All proposed mitigation improvements must be consistent with the appropriate city and county comprehensive plans transportation element. By way of example, if a proposed improvement is to widen a county roadway beyond that of which is indicated on the county's adopted Future Number of Lanes, the mitigation will consider improvements to a parallel facility. It should be noted that mitigation and associated credits towards impact fees will be addressed in accordance with Florida Statutes 163.3180.



Attachments

| Residential Data | | | | |
|-----------------------|---------------|------------|-------------|------------|
| Description | | | Required | Proposed |
| Lot | | | | |
| Parcel ID | | | | |
| | | | | |
| 811000000080 | 83,199.60 sf | 1.91 Acres | | |
| 811000000041 | 196,020.00 sf | 4.50 Acres | | |
| Lot Area Summary | | | | |
| Gross Lot Area: | 279,220 sf | 6.41 Acres | | |
| | | | | |
| Zonning District | | | | |
| | | | District | |
| Proposed Residential | 279,220 sf | | | PUD |
| | 6.41 Acres | | | |
| Density | | | | |
| Density | 6.41 Acres | | 77 Units | 120 Units |
| | | | 12.00 Du/AC | 0 |
| Building Height | | | | |
| Building Height: | | | | 40'-0" |
| | | | | 0 |
| Building Setbacks | | | | |
| Front Setback (East) | | | 25'-0" | 41'-0" |
| Side Setback (North) | | | 25'-0" | 25'-0" |
| Side Setback (South) | | | 25'-0" | 25'-0" |
| Rear Setback (West) | | | 25'-0" | 56'-0" |
| General Requirements | | | | |
| Floor Area Ratio | | | | 121,486 sf |
| | | | | 43.51% |
| Lot Coverage | | | N/A | 45,500 sf |
| | | | | 16.30% |
| Landscape Open Space: | | | 69,805 sf | 91,783 sf |
| | | | 25 % | 32.87% |
| Total Paved Area | | | N/A | 120,214 sf |
| | | | | 43.05% |
| Sidewalk Area | | | N/A | 21,723 sf |
| | | | | 7.78% |

| Building Area A | | | | | |
|--|---------------|--------------|-----------------|--|---------------------|
| Total Sq Ft. does not include Balcony Sq Ft. | | | | | |
| Levels | Leasable Area | Non-Leasable | | | Total Bldg Gross SF |
| Level 1 | 7,860 sf | 1,247 sf | | | 9,107 sf |
| Level 2 | 7,860 sf | 1,087 sf | | | 8,947 sf |
| Level 3 | 7,860 sf | 1,087 sf | | | 8,947 sf |
| | | | | | |
| Total | 23,580 sf | 3,421 sf | | | 27,001 sf |
| | | | Total of 2 Bldg | | 54,002 sf |
| | | | | | |
| Building Area B | | | | | |
| Total Sq Ft. does not include Balcony Sq Ft. | | | | | |
| Levels | Leasable Area | Non-Leasable | | | Total Bldg Gross SF |
| Level 1 | 9,564 sf | 1,778 sf | | | 11,342 sf |
| Level 2 | 9,564 sf | 1,636 sf | | | 11,200 sf |
| Level 3 | 9,564 sf | 1,636 sf | | | 11,200 sf |
| | | | | | |
| Total | 28,692 sf | 5,050 sf | | | 33,742 sf |
| | | | Total of 2 Bldg | | 67,484 sf |

| Unit Area | | | | | | |
|-----------------|---------|--|---------------|---------------|--------------|-------------|
| | | | | | | |
| | | | Unit A (1 BD) | Unit B (2 BD) | Uni C (3 BD) | Total Units |
| | | | 651 sf | 870 sf | 1,095 sf | |
| | | | | | | |
| | | | | | | |
| Type A | Level 1 | | | 4 Units | 4 Units | 8 Units |
| | Level 2 | | | 4 Units | 4 Units | 8 Units |
| | Level 3 | | | 4 Units | 4 Units | 8 Units |
| Sub Total | | | | 12 Units | 12 Units | 24 Units |
| Total of 2 Bldg | | | | 24 Units | 24 Units | 48 Units |
| | | | | | | |
| Type B | Level 1 | | 4 Units | 8 Units | | 12 Units |
| | Level 2 | | 4 Units | 8 Units | | 12 Units |
| | Level 3 | | 4 Units | 8 Units | | 12 Units |
| Sub Total | | | 12 Units | 24 Units | | 36 Units |
| Total of 2 Bldg | | | 24 Units | 48 Units | | 72 Units |
| | | | | | | |
| | | | | Total Units | | 120 Units |

| Residential Parking Requirement | | | | | | | |
|---------------------------------|------------|-------------------------------------|----------|-----------|---------------|------------|------------|
| | | | | | | Required | Provided |
| | | | | | | | |
| | | | | | | | |
| Unit A (1 BD) | 24 Units | 20.00% | | | 1.5 SP/DU | 36 spaces | |
| Unit B (2 BD) | 72 Units | 60.00% | | | 2.0 SP/DU | 144 spaces | |
| Uni C (3 BD) | 24 Units | 20.00% | | | 2.0 SP/DU | 48 spaces | |
| Total Units | 120 Units | 100.00% | | | | | |
| Visitors | | | | | 1 sp/10 units | 12 spaces | |
| | | | | | Sub Total | 240 spaces | |
| | | | | | | | |
| | | | | | | | |
| | | | | Sub Total | | 240 spaces | |
| | | | | | | | |
| Parking Provided | | | | | | | |
| | | | | | | | |
| Surface | Standard | HC | Parallel | | | | 240 spaces |
| | 233 | 7 | | | | | |
| | | | | | | 240 spaces | 240 spaces |
| | | | | | | | |
| | | | | | | | |
| Bicycle Requirements | | | | | | | |
| Parking Space | 240 spaces | 6 Plus 1 for each 20 Autos over 100 | | | | 10 spaces | 10 spaces |

Vehicle Pass-By Rates by Land Use

Source: ITE *Trip Generation Manual*, 11th Edition

[illegible]

Via Email: (info@tedcbuilds.org)

Ref: 5903.01

TECHNICAL MEMORANDUM

To: Ms. Carol Gardner, Tacolcy Economic Development Corporation

From: Matthew West, AICP

Subject: New Hope PUD – Comprehensive Plan Amendment (CPA) and Rezoning Traffic Impact Analysis (RTIA)
Deltona, FL

Date: April 26, 2023

INTRODUCTION

LTG, Inc. (LTG) has been retained by Tacolcy Economic Development Corporation, to prepare a traffic impact analysis in support of a future land use change and a rezoning for the proposed New Hope PUD. The subject property is located on the east and west sides of Lake Helen Osteen Road, south of Haulover Boulevard, in the City of Deltona, Florida. The land on the west side of Lake Helen Osteen Road is 6.24-acres and is currently vacant. The land on the east side of Lake Helen Osteen Road currently has a 648-seat church and an 85-student capacity day care center. Figure 1 shows the location of the project relative to the surrounding roadway network.

COMPREHENSIVE PLAN AMENDMENT (CPA)

The future land use proposed change for the subject property is from Low Density Residential (LDR) to High Density Residential (HDR) on six (6) acres of the 14.4-acre property. The breakdown of the existing and proposed future land use categories on the subject property, by acreage, and the resultant maximum theoretical development are shown in Table 1 below.

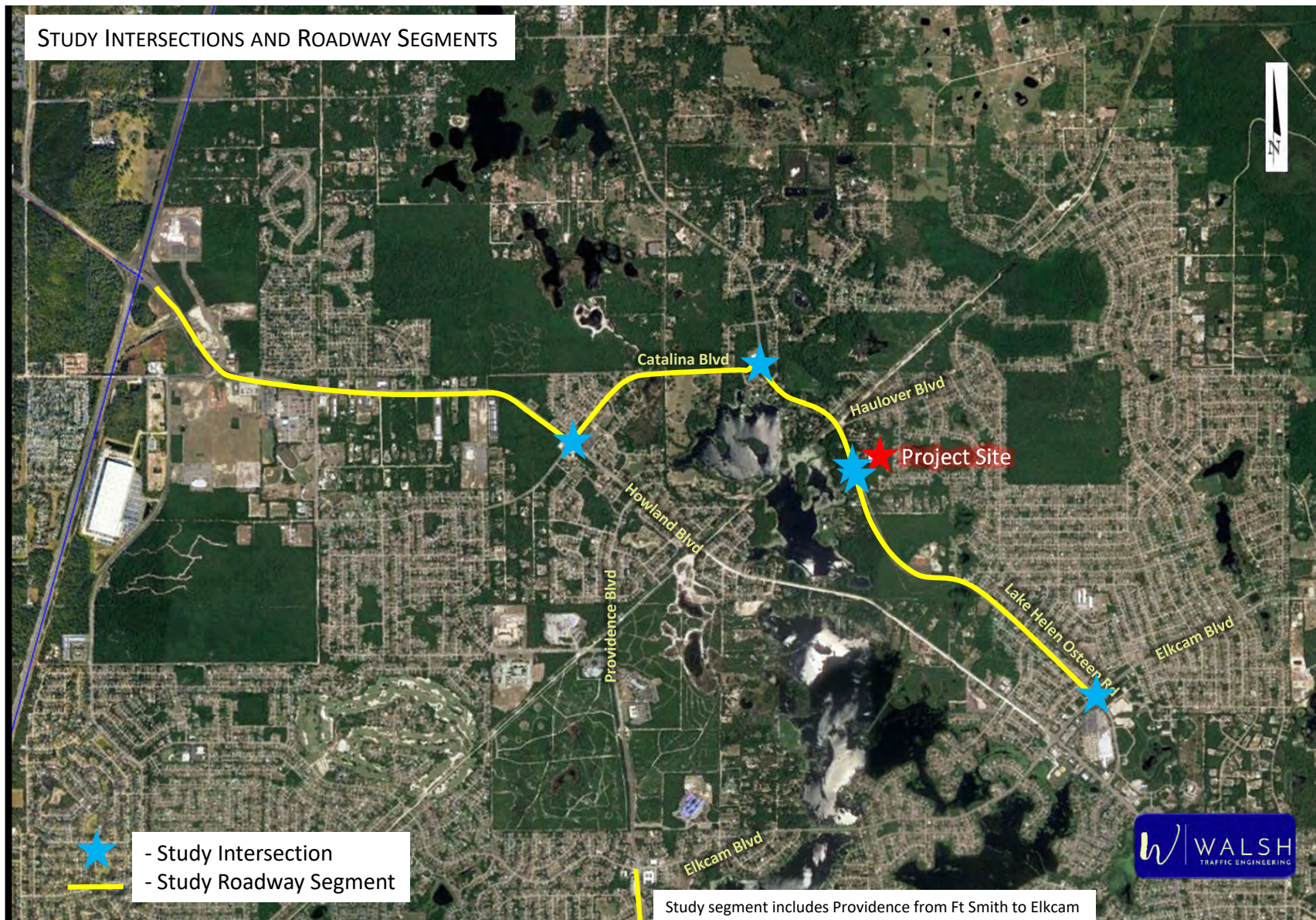
Table 1
Existing and Proposed Future Land Use
New Hope PUD CPA and RTIA

| Condition | FLUM | Land Use | Acreage | Intensity/Density | Resultant Size | Units |
|-----------|------|--------------------------|---------|-------------------------|----------------|-------|
| Existing | LDR | Single-Family | 6.00 | 6 DU/Acre | 36 | DU |
| Proposed | HDR | Multi-Family Low Rise | 6.00 | 20 DU/Acre (limited) | 120 | DU |

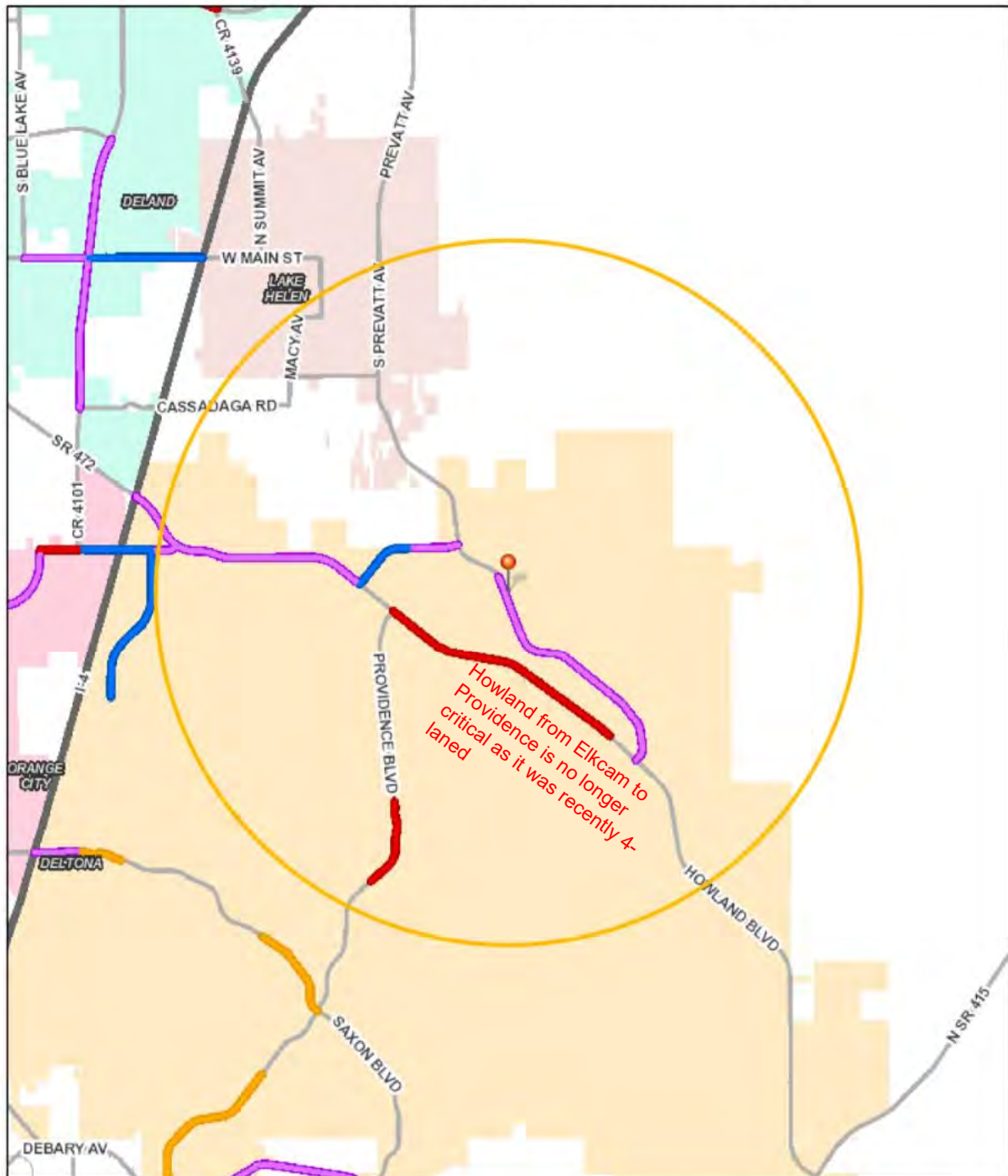
TRIP GENERATION FOR THE EXISTING VS. PROPOSED FLU DESIGNATIONS

The site has an existing future land use designation of LDR, which allows for single-family residential land uses at the density indicated in Table 1. The daily, AM and PM peak-hour trip generation for the existing future land uses were determined using the Institute of Transportation Engineers (ITE) document, *Trip Generation Manual*, 11th Edition and are presented in Table 2, below.

STUDY INTERSECTIONS AND ROADWAY SEGMENTS



Traffic Impact Buffer Map - 3 Mile Radius



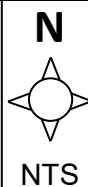
3/27/2023, 10:55:35 AM

Critical and Near Critical
 Critical Vested
 Critical
 Near Critical Vested
 Near Critical

1:72,099
 0 0.5 1 2 mi
 0 1 2 4 km

Note: Map includes all critical and near-critical roadway segments within 3-miles of proposed development.

New Hope PUD



3-Mile Radius
 Critical Map

Project No.: 5903.01

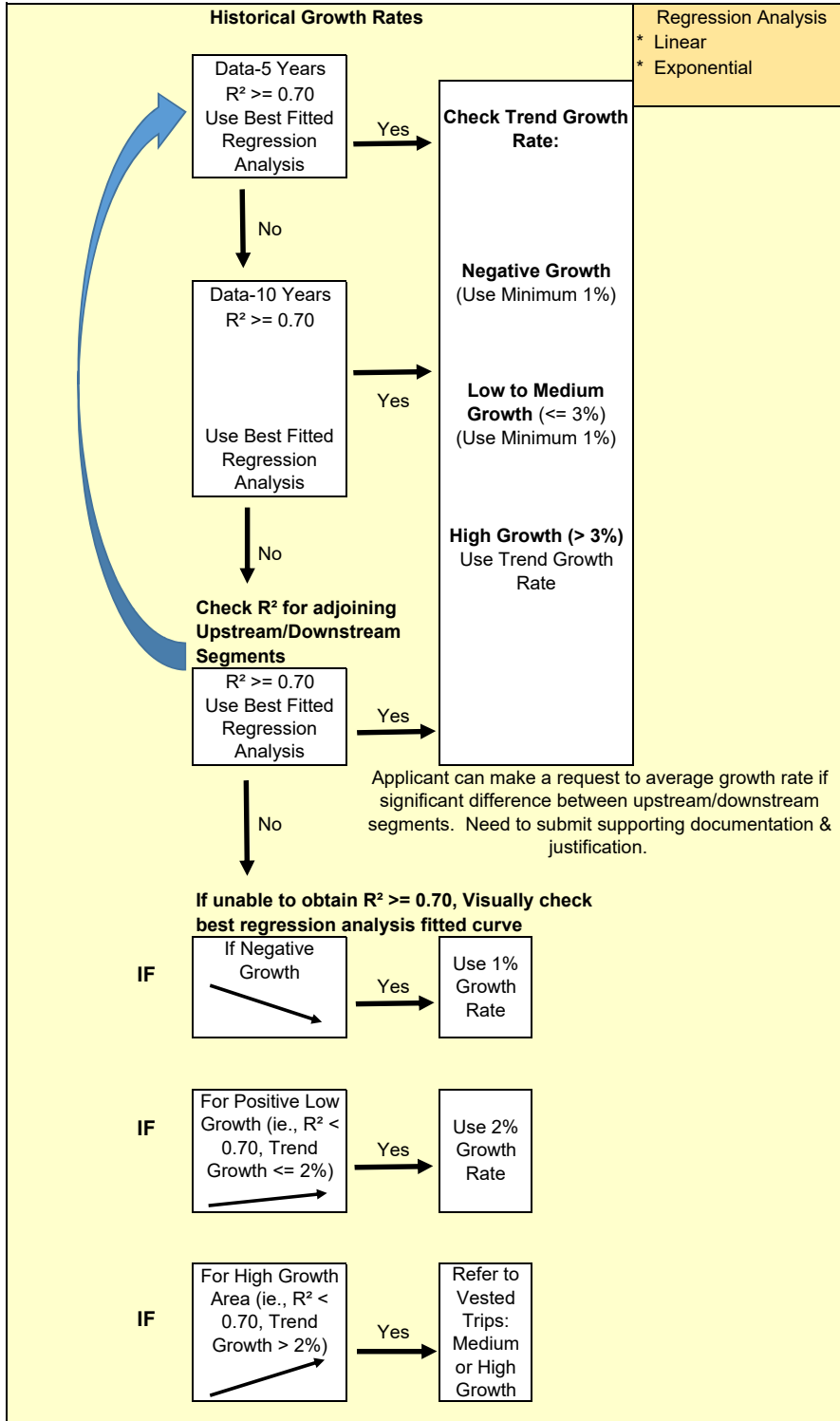
Figure: 2



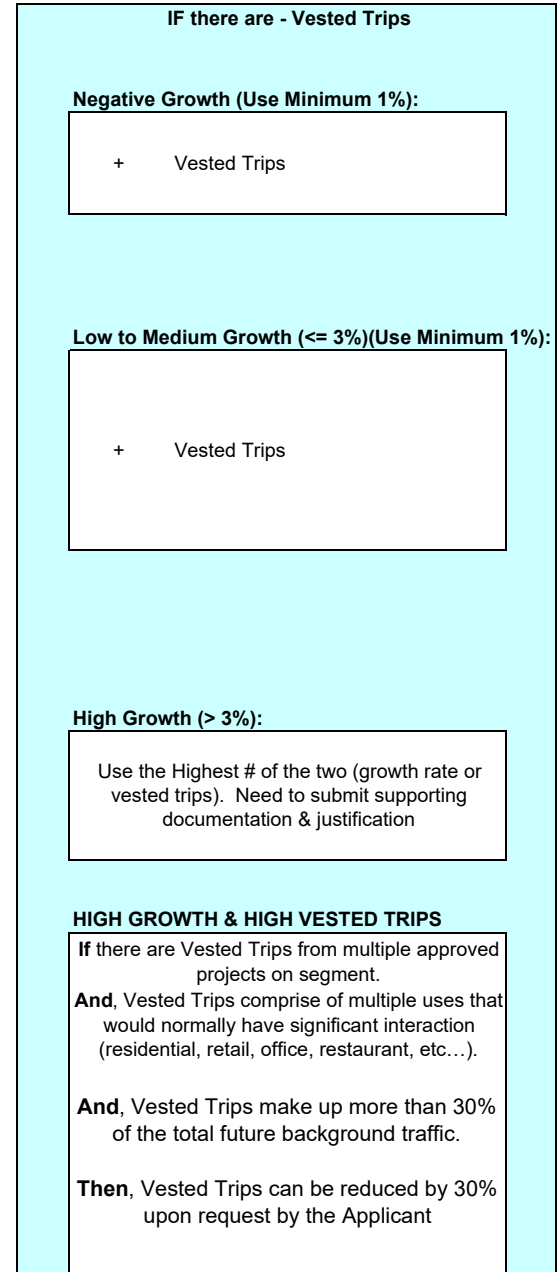
LTG Engineering
 & Planning

1450 W. Granada Blvd., Suite 2, Ormond Beach, Florida 32174
 Telephone: 386.257.2571 Fax: 386.257.6996

Volusia County's Segment Growth Rates and Vested Trips Instructions Policy



AND



Signed: _____
 Jon E. Cheney, P.E.

Date: _____

Appendix C

Traffic Counts



National Data & Surveying Services

Intersection Turning Movement Count

Location: Catalina Blvd & Howland Blvd
City: Deltona
Control: Signalized

Project ID: 24-130025-005
Date: 1/18/2024

Data - Total

| NS/EW Streets: | Catalina Blvd | | | | Catalina Blvd | | | | Howland Blvd | | | | Howland Blvd | | | | |
|------------------|---------------------|---------|---------|---------|---------------|---------|---------|---------|--------------|---------|---------|---------|--------------|---------|---------|---------|-------|
| AM | NORTHBOUND | | | | SOUTHBOUND | | | | EASTBOUND | | | | WESTBOUND | | | | TOTAL |
| | 0 NL | 0 NT | 0 NR | 0 NU | 0 SL | 0 ST | 0 SR | 0 SU | 0 EL | 0 ET | 0 ER | 0 EU | 0 WL | 0 WT | 0 WR | 0 WU | |
| 7:00 AM | 17 | 9 | 5 | 0 | 13 | 12 | 131 | 0 | 23 | 105 | 10 | 0 | 5 | 230 | 16 | 0 | 576 |
| 7:15 AM | 15 | 15 | 7 | 0 | 28 | 13 | 147 | 0 | 28 | 139 | 10 | 0 | 6 | 245 | 23 | 0 | 676 |
| 7:30 AM | 26 | 41 | 7 | 0 | 39 | 31 | 122 | 0 | 16 | 132 | 5 | 0 | 8 | 250 | 23 | 1 | 701 |
| 7:45 AM | 31 | 28 | 9 | 0 | 39 | 35 | 107 | 0 | 41 | 114 | 11 | 0 | 9 | 233 | 20 | 0 | 677 |
| 8:00 AM | 34 | 22 | 11 | 0 | 18 | 18 | 111 | 0 | 31 | 128 | 5 | 0 | 5 | 249 | 9 | 0 | 641 |
| 8:15 AM | 18 | 9 | 11 | 0 | 10 | 14 | 114 | 0 | 34 | 129 | 7 | 0 | 10 | 209 | 10 | 0 | 575 |
| 8:30 AM | 16 | 22 | 8 | 0 | 10 | 18 | 96 | 0 | 50 | 156 | 12 | 0 | 10 | 213 | 5 | 1 | 617 |
| 8:45 AM | 18 | 11 | 5 | 0 | 15 | 18 | 84 | 0 | 29 | 134 | 8 | 0 | 4 | 167 | 5 | 0 | 498 |
| TOTAL VOLUMES : | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| APPROACH %'s : | 175 | 157 | 63 | 0 | 172 | 159 | 912 | 0 | 252 | 1037 | 68 | 0 | 57 | 1796 | 111 | 2 | 4961 |
| | 44.30% | 39.75% | 15.95% | 0.00% | 13.84% | 12.79% | 73.37% | 0.00% | 18.57% | 76.42% | 5.01% | 0.00% | 2.90% | 91.35% | 5.65% | 0.10% | |
| PEAK HR : | 07:15 AM - 08:15 AM | | | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 106 | 106 | 34 | 0 | 124 | 97 | 487 | 0 | 116 | 513 | 31 | 0 | 28 | 977 | 75 | 1 | 2695 |
| PEAK HR FACTOR : | 0.779 | 0.646 | 0.773 | 0.000 | 0.795 | 0.693 | 0.828 | 0.000 | 0.707 | 0.923 | 0.705 | 0.000 | 0.778 | 0.977 | 0.815 | 0.250 | 0.961 |
| | 0.831 | | | | 0.922 | | | | 0.932 | | | | 0.958 | | | | |
| PM | NORTHBOUND | | | | SOUTHBOUND | | | | EASTBOUND | | | | WESTBOUND | | | | TOTAL |
| | 0 NL | 0 NT | 0 NR | 0 NU | 0 SL | 0 ST | 0 SR | 0 SU | 0 EL | 0 ET | 0 ER | 0 EU | 0 WL | 0 WT | 0 WR | 0 WU | |
| 4:00 PM | 16 | 11 | 4 | 0 | 32 | 20 | 51 | 0 | 92 | 261 | 11 | 0 | 10 | 157 | 20 | 2 | 687 |
| 4:15 PM | 15 | 28 | 12 | 0 | 29 | 25 | 67 | 0 | 101 | 255 | 7 | 0 | 11 | 145 | 14 | 0 | 709 |
| 4:30 PM | 17 | 25 | 9 | 0 | 21 | 18 | 61 | 0 | 101 | 229 | 12 | 0 | 10 | 149 | 24 | 2 | 678 |
| 4:45 PM | 12 | 25 | 10 | 0 | 22 | 20 | 69 | 0 | 98 | 258 | 13 | 0 | 11 | 164 | 12 | 0 | 714 |
| 5:00 PM | 11 | 23 | 7 | 0 | 32 | 16 | 44 | 0 | 88 | 277 | 22 | 0 | 10 | 143 | 19 | 0 | 692 |
| 5:15 PM | 10 | 21 | 6 | 0 | 27 | 22 | 59 | 0 | 99 | 271 | 14 | 0 | 14 | 155 | 20 | 2 | 720 |
| 5:30 PM | 9 | 24 | 2 | 0 | 25 | 16 | 75 | 0 | 108 | 265 | 12 | 0 | 15 | 163 | 15 | 0 | 729 |
| 5:45 PM | 15 | 17 | 4 | 0 | 40 | 31 | 60 | 0 | 105 | 276 | 12 | 0 | 4 | 150 | 12 | 0 | 726 |
| TOTAL VOLUMES : | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| APPROACH %'s : | 105 | 174 | 54 | 0 | 228 | 168 | 486 | 0 | 792 | 2092 | 103 | 0 | 85 | 1226 | 136 | 6 | 5655 |
| | 31.53% | 52.25% | 16.22% | 0.00% | 25.85% | 19.05% | 55.10% | 0.00% | 26.51% | 70.04% | 3.45% | 0.00% | 5.85% | 84.38% | 9.36% | 0.41% | |
| PEAK HR : | 05:00 PM - 06:00 PM | | | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 45 | 85 | 19 | 0 | 124 | 85 | 238 | 0 | 400 | 1089 | 60 | 0 | 43 | 611 | 66 | 2 | 2867 |
| PEAK HR FACTOR : | 0.750 | 0.885 | 0.679 | 0.000 | 0.775 | 0.685 | 0.793 | 0.000 | 0.926 | 0.983 | 0.682 | 0.000 | 0.717 | 0.937 | 0.825 | 0.250 | 0.983 |
| | 0.909 | | | | 0.853 | | | | 0.985 | | | | 0.935 | | | | |
| | 1% | 1% | 3% | #DIV/0! | 2% | 0% | 2% | #DIV/0! | 4% | 5% | 3% | #DIV/0! | 0% | 3% | 3% | 0% | |
| | 2% | 0% | 0% | #DIV/0! | 0% | 0% | 3% | #DIV/0! | 1% | 1% | 5% | #DIV/0! | 0% | 1% | 0% | 0% | |

National Data & Surveying Services

Intersection Turning Movement Count

Location: Catalina Blvd & Howland Blvd
City: Deltona
Control: Signalized

Project ID: 24-130025-005
Date: 1/18/2024

Data - Cars

| NS/EW Streets: | Catalina Blvd | | | | Catalina Blvd | | | | Howland Blvd | | | | Howland Blvd | | | | |
|------------------|---------------------|-----------|----------|---------|---------------|-----------|-----------|---------|--------------|-----------|----------|---------|--------------|------------|-----------|---------|---------------|
| AM | NORTHBOUND | | | | SOUTHBOUND | | | | EASTBOUND | | | | WESTBOUND | | | | TOTAL |
| | 0 NL | 0 NT | 0 NR | 0 NU | 0 SL | 0 ST | 0 SR | 0 SU | 0 EL | 0 ET | 0 ER | 0 EU | 0 WL | 0 WT | 0 WR | 0 WU | |
| 7:00 AM | 16 | 8 | 5 | 0 | 13 | 12 | 129 | 0 | 23 | 102 | 9 | 0 | 5 | 229 | 15 | 0 | 566 |
| 7:15 AM | 14 | 14 | 7 | 0 | 27 | 13 | 145 | 0 | 28 | 133 | 9 | 0 | 6 | 240 | 23 | 0 | 659 |
| 7:30 AM | 26 | 41 | 7 | 0 | 38 | 31 | 122 | 0 | 14 | 129 | 5 | 0 | 8 | 242 | 22 | 1 | 686 |
| 7:45 AM | 31 | 28 | 9 | 0 | 39 | 35 | 104 | 0 | 41 | 113 | 11 | 0 | 9 | 230 | 20 | 0 | 670 |
| 8:00 AM | 34 | 22 | 10 | 0 | 18 | 18 | 107 | 0 | 28 | 113 | 5 | 0 | 5 | 239 | 8 | 0 | 607 |
| 8:15 AM | 17 | 9 | 11 | 0 | 10 | 14 | 112 | 0 | 34 | 122 | 6 | 0 | 10 | 202 | 9 | 0 | 556 |
| 8:30 AM | 15 | 20 | 8 | 0 | 10 | 16 | 96 | 0 | 49 | 150 | 12 | 0 | 10 | 205 | 5 | 1 | 597 |
| 8:45 AM | 18 | 11 | 5 | 0 | 15 | 16 | 80 | 0 | 26 | 131 | 8 | 0 | 4 | 165 | 5 | 0 | 484 |
| TOTAL VOLUMES : | NL 171 | NT 153 | NR 62 | NU 0 | SL 170 | ST 155 | SR 895 | SU 0 | EL 243 | ET 993 | ER 65 | EU 0 | WL 57 | WT 1752 | WR 107 | WU 2 | TOTAL 4825 |
| APPROACH %'s : | 44.30% | 39.64% | 16.06% | 0.00% | 13.93% | 12.70% | 73.36% | 0.00% | 18.68% | 76.33% | 5.00% | 0.00% | 2.97% | 91.35% | 5.58% | 0.10% | |
| PEAK HR : | 07:15 AM - 08:15 AM | | | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 105 | 105 | 33 | 0 | 122 | 97 | 478 | 0 | 111 | 488 | 30 | 0 | 28 | 951 | 73 | 1 | 2622 |
| PEAK HR FACTOR : | 0.772 | 0.640 | 0.825 | 0.000 | 0.782 | 0.693 | 0.824 | 0.000 | 0.677 | 0.917 | 0.682 | 0.000 | 0.778 | 0.982 | 0.793 | 0.250 | 0.956 |
| | 0.821 | | | | 0.912 | | | | 0.925 | | | | 0.964 | | | | |

| PM | NORTHBOUND | | | | SOUTHBOUND | | | | EASTBOUND | | | | WESTBOUND | | | | TOTAL |
|------------------|---------------------|-----------|----------|---------|------------|-----------|-----------|---------|-----------|------------|----------|---------|-----------|------------|-----------|---------|---------------|
| | 0 NL | 0 NT | 0 NR | 0 NU | 0 SL | 0 ST | 0 SR | 0 SU | 0 EL | 0 ET | 0 ER | 0 EU | 0 WL | 0 WT | 0 WR | 0 WU | |
| 4:00 PM | 16 | 10 | 4 | 0 | 29 | 20 | 50 | 0 | 88 | 256 | 10 | 0 | 10 | 155 | 19 | 2 | 669 |
| 4:15 PM | 15 | 27 | 12 | 0 | 28 | 25 | 66 | 0 | 101 | 248 | 7 | 0 | 11 | 138 | 13 | 0 | 691 |
| 4:30 PM | 16 | 24 | 9 | 0 | 21 | 18 | 60 | 0 | 101 | 227 | 12 | 0 | 10 | 148 | 24 | 2 | 672 |
| 4:45 PM | 12 | 25 | 10 | 0 | 20 | 19 | 68 | 0 | 94 | 255 | 12 | 0 | 11 | 159 | 11 | 0 | 696 |
| 5:00 PM | 11 | 23 | 7 | 0 | 32 | 16 | 44 | 0 | 88 | 273 | 22 | 0 | 10 | 143 | 19 | 0 | 688 |
| 5:15 PM | 10 | 21 | 6 | 0 | 27 | 22 | 57 | 0 | 96 | 269 | 12 | 0 | 14 | 151 | 20 | 2 | 707 |
| 5:30 PM | 8 | 24 | 2 | 0 | 25 | 16 | 72 | 0 | 106 | 265 | 11 | 0 | 15 | 161 | 15 | 0 | 720 |
| 5:45 PM | 15 | 17 | 4 | 0 | 40 | 31 | 57 | 0 | 105 | 272 | 12 | 0 | 4 | 148 | 12 | 0 | 717 |
| TOTAL VOLUMES : | NL 103 | NT 171 | NR 54 | NU 0 | SL 222 | ST 167 | SR 474 | SU 0 | EL 779 | ET 2065 | ER 98 | EU 0 | WL 85 | WT 1203 | WR 133 | WU 6 | TOTAL 5560 |
| APPROACH %'s : | 31.40% | 52.13% | 16.46% | 0.00% | 25.72% | 19.35% | 54.92% | 0.00% | 26.48% | 70.19% | 3.33% | 0.00% | 5.96% | 84.30% | 9.32% | 0.42% | |
| PEAK HR : | 05:00 PM - 06:00 PM | | | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 44 | 85 | 19 | 0 | 124 | 85 | 230 | 0 | 395 | 1079 | 57 | 0 | 43 | 603 | 66 | 2 | 2832 |
| PEAK HR FACTOR : | 0.733 | 0.885 | 0.679 | 0.000 | 0.775 | 0.685 | 0.799 | 0.000 | 0.932 | 0.988 | 0.648 | 0.000 | 0.717 | 0.936 | 0.825 | 0.250 | 0.983 |
| | 0.902 | | | | 0.857 | | | | 0.984 | | | | 0.935 | | | | |

National Data & Surveying Services

Intersection Turning Movement Count

Location: Catalina Blvd & Howland Blvd
City: Deltona
Control: Signalized

Project ID: 24-130025-005
Date: 1/18/2024

Data - HT

| NS/EW Streets: | Catalina Blvd | | | | Catalina Blvd | | | | Howland Blvd | | | | Howland Blvd | | | | |
|------------------|---------------------|---------|---------|---------|---------------|---------|---------|---------|--------------|---------|---------|---------|--------------|---------|---------|---------|-------|
| AM | NORTHBOUND | | | | SOUTHBOUND | | | | EASTBOUND | | | | WESTBOUND | | | | TOTAL |
| | 0 NL | 0 NT | 0 NR | 0 NU | 0 SL | 0 ST | 0 SR | 0 SU | 0 EL | 0 ET | 0 ER | 0 EU | 0 WL | 0 WT | 0 WR | 0 WU | |
| 7:00 AM | 1 | 1 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 3 | 1 | 0 | 0 | 1 | 1 | 0 | 10 |
| 7:15 AM | 1 | 1 | 0 | 0 | 1 | 0 | 2 | 0 | 0 | 6 | 1 | 0 | 0 | 5 | 0 | 0 | 17 |
| 7:30 AM | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 2 | 3 | 0 | 0 | 0 | 8 | 1 | 0 | 15 |
| 7:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 1 | 0 | 0 | 0 | 3 | 0 | 0 | 7 |
| 8:00 AM | 0 | 0 | 1 | 0 | 0 | 0 | 4 | 0 | 3 | 15 | 0 | 0 | 0 | 10 | 1 | 0 | 34 |
| 8:15 AM | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 7 | 1 | 0 | 0 | 7 | 1 | 0 | 19 |
| 8:30 AM | 1 | 2 | 0 | 0 | 0 | 2 | 0 | 0 | 1 | 6 | 0 | 0 | 0 | 8 | 0 | 0 | 20 |
| 8:45 AM | 0 | 0 | 0 | 0 | 0 | 2 | 4 | 0 | 3 | 3 | 0 | 0 | 0 | 2 | 0 | 0 | 14 |
| TOTAL VOLUMES : | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| APPROACH %'s : | 4 | 4 | 1 | 0 | 2 | 4 | 17 | 0 | 9 | 44 | 3 | 0 | 0 | 44 | 4 | 0 | 136 |
| | 44.44% | 44.44% | 11.11% | 0.00% | 8.70% | 17.39% | 73.91% | 0.00% | 16.07% | 78.57% | 5.36% | 0.00% | 0.00% | 91.67% | 8.33% | 0.00% | |
| PEAK HR : | 07:15 AM - 08:15 AM | | | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 1 | 1 | 1 | 0 | 2 | 0 | 9 | 0 | 5 | 25 | 1 | 0 | 0 | 26 | 2 | 0 | 73 |
| PEAK HR FACTOR : | 0.250 | 0.250 | 0.250 | 0.000 | 0.500 | 0.000 | 0.563 | 0.000 | 0.417 | 0.417 | 0.250 | 0.000 | 0.000 | 0.650 | 0.500 | 0.000 | 0.537 |
| | 0.375 | | | | 0.688 | | | | 0.431 | | | | 0.636 | | | | |
| PM | NORTHBOUND | | | | SOUTHBOUND | | | | EASTBOUND | | | | WESTBOUND | | | | TOTAL |
| | 0 NL | 0 NT | 0 NR | 0 NU | 0 SL | 0 ST | 0 SR | 0 SU | 0 EL | 0 ET | 0 ER | 0 EU | 0 WL | 0 WT | 0 WR | 0 WU | |
| 4:00 PM | 0 | 1 | 0 | 0 | 3 | 0 | 1 | 0 | 4 | 5 | 1 | 0 | 0 | 2 | 1 | 0 | 18 |
| 4:15 PM | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 7 | 0 | 0 | 0 | 7 | 1 | 0 | 18 |
| 4:30 PM | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 2 | 0 | 0 | 0 | 1 | 0 | 0 | 6 |
| 4:45 PM | 0 | 0 | 0 | 0 | 2 | 1 | 1 | 0 | 4 | 3 | 1 | 0 | 0 | 5 | 1 | 0 | 18 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 3 | 2 | 2 | 0 | 0 | 4 | 0 | 0 | 13 |
| 5:30 PM | 1 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 2 | 0 | 1 | 0 | 0 | 2 | 0 | 0 | 9 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 4 | 0 | 0 | 0 | 2 | 0 | 0 | 9 |
| TOTAL VOLUMES : | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| APPROACH %'s : | 2 | 3 | 0 | 0 | 6 | 1 | 12 | 0 | 13 | 27 | 5 | 0 | 0 | 23 | 3 | 0 | 95 |
| | 40.00% | 60.00% | 0.00% | 0.00% | 31.58% | 5.26% | 63.16% | 0.00% | 28.89% | 60.00% | 11.11% | 0.00% | 0.00% | 88.46% | 11.54% | 0.00% | |
| PEAK HR : | 05:00 PM - 06:00 PM | | | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 1 | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 5 | 10 | 3 | 0 | 0 | 8 | 0 | 0 | 35 |
| PEAK HR FACTOR : | 0.250 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.667 | 0.000 | 0.417 | 0.625 | 0.375 | 0.000 | 0.000 | 0.500 | 0.000 | 0.000 | 0.673 |
| | 0.250 | | | | 0.667 | | | | 0.643 | | | | 0.500 | | | | |

National Data & Surveying Services

Intersection Turning Movement Count

Location: Catalina Blvd & Howland Blvd
City: Deltona
Control: Signalized

Project ID: 24-130025-005
Date: 1/18/2024

Data - Bikes

| NS/EW Streets: | Catalina Blvd | | | | Catalina Blvd | | | | Howland Blvd | | | | Howland Blvd | | | | |
|------------------|---------------------|---------|---------|---------|---------------|---------|---------|---------|--------------|---------|---------|---------|--------------|---------|---------|---------|-------|
| AM | NORTHBOUND | | | | SOUTHBOUND | | | | EASTBOUND | | | | WESTBOUND | | | | TOTAL |
| | 0 NL | 0 NT | 0 NR | 0 NU | 0 SL | 0 ST | 0 SR | 0 SU | 0 EL | 0 ET | 0 ER | 0 EU | 0 WL | 0 WT | 0 WR | 0 WU | |
| 7:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 |
| 8:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| TOTAL VOLUMES : | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| APPROACH %'s : | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 2 |
| | | | | | 0.00% | 0.00% | 100.00% | 0.00% | | | | | 0.00% | 100.00% | 0.00% | 0.00% | |
| PEAK HR : | 07:15 AM - 08:15 AM | | | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 |
| PEAK HR FACTOR : | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.250 | 0.000 | 0.000 | 0.250 |

| PM | NORTHBOUND | | | | SOUTHBOUND | | | | EASTBOUND | | | | WESTBOUND | | | | TOTAL |
|------------------|---------------------|---------|---------|---------|------------|---------|---------|---------|-----------|---------|---------|---------|-----------|---------|---------|---------|-------|
| | 0 NL | 0 NT | 0 NR | 0 NU | 0 SL | 0 ST | 0 SR | 0 SU | 0 EL | 0 ET | 0 ER | 0 EU | 0 WL | 0 WT | 0 WR | 0 WU | |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 5:30 PM | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 |
| TOTAL VOLUMES : | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| APPROACH %'s : | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 1 | 0 | 6 |
| | 0.00% | 100.00% | 0.00% | 0.00% | | | | | 0.00% | 100.00% | 0.00% | 0.00% | 0.00% | 0.00% | 100.00% | 0.00% | |
| PEAK HR : | 05:00 PM - 06:00 PM | | | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 1 | 0 | 5 |
| PEAK HR FACTOR : | 0.000 | 0.250 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.750 | 0.000 | 0.000 | 0.000 | 0.000 | 0.250 | 0.000 | 0.625 |

National Data & Surveying Services

Intersection Turning Movement Count

Location: Catalina Blvd & Howland Blvd
City: Deltona

Project ID: 24-130025-005
Date: 1/18/2024

Data - Pedestrians (Crosswalks)

| NS/EW Streets: | Catalina Blvd | | Catalina Blvd | | Howland Blvd | | Howland Blvd | | |
|------------------|---------------------|---------|---------------|----|--------------|----|--------------|----|-------|
| AM | NORTH LEG | | SOUTH LEG | | EAST LEG | | WEST LEG | | TOTAL |
| | EB | WB | EB | WB | NB | SB | NB | SB | |
| 7:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 AM | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 8:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| TOTAL VOLUMES : | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| APPROACH %'s : | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| | 0.00% | 100.00% | | | | | | | |
| PEAK HR : | 07:15 AM - 08:15 AM | | | | | | | | TOTAL |
| PEAK HR VOL : | 0 | 1 | | | | | | | 1 |
| PEAK HR FACTOR : | | 0.250 | 0 | 0 | 0 | 0 | 0 | 0 | 0.250 |
| | | 0.250 | | | | | | | |

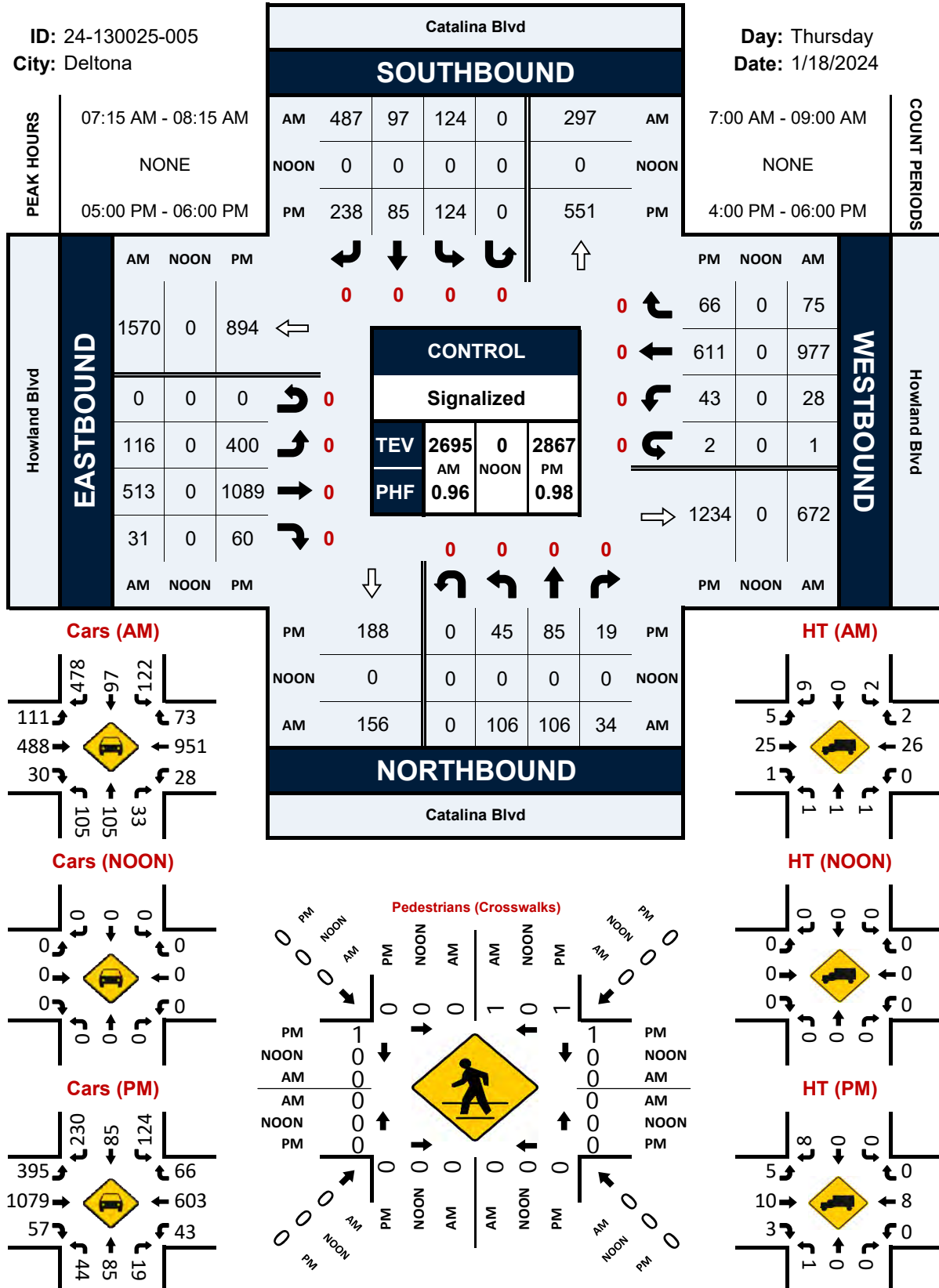
| PM | NORTH LEG | | SOUTH LEG | | EAST LEG | | WEST LEG | | TOTAL |
|------------------|---------------------|--------|-----------|-------|----------|--------|----------|---------|-------|
| | EB | WB | EB | WB | NB | SB | NB | SB | |
| 4:00 PM | 3 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 4 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 2 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 3 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| TOTAL VOLUMES : | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| APPROACH %'s : | 3 | 1 | 1 | 0 | 2 | 1 | 0 | 1 | 9 |
| | 75.00% | 25.00% | 100.00% | 0.00% | 66.67% | 33.33% | 0.00% | 100.00% | |
| PEAK HR : | 05:00 PM - 06:00 PM | | | | | | | | TOTAL |
| PEAK HR VOL : | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 3 |
| PEAK HR FACTOR : | | 0.250 | | | | 0.250 | | 0.250 | 0.250 |
| | | 0.250 | | | 0.250 | | 0.250 | | |

Catalina Blvd & Howland Blvd

Peak Hour Turning Movement Count

ID: 24-130025-005
City: Deltona

Day: Thursday
Date: 1/18/2024



PROJECT ID: 24-130025-005
DATE: Thu, Jan 18, 2024

[illegible]

PROJECT ID: 24-130025-005
DATE: Thu, Jan 18, 2024



| 15-Min Count Period Beginning At | Catalina Blvd Northbound | | | | | Catalina Blvd Southbound | | | | | Howland Blvd Eastbound | | | | | Howland Blvd Westbound | | | | | Total | Hourly Total |
|--|-----------------------------|------|-----|---|----|-----------------------------|------|-----|---|----|---------------------------|------|-----|---|----|---------------------------|------|-----|---|----|-------|-----------------|
| | Left | Thru | Rgt | U | R* | Left | Thru | Rgt | U | R* | Left | Thru | Rgt | U | R* | Left | Thru | Rgt | U | R* | | |
| 4:00 PM | 16 | 11 | 4 | 0 | | 32 | 20 | 51 | 0 | | 92 | 261 | 11 | 0 | | 10 | 157 | 20 | 2 | | 687 | 2788 |
| 4:15 PM | 15 | 28 | 12 | 0 | | 29 | 25 | 67 | 0 | | 101 | 255 | 7 | 0 | | 11 | 145 | 14 | 0 | | 709 | 2793 |
| 4:30 PM | 17 | 25 | 9 | 0 | | 21 | 18 | 61 | 0 | | 101 | 229 | 12 | 0 | | 10 | 149 | 24 | 2 | | 678 | 2804 |
| 4:45 PM | 12 | 25 | 10 | 0 | | 22 | 20 | 69 | 0 | | 98 | 258 | 13 | 0 | | 11 | 164 | 12 | 0 | | 714 | 2855 |
| 5:00 PM | 11 | 23 | 7 | 0 | | 32 | 16 | 44 | 0 | | 88 | 277 | 22 | 0 | | 10 | 143 | 19 | 0 | | 692 | 2867 |
| 5:15 PM | 10 | 21 | 6 | 0 | | 27 | 22 | 59 | 0 | | 99 | 271 | 14 | 0 | | 14 | 155 | 20 | 2 | | 720 | 2175 |
| 5:30 PM | 9 | 24 | 2 | 0 | | 25 | 16 | 75 | 0 | | 108 | 265 | 12 | 0 | | 15 | 163 | 15 | 0 | | 729 | 1455 |
| 5:45 PM | 15 | 17 | 4 | 0 | | 40 | 31 | 60 | 0 | | 105 | 276 | 12 | 0 | | 4 | 150 | 12 | 0 | | 726 | 726 |
| Peak 15-Min Flowrates | Northbound | | | | | Southbound | | | | | Eastbound | | | | | Westbound | | | | | Total | |
| | Left | Thru | Rgt | U | R* | Left | Thru | Rgt | U | R* | Left | Thru | Rgt | U | R* | Left | Thru | Rgt | U | R* | | |
| All Vehicles | 60 | 96 | 28 | 0 | | 160 | 124 | 300 | 0 | | 432 | 1108 | 88 | 0 | | 60 | 652 | 80 | 0 | | 3196 | |
| Heavy Trucks | 4 | 0 | 0 | 0 | | 0 | 0 | 12 | 0 | | 12 | 16 | 8 | 0 | | 0 | 16 | 0 | 0 | | 68 | |
| Pedestrians | | 0 | | | | | | 4 | | | | 4 | | | | | 4 | | | | 12 | |
| Bicycles | 0 | 4 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 4 | 0 | 0 | | 0 | 0 | 4 | 0 | | 12 | |
| Buses | | | | | | | | | | | | | | | | | | | | | | |
| Stopped Buses | | | | | | | | | | | | | | | | | | | | | | |

National Data & Surveying Services

Intersection Turning Movement Count

Location: Lake Helen Osteen Rd & Catalina Blvd
City: Deltona
Control: Signalized

Project ID: 24-130025-004
Date: 1/18/2024

Data - Total

| NS/EW Streets: | Lake Helen Osteen Rd | | | | Lake Helen Osteen Rd | | | | Catalina Blvd | | | | Catalina Blvd | | | | |
|------------------|----------------------|---------|---------|---------|----------------------|---------|---------|---------|---------------|---------|---------|---------|---------------|---------|---------|---------|-------|
| AM | NORTHBOUND | | | | SOUTHBOUND | | | | EASTBOUND | | | | WESTBOUND | | | | TOTAL |
| | 0 NL | 0 NT | 0 NR | 0 NU | 0 SL | 0 ST | 0 SR | 0 SU | 0 EL | 0 ET | 0 ER | 0 EU | 0 WL | 0 WT | 0 WR | 0 WU | |
| 7:00 AM | 107 | 81 | 0 | 0 | 0 | 33 | 37 | 0 | 14 | 0 | 16 | 0 | 0 | 0 | 0 | 0 | 288 |
| 7:15 AM | 116 | 109 | 0 | 0 | 0 | 34 | 42 | 0 | 11 | 0 | 28 | 0 | 0 | 0 | 0 | 0 | 340 |
| 7:30 AM | 106 | 113 | 0 | 0 | 0 | 51 | 53 | 0 | 19 | 0 | 26 | 0 | 0 | 0 | 0 | 0 | 368 |
| 7:45 AM | 89 | 81 | 0 | 0 | 0 | 81 | 47 | 0 | 10 | 0 | 37 | 0 | 0 | 0 | 0 | 0 | 345 |
| 8:00 AM | 69 | 61 | 0 | 0 | 0 | 29 | 40 | 0 | 18 | 0 | 40 | 0 | 0 | 0 | 0 | 0 | 257 |
| 8:15 AM | 80 | 48 | 0 | 0 | 0 | 33 | 42 | 0 | 13 | 0 | 38 | 0 | 0 | 0 | 0 | 0 | 254 |
| 8:30 AM | 65 | 53 | 0 | 0 | 0 | 28 | 25 | 0 | 25 | 0 | 36 | 0 | 0 | 0 | 0 | 0 | 232 |
| 8:45 AM | 65 | 39 | 0 | 0 | 0 | 29 | 30 | 0 | 10 | 0 | 29 | 0 | 0 | 0 | 0 | 0 | 202 |
| TOTAL VOLUMES : | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| APPROACH %'s : | 697 | 585 | 0 | 0 | 0 | 318 | 316 | 0 | 120 | 0 | 250 | 0 | 0 | 0 | 0 | 0 | 2286 |
| | 54.37% | 45.63% | 0.00% | 0.00% | 0.00% | 50.16% | 49.84% | 0.00% | 32.43% | 0.00% | 67.57% | 0.00% | 0 | 0 | 0 | 0 | |
| PEAK HR : | 07:00 AM - 08:00 AM | | | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 418 | 384 | 0 | 0 | 0 | 199 | 179 | 0 | 54 | 0 | 107 | 0 | 0 | 0 | 0 | 0 | 1341 |
| PEAK HR FACTOR : | 0.901 | 0.850 | 0.000 | 0.000 | 0.000 | 0.614 | 0.844 | 0.000 | 0.711 | 0.000 | 0.723 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.911 |
| | 0.891 | | | | 0.738 | | | | 0.856 | | | | | | | | |
| PM | NORTHBOUND | | | | SOUTHBOUND | | | | EASTBOUND | | | | WESTBOUND | | | | TOTAL |
| | 0 NL | 0 NT | 0 NR | 0 NU | 0 SL | 0 ST | 0 SR | 0 SU | 0 EL | 0 ET | 0 ER | 0 EU | 0 WL | 0 WT | 0 WR | 0 WU | |
| 4:00 PM | 56 | 46 | 0 | 0 | 0 | 58 | 23 | 0 | 25 | 0 | 68 | 0 | 0 | 0 | 0 | 0 | 276 |
| 4:15 PM | 57 | 41 | 0 | 0 | 0 | 85 | 25 | 0 | 43 | 0 | 86 | 0 | 0 | 0 | 0 | 0 | 337 |
| 4:30 PM | 44 | 50 | 0 | 0 | 0 | 62 | 22 | 0 | 28 | 0 | 89 | 0 | 0 | 0 | 0 | 0 | 295 |
| 4:45 PM | 48 | 40 | 0 | 0 | 0 | 81 | 24 | 0 | 29 | 0 | 76 | 0 | 0 | 0 | 0 | 0 | 298 |
| 5:00 PM | 43 | 44 | 0 | 0 | 0 | 73 | 20 | 0 | 46 | 0 | 76 | 0 | 0 | 0 | 0 | 0 | 302 |
| 5:15 PM | 51 | 38 | 0 | 0 | 0 | 111 | 23 | 0 | 34 | 0 | 97 | 0 | 0 | 0 | 0 | 0 | 354 |
| 5:30 PM | 42 | 45 | 0 | 0 | 0 | 93 | 24 | 0 | 37 | 0 | 84 | 0 | 0 | 0 | 0 | 0 | 325 |
| 5:45 PM | 59 | 39 | 0 | 0 | 0 | 78 | 26 | 0 | 52 | 0 | 79 | 0 | 0 | 0 | 0 | 0 | 333 |
| TOTAL VOLUMES : | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| APPROACH %'s : | 400 | 343 | 0 | 0 | 0 | 641 | 187 | 0 | 294 | 0 | 655 | 0 | 0 | 0 | 0 | 0 | 2520 |
| | 53.84% | 46.16% | 0.00% | 0.00% | 0.00% | 77.42% | 22.58% | 0.00% | 30.98% | 0.00% | 69.02% | 0.00% | 0 | 0 | 0 | 0 | |
| PEAK HR : | 05:00 PM - 06:00 PM | | | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 195 | 166 | 0 | 0 | 0 | 355 | 93 | 0 | 169 | 0 | 336 | 0 | 0 | 0 | 0 | 0 | 1314 |
| PEAK HR FACTOR : | 0.826 | 0.922 | 0.000 | 0.000 | 0.000 | 0.800 | 0.894 | 0.000 | 0.813 | 0.000 | 0.866 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.928 |
| | 0.921 | | | | 0.836 | | | | 0.964 | | | | | | | | |

1% 3% #DIV/0! #DIV/0! #DIV/0! 5% 1% #DIV/0! 0% #DIV/0! 3% #DIV/0! #DIV/0! #DIV/0! #DIV/0! #DIV/0!
5% 2% #DIV/0! #DIV/0! #DIV/0! 3% 4% #DIV/0! 1% #DIV/0! 2% #DIV/0! #DIV/0! #DIV/0! #DIV/0! #DIV/0!

National Data & Surveying Services

Intersection Turning Movement Count

Location: Lake Helen Osteen Rd & Catalina Blvd
City: Deltona
Control: Signalized

Project ID: 24-130025-004
Date: 1/18/2024

Data - Cars

| NS/EW Streets: | Lake Helen Osteen Rd | | | | Lake Helen Osteen Rd | | | | Catalina Blvd | | | | Catalina Blvd | | | | |
|-----------------------------------|----------------------|---------------------|------------------|------------------|----------------------|---------------------|---------------------|------------------|---------------------|------------------|---------------------|------------------|------------------|------------------|------------------|------------------|---------------|
| AM | NORTHBOUND | | | | SOUTHBOUND | | | | EASTBOUND | | | | WESTBOUND | | | | TOTAL |
| | 0 NL | 0 NT | 0 NR | 0 NU | 0 SL | 0 ST | 0 SR | 0 SU | 0 EL | 0 ET | 0 ER | 0 EU | 0 WL | 0 WT | 0 WR | 0 WU | |
| 7:00 AM | 107 | 80 | 0 | 0 | 0 | 31 | 37 | 0 | 14 | 0 | 15 | 0 | 0 | 0 | 0 | 0 | 284 |
| 7:15 AM | 114 | 106 | 0 | 0 | 0 | 31 | 42 | 0 | 11 | 0 | 28 | 0 | 0 | 0 | 0 | 0 | 332 |
| 7:30 AM | 105 | 110 | 0 | 0 | 0 | 49 | 52 | 0 | 19 | 0 | 25 | 0 | 0 | 0 | 0 | 0 | 360 |
| 7:45 AM | 88 | 76 | 0 | 0 | 0 | 78 | 46 | 0 | 10 | 0 | 36 | 0 | 0 | 0 | 0 | 0 | 334 |
| 8:00 AM | 67 | 59 | 0 | 0 | 0 | 28 | 40 | 0 | 18 | 0 | 38 | 0 | 0 | 0 | 0 | 0 | 250 |
| 8:15 AM | 78 | 48 | 0 | 0 | 0 | 31 | 42 | 0 | 12 | 0 | 37 | 0 | 0 | 0 | 0 | 0 | 248 |
| 8:30 AM | 65 | 50 | 0 | 0 | 0 | 28 | 24 | 0 | 23 | 0 | 36 | 0 | 0 | 0 | 0 | 0 | 226 |
| 8:45 AM | 61 | 37 | 0 | 0 | 0 | 25 | 26 | 0 | 10 | 0 | 27 | 0 | 0 | 0 | 0 | 0 | 186 |
| TOTAL VOLUMES : APPROACH %'s : | NL 685 54.76% | NT 566 45.24% | NR 0 0.00% | NU 0 0.00% | SL 0 0.00% | ST 301 49.34% | SR 309 50.66% | SU 0 0.00% | EL 117 32.59% | ET 0 0.00% | ER 242 67.41% | EU 0 0.00% | WL 0 0.00% | WT 0 0.00% | WR 0 0.00% | WU 0 0.00% | TOTAL 2220 |
| PEAK HR : | 07:00 AM - 08:00 AM | | | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 414 | 372 | 0 | 0 | 0 | 189 | 177 | 0 | 54 | 0 | 104 | 0 | 0 | 0 | 0 | 0 | 1310 |
| PEAK HR FACTOR : | 0.908 | 0.845 | 0.000 | 0.000 | 0.000 | 0.606 | 0.851 | 0.000 | 0.711 | 0.000 | 0.722 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.910 |
| | 0.893 | | | | 0.738 | | | | 0.859 | | | | | | | | |
| PM | NORTHBOUND | | | | SOUTHBOUND | | | | EASTBOUND | | | | WESTBOUND | | | | TOTAL |
| | 0 NL | 0 NT | 0 NR | 0 NU | 0 SL | 0 ST | 0 SR | 0 SU | 0 EL | 0 ET | 0 ER | 0 EU | 0 WL | 0 WT | 0 WR | 0 WU | |
| 4:00 PM | 53 | 43 | 0 | 0 | 0 | 55 | 22 | 0 | 24 | 0 | 65 | 0 | 0 | 0 | 0 | 0 | 262 |
| 4:15 PM | 56 | 38 | 0 | 0 | 0 | 83 | 25 | 0 | 41 | 0 | 85 | 0 | 0 | 0 | 0 | 0 | 328 |
| 4:30 PM | 43 | 48 | 0 | 0 | 0 | 61 | 21 | 0 | 27 | 0 | 87 | 0 | 0 | 0 | 0 | 0 | 287 |
| 4:45 PM | 47 | 36 | 0 | 0 | 0 | 79 | 23 | 0 | 28 | 0 | 73 | 0 | 0 | 0 | 0 | 0 | 286 |
| 5:00 PM | 43 | 42 | 0 | 0 | 0 | 71 | 17 | 0 | 44 | 0 | 76 | 0 | 0 | 0 | 0 | 0 | 293 |
| 5:15 PM | 47 | 38 | 0 | 0 | 0 | 105 | 23 | 0 | 34 | 0 | 97 | 0 | 0 | 0 | 0 | 0 | 344 |
| 5:30 PM | 37 | 45 | 0 | 0 | 0 | 90 | 24 | 0 | 37 | 0 | 80 | 0 | 0 | 0 | 0 | 0 | 313 |
| 5:45 PM | 58 | 38 | 0 | 0 | 0 | 78 | 25 | 0 | 52 | 0 | 76 | 0 | 0 | 0 | 0 | 0 | 327 |
| TOTAL VOLUMES : APPROACH %'s : | NL 384 53.93% | NT 328 46.07% | NR 0 0.00% | NU 0 0.00% | SL 0 0.00% | ST 622 77.56% | SR 180 22.44% | SU 0 0.00% | EL 287 30.99% | ET 0 0.00% | ER 639 69.01% | EU 0 0.00% | WL 0 0.00% | WT 0 0.00% | WR 0 0.00% | WU 0 0.00% | TOTAL 2440 |
| PEAK HR : | 05:00 PM - 06:00 PM | | | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 185 | 163 | 0 | 0 | 0 | 344 | 89 | 0 | 167 | 0 | 329 | 0 | 0 | 0 | 0 | 0 | 1277 |
| PEAK HR FACTOR : | 0.797 | 0.906 | 0.000 | 0.000 | 0.000 | 0.819 | 0.890 | 0.000 | 0.803 | 0.000 | 0.848 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.928 |
| | 0.906 | | | | 0.846 | | | | 0.947 | | | | | | | | |

National Data & Surveying Services

Intersection Turning Movement Count

Location: Lake Helen Osteen Rd & Catalina Blvd
City: Deltona
Control: Signalized

Project ID: 24-130025-004
Date: 1/18/2024

Data - HT

| NS/EW Streets: | Lake Helen Osteen Rd | | | | Lake Helen Osteen Rd | | | | Catalina Blvd | | | | Catalina Blvd | | | |
|------------------|----------------------|----------|---------|---------|----------------------|----------|---------|---------|---------------|---------|----------|---------|---------------|---------|---------|---------|
| AM | NORTHBOUND | | | | SOUTHBOUND | | | | EASTBOUND | | | | WESTBOUND | | | |
| | 0 NL | 0 NT | 0 NR | 0 NU | 0 SL | 0 ST | 0 SR | 0 SU | 0 EL | 0 ET | 0 ER | 0 EU | 0 WL | 0 WT | 0 WR | 0 WU |
| 7:00 AM | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 |
| 7:15 AM | 2 | 3 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:30 AM | 1 | 3 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 |
| 7:45 AM | 1 | 5 | 0 | 0 | 0 | 3 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 |
| 8:00 AM | 2 | 2 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 |
| 8:15 AM | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 |
| 8:30 AM | 0 | 3 | 0 | 0 | 0 | 0 | 1 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:45 AM | 4 | 2 | 0 | 0 | 0 | 4 | 4 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 |
| TOTAL VOLUMES : | NL 12 | NT 19 | NR 0 | NU 0 | SL 0 | ST 17 | SR 7 | SU 0 | EL 3 | ET 0 | ER 8 | EU 0 | WL 0 | WT 0 | WR 0 | WU 0 |
| APPROACH %'s : | 38.71% | 61.29% | 0.00% | 0.00% | 0.00% | 70.83% | 29.17% | 0.00% | 27.27% | 0.00% | 72.73% | 0.00% | | | | |
| PEAK HR : | 07:00 AM - 08:00 AM | | | | | | | | | | | | | | | |
| PEAK HR VOL : | 4 | 12 | 0 | 0 | 0 | 10 | 2 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 |
| PEAK HR FACTOR : | 0.500 | 0.600 | 0.000 | 0.000 | 0.000 | 0.833 | 0.500 | 0.000 | 0.000 | 0.000 | 0.750 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 0.667 | | | | 0.750 | | | | 0.750 | | | | | | | |
| TOTAL | | | | | | | | | | | | | | | | |
| 31 | | | | | | | | | | | | | | | | |
| 0.705 | | | | | | | | | | | | | | | | |
| PM | NORTHBOUND | | | | SOUTHBOUND | | | | EASTBOUND | | | | WESTBOUND | | | |
| | 0 NL | 0 NT | 0 NR | 0 NU | 0 SL | 0 ST | 0 SR | 0 SU | 0 EL | 0 ET | 0 ER | 0 EU | 0 WL | 0 WT | 0 WR | 0 WU |
| 4:00 PM | 3 | 3 | 0 | 0 | 0 | 3 | 1 | 0 | 1 | 0 | 3 | 0 | 0 | 0 | 0 | 0 |
| 4:15 PM | 1 | 3 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 1 | 2 | 0 | 0 | 0 | 1 | 1 | 0 | 1 | 0 | 2 | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 1 | 4 | 0 | 0 | 0 | 2 | 1 | 0 | 1 | 0 | 3 | 0 | 0 | 0 | 0 | 0 |
| 5:00 PM | 0 | 2 | 0 | 0 | 0 | 2 | 3 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:15 PM | 4 | 0 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM | 5 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 |
| 5:45 PM | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 |
| TOTAL VOLUMES : | NL 16 | NT 15 | NR 0 | NU 0 | SL 0 | ST 19 | SR 7 | SU 0 | EL 7 | ET 0 | ER 16 | EU 0 | WL 0 | WT 0 | WR 0 | WU 0 |
| APPROACH %'s : | 51.61% | 48.39% | 0.00% | 0.00% | 0.00% | 73.08% | 26.92% | 0.00% | 30.43% | 0.00% | 69.57% | 0.00% | | | | |
| PEAK HR : | 05:00 PM - 06:00 PM | | | | | | | | | | | | | | | |
| PEAK HR VOL : | 10 | 3 | 0 | 0 | 0 | 11 | 4 | 0 | 2 | 0 | 7 | 0 | 0 | 0 | 0 | 0 |
| PEAK HR FACTOR : | 0.500 | 0.375 | 0.000 | 0.000 | 0.000 | 0.458 | 0.333 | 0.000 | 0.250 | 0.000 | 0.438 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 0.650 | | | | 0.625 | | | | 0.563 | | | | | | | |
| TOTAL | | | | | | | | | | | | | | | | |
| 37 | | | | | | | | | | | | | | | | |
| 0.771 | | | | | | | | | | | | | | | | |

Location: Lake Helen Osteen Rd & Catalina Blvd
City: Deltona
Control: Signalized

Data - Bikes

| NS/EW Streets: | | Lake Helen Osten Rd | | | | Lake Helen Osten Rd | | | | Catalina Blvd | | | | Catalina Blvd | | | | |
|-----------------------------------|---------|---------------------|--------------------|------------------|------------------|---------------------|---------|---------|---------|---------------|---------|---------|---------|---------------|---------|---------|---------|------------|
| AM | | NORTHBOUND | | | | SOUTHBOUND | | | | EASTBOUND | | | | WESTBOUND | | | | |
| | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| | | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| | 7:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 7:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 7:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 7:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 8:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 8:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 8:30 AM | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| | 8:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| TOTAL VOLUMES : APPROACH %'s : | | NL 1 100.00% | NT 0 0.00% | NR 0 0.00% | NU 0 0.00% | SL 0 | ST 0 | SR 0 | SU 0 | EL 0 | ET 0 | ER 0 | EU 0 | WL 0 | WT 0 | WR 0 | WU 0 | TOTAL 1 |
| PEAK HR : | | 07:00 AM - 08:00 AM | | | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | | 0 | | | | 0 | | | | 0 | | | | 0 | | | | 0 |
| PEAK HR FACTOR : | | 0.000 | | | | 0.000 | | | | 0.000 | | | | 0.000 | | | | 0.000 |
| PM | | NORTHBOUND | | | | SOUTHBOUND | | | | EASTBOUND | | | | WESTBOUND | | | | |
| | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| | | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| | 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 4:15 PM | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| | 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| TOTAL VOLUMES : APPROACH %'s : | | NL 0 0.00% | NT 2 100.00% | NR 0 0.00% | NU 0 0.00% | SL 0 | ST 0 | SR 0 | SU 0 | EL 0 | ET 0 | ER 0 | EU 0 | WL 0 | WT 0 | WR 0 | WU 0 | TOTAL 2 |
| PEAK HR : | | 05:00 PM - 06:00 PM | | | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | | 0 | | | | 0 | | | | 0 | | | | 0 | | | | 0 |
| PEAK HR FACTOR : | | 0.000 | | | | 0.000 | | | | 0.000 | | | | 0.000 | | | | 0.000 |

National Data & Surveying Services

Intersection Turning Movement Count

Location: Lake Helen Osteen Rd & Catalina Blvd
City: Deltona

Project ID: 24-130025-004
Date: 1/18/2024

Data - Pedestrians (Crosswalks)

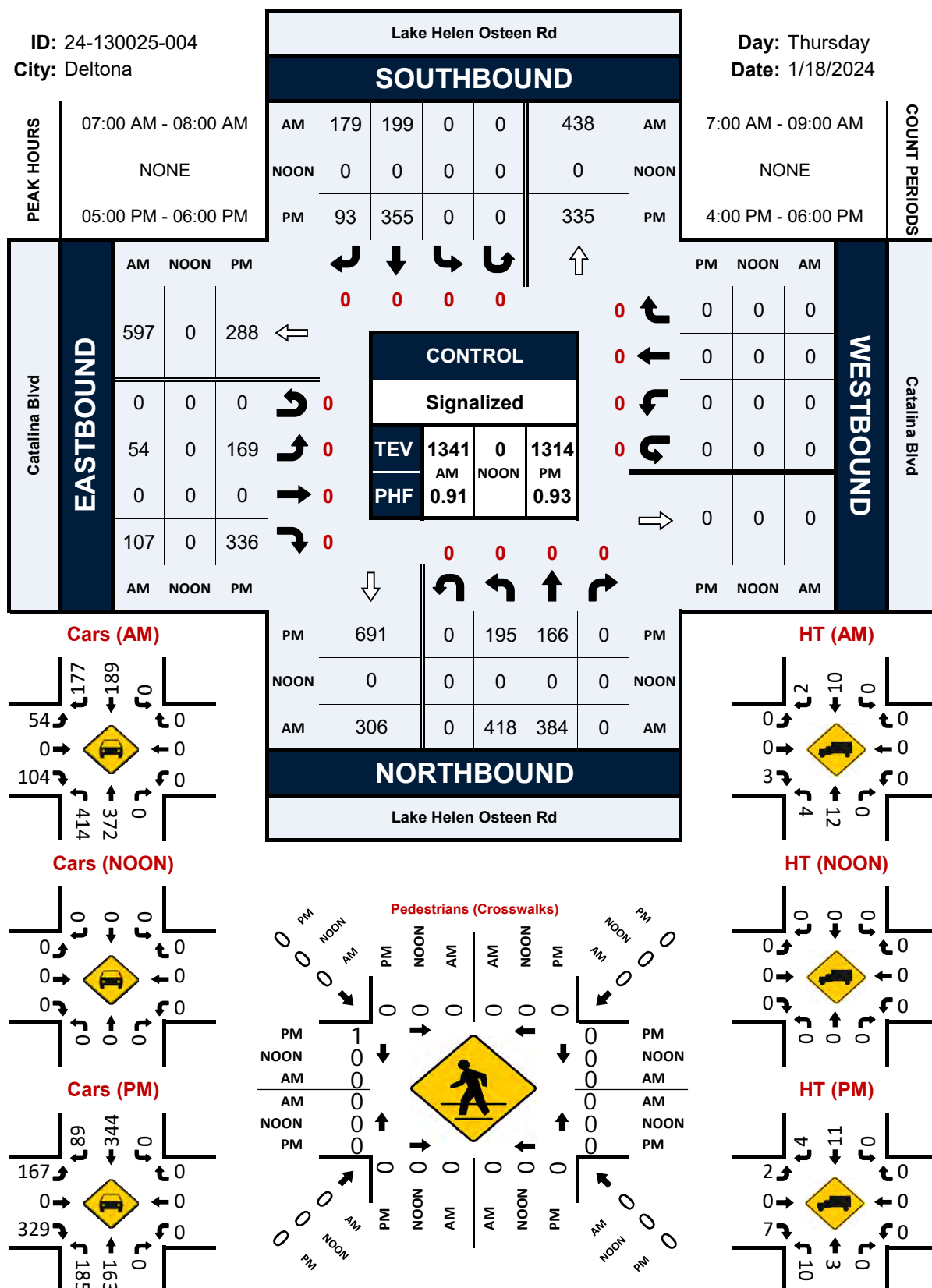
| NS/EW Streets: | Lake Helen Osteen Rd | | Lake Helen Osteen Rd | | Catalina Blvd | | Catalina Blvd | | |
|------------------|----------------------|----|----------------------|----|---------------|----|---------------|----|-------|
| AM | NORTH LEG | | SOUTH LEG | | EAST LEG | | WEST LEG | | TOTAL |
| | EB | WB | EB | WB | NB | SB | NB | SB | |
| 7:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| TOTAL VOLUMES : | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| APPROACH %'s : | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PEAK HR : | 07:00 AM - 08:00 AM | | | | | | | | TOTAL |
| PEAK HR VOL : | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PEAK HR FACTOR : | | | | | | | | | |

| PM | NORTH LEG | | SOUTH LEG | | EAST LEG | | WEST LEG | | TOTAL |
|------------------|---------------------|----|-----------|----|----------|----|-------------|-------------|-------|
| | EB | WB | EB | WB | NB | SB | NB | SB | |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| TOTAL VOLUMES : | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| APPROACH %'s : | 0 | 0 | 0 | 0 | 0 | 0 | 1 50.00% | 1 50.00% | 2 |
| PEAK HR : | 05:00 PM - 06:00 PM | | | | | | | | TOTAL |
| PEAK HR VOL : | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 |
| PEAK HR FACTOR : | | | | | | | 0.250 | 0.250 | 0.250 |

Peak Hour Turning Movement Count

City: Deltona

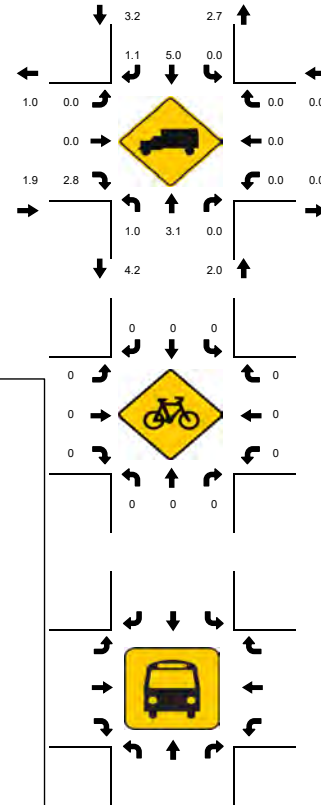
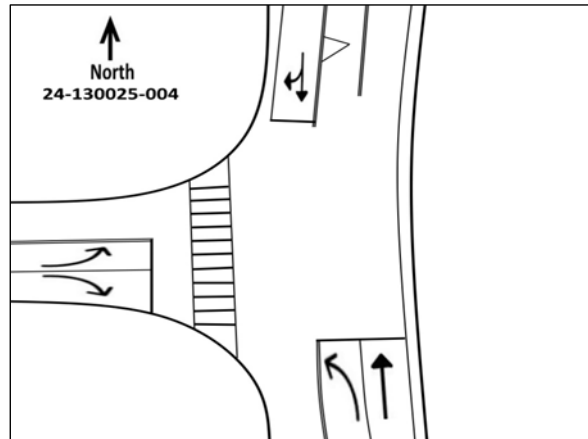
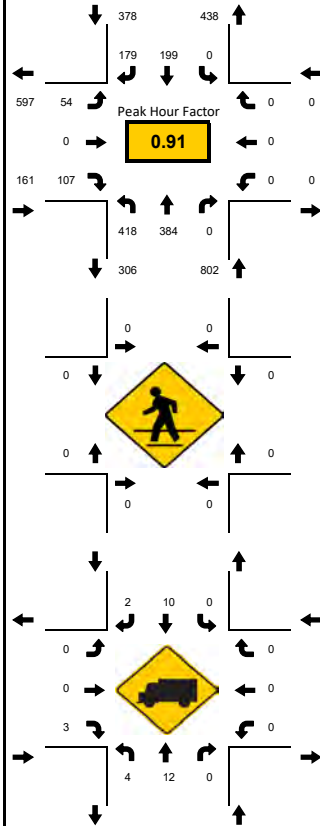
Date: 1/18/2024



LOCATION: Lake Helen Osteen Rd & Catalina Blvd
CITY/STATE: Deltona, FL

PROJECT ID: 24-130025-004
DATE: Thu, Jan 18, 2024

Peak-Hour: 07:00 AM - 08:00 AM
Peak 15-Minute: 07:30 AM - 07:45 AM



| 15-Min Count Period Beginning At | Lake Helen Osteen Rd Northbound | | | | | Lake Helen Osteen Rd Southbound | | | | | Catalina Blvd Eastbound | | | | | Catalina Blvd Westbound | | | | | Total | Hourly Total |
|--|------------------------------------|------|-----|---|----|------------------------------------|------|-----|---|----|----------------------------|------|-----|---|----|----------------------------|------|-----|---|----|-------|-----------------|
| | Left | Thru | Rgt | U | R* | Left | Thru | Rgt | U | R* | Left | Thru | Rgt | U | R* | Left | Thru | Rgt | U | R* | | |
| 7:00 AM | 107 | 81 | 0 | 0 | | 0 | 33 | 37 | 0 | | 14 | 0 | 16 | 0 | | 0 | 0 | 0 | 0 | | 288 | 1341 |
| 7:15 AM | 116 | 109 | 0 | 0 | | 0 | 34 | 42 | 0 | | 11 | 0 | 28 | 0 | | 0 | 0 | 0 | 0 | | 340 | 1310 |
| 7:30 AM | 106 | 113 | 0 | 0 | | 0 | 51 | 53 | 0 | | 19 | 0 | 26 | 0 | | 0 | 0 | 0 | 0 | | 368 | 1224 |
| 7:45 AM | 89 | 81 | 0 | 0 | | 0 | 81 | 47 | 0 | | 10 | 0 | 37 | 0 | | 0 | 0 | 0 | 0 | | 345 | 1088 |
| 8:00 AM | 69 | 61 | 0 | 0 | | 0 | 29 | 40 | 0 | | 18 | 0 | 40 | 0 | | 0 | 0 | 0 | 0 | | 257 | 945 |
| 8:15 AM | 80 | 48 | 0 | 0 | | 0 | 33 | 42 | 0 | | 13 | 0 | 38 | 0 | | 0 | 0 | 0 | 0 | | 254 | 688 |
| 8:30 AM | 65 | 53 | 0 | 0 | | 0 | 28 | 25 | 0 | | 25 | 0 | 36 | 0 | | 0 | 0 | 0 | 0 | | 232 | 434 |
| 8:45 AM | 65 | 39 | 0 | 0 | | 0 | 29 | 30 | 0 | | 10 | 0 | 29 | 0 | | 0 | 0 | 0 | 0 | | 202 | 202 |
| Peak 15-Min Flowrates | Left | Thru | Rgt | U | R* | Left | Thru | Rgt | U | R* | Left | Thru | Rgt | U | R* | Left | Thru | Rgt | U | R* | Total | |
| All Vehicles | 464 | 452 | 0 | 0 | | 0 | 324 | 212 | 0 | | 76 | 0 | 148 | 0 | | 0 | 0 | 0 | 0 | | 1676 | |
| Heavy Trucks | 8 | 20 | 0 | 0 | | 0 | 12 | 4 | 0 | | 0 | 0 | 4 | 0 | | 0 | 0 | 0 | 0 | | 48 | |
| Pedestrians | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | |
| Bicycles | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | |
| Buses | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | |
| Stopped Buses | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | |

PROJECT ID: 24-130025-004
DATE: Thu, Jan 18, 2024

[illegible]

National Data & Surveying Services

Intersection Turning Movement Count

Location: Lake Helen Osteen Rd & New Hope Baptist Church N Dwy
City: Deltona
Control: 1-Way Stop(WB)

Project ID: 24-130025-003
Date: 1/18/2024

Data - Total

| NS/EW Streets: | Lake Helen Osteen Rd | | | | Lake Helen Osteen Rd | | | | New Hope Baptist Church N Dwy | | | | New Hope Baptist Church N Dwy | | | | | | |
|-----------------------------------|----------------------|----------------------|------------------|------------------|----------------------|----------------------|------------------|------------------|-------------------------------|------------------|------------------|------------------|-------------------------------|------------------|--------------------|------------------|---------------|-----|-----|
| AM | NORTHBOUND | | | | SOUTHBOUND | | | | EASTBOUND | | | | WESTBOUND | | | | TOTAL | | |
| | 0 NL | 0 NT | 0 NR | 0 NU | 0 SL | 0 ST | 0 SR | 0 SU | 0 EL | 0 ET | 0 ER | 0 EU | 0 WL | 0 WT | 0 WR | 0 WU | | | |
| | 7:00 AM | 0 | 104 | 0 | 0 | 0 | 38 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | | 0 | 143 |
| | 7:15 AM | 0 | 124 | 0 | 0 | 0 | 41 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | | 167 | |
| | 7:30 AM | 0 | 137 | 0 | 0 | 0 | 66 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | | 207 | |
| | 7:45 AM | 0 | 99 | 0 | 0 | 0 | 85 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 2 | 0 | | 187 | |
| | 8:00 AM | 0 | 80 | 0 | 0 | 0 | 44 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | 124 | |
| | 8:15 AM | 0 | 58 | 0 | 0 | 0 | 56 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | | 118 | |
| | 8:30 AM | 0 | 67 | 0 | 0 | 0 | 45 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 3 | 0 | | 116 | |
| | 8:45 AM | 0 | 60 | 0 | 0 | 0 | 36 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | | 98 | |
| TOTAL VOLUMES : APPROACH %'s : | NL 0 0.00% | NT 729 100.00% | NR 0 0.00% | NU 0 0.00% | SL 0 0.00% | ST 411 100.00% | SR 0 0.00% | SU 0 0.00% | EL 0 0.00% | ET 0 0.00% | ER 0 0.00% | EU 0 0.00% | WL 8 40.00% | WT 0 0.00% | WR 12 60.00% | WU 0 0.00% | TOTAL 1160 | | |
| PEAK HR : | 07:00 AM - 08:00 AM | | | | | | | | | | | | | | | | TOTAL | | |
| PEAK HR VOL : | 0 | 464 | 0 | 0 | 0 | 230 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 7 | 0 | 704 | | |
| PEAK HR FACTOR : | 0.000 | 0.847 | 0.000 | 0.000 | 0.000 | 0.676 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.750 | 0.000 | 0.438 | 0.000 | 0.850 | | |
| | | | | 0.847 | | | | 0.676 | | | | 0.625 | | | | | | | |
| PM | NORTHBOUND | | | | SOUTHBOUND | | | | EASTBOUND | | | | WESTBOUND | | | | TOTAL | | |
| | 0 NL | 0 NT | 0 NR | 0 NU | 0 SL | 0 ST | 0 SR | 0 SU | 0 EL | 0 ET | 0 ER | 0 EU | 0 WL | 0 WT | 0 WR | 0 WU | | | |
| | 4:00 PM | 0 | 67 | 0 | 0 | 0 | 72 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | | 140 | |
| | 4:15 PM | 0 | 71 | 0 | 0 | 0 | 109 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | | 183 | |
| | 4:30 PM | 0 | 66 | 0 | 0 | 0 | 81 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 2 | 0 | | 152 | |
| | 4:45 PM | 0 | 64 | 0 | 0 | 0 | 90 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | | 155 | |
| | 5:00 PM | 0 | 66 | 0 | 0 | 0 | 87 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | | 157 | |
| | 5:15 PM | 0 | 55 | 0 | 0 | 0 | 145 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | | 204 | |
| | 5:30 PM | 0 | 73 | 0 | 0 | 0 | 112 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 2 | 0 | | 188 | |
| | 5:45 PM | 0 | 64 | 0 | 0 | 0 | 92 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | 156 | |
| TOTAL VOLUMES : APPROACH %'s : | NL 0 0.00% | NT 526 100.00% | NR 0 0.00% | NU 0 0.00% | SL 0 0.00% | ST 788 100.00% | SR 0 0.00% | SU 0 0.00% | EL 0 0.00% | ET 0 0.00% | ER 0 0.00% | EU 0 0.00% | WL 12 57.14% | WT 0 0.00% | WR 9 42.86% | WU 0 0.00% | TOTAL 1335 | | |
| PEAK HR : | 05:00 PM - 06:00 PM | | | | | | | | | | | | | | | | TOTAL | | |
| PEAK HR VOL : | 0 | 258 | 0 | 0 | 0 | 436 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 6 | 0 | 705 | | |
| PEAK HR FACTOR : | 0.000 | 0.884 | 0.000 | 0.000 | 0.000 | 0.752 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.625 | 0.000 | 0.750 | 0.000 | 0.864 | | |
| | | | | 0.884 | | | | 0.752 | | | | 0.688 | | | | | | | |
| #DIV/0! | | 3% | #DIV/0! | #DIV/0! | #DIV/0! | 4% | #DIV/0! | #DIV/0! | #DIV/0! | #DIV/0! | #DIV/0! | #DIV/0! | 0% | #DIV/0! | 0% | #DIV/0! | | | |
| #DIV/0! | | 2% | #DIV/0! | #DIV/0! | #DIV/0! | 3% | #DIV/0! | #DIV/0! | #DIV/0! | #DIV/0! | #DIV/0! | #DIV/0! | 0% | #DIV/0! | 17% | #DIV/0! | | | |

National Data & Surveying Services

Intersection Turning Movement Count

Location: Lake Helen Osteen Rd & New Hope Baptist Church N Dwy
City: Deltona
Control: 1-Way Stop(WB)

Project ID: 24-130025-003
Date: 1/18/2024

Data - Cars

| NS/EW Streets: | Lake Helen Osteen Rd | | | | Lake Helen Osteen Rd | | | | New Hope Baptist Church N Dwy | | | | New Hope Baptist Church N Dwy | | | | |
|------------------|----------------------|---------|---------|---------|----------------------|---------|---------|---------|-------------------------------|---------|---------|---------|-------------------------------|---------|---------|---------|-------|
| AM | NORTHBOUND | | | | SOUTHBOUND | | | | EASTBOUND | | | | WESTBOUND | | | | TOTAL |
| | 0 NL | 0 NT | 0 NR | 0 NU | 0 SL | 0 ST | 0 SR | 0 SU | 0 EL | 0 ET | 0 ER | 0 EU | 0 WL | 0 WT | 0 WR | 0 WU | |
| 7:00 AM | 0 | 103 | 0 | 0 | 0 | 38 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 142 |
| 7:15 AM | 0 | 119 | 0 | 0 | 0 | 39 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 160 |
| 7:30 AM | 0 | 134 | 0 | 0 | 0 | 63 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 201 |
| 7:45 AM | 0 | 96 | 0 | 0 | 0 | 80 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 2 | 0 | 179 |
| 8:00 AM | 0 | 75 | 0 | 0 | 0 | 41 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 116 |
| 8:15 AM | 0 | 57 | 0 | 0 | 0 | 53 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 114 |
| 8:30 AM | 0 | 65 | 0 | 0 | 0 | 44 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 3 | 0 | 113 |
| 8:45 AM | 0 | 57 | 0 | 0 | 0 | 30 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 89 |
| TOTAL VOLUMES : | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| APPROACH %'s : | 0 | 706 | 0 | 0 | 0 | 388 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 12 | 0 | 1114 |
| | 0.00% | 100.00% | 0.00% | 0.00% | 0.00% | 100.00% | 0.00% | 0.00% | | | | | 40.00% | 0.00% | 60.00% | 0.00% | |
| PEAK HR : | 07:00 AM - 08:00 AM | | | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 0 | 452 | 0 | 0 | 0 | 220 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 7 | 0 | 682 |
| PEAK HR FACTOR : | 0.000 | 0.843 | 0.000 | 0.000 | 0.000 | 0.688 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.750 | 0.000 | 0.438 | 0.000 | 0.848 |
| | 0.843 | | | | 0.688 | | | | | | | | 0.625 | | | | |
| PM | NORTHBOUND | | | | SOUTHBOUND | | | | EASTBOUND | | | | WESTBOUND | | | | TOTAL |
| | 0 NL | 0 NT | 0 NR | 0 NU | 0 SL | 0 ST | 0 SR | 0 SU | 0 EL | 0 ET | 0 ER | 0 EU | 0 WL | 0 WT | 0 WR | 0 WU | |
| 4:00 PM | 0 | 64 | 0 | 0 | 0 | 68 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 133 |
| 4:15 PM | 0 | 67 | 0 | 0 | 0 | 107 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 177 |
| 4:30 PM | 0 | 65 | 0 | 0 | 0 | 80 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 2 | 0 | 150 |
| 4:45 PM | 0 | 61 | 0 | 0 | 0 | 89 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 151 |
| 5:00 PM | 0 | 65 | 0 | 0 | 0 | 86 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 154 |
| 5:15 PM | 0 | 53 | 0 | 0 | 0 | 140 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 197 |
| 5:30 PM | 0 | 71 | 0 | 0 | 0 | 107 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 2 | 0 | 181 |
| 5:45 PM | 0 | 64 | 0 | 0 | 0 | 92 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 156 |
| TOTAL VOLUMES : | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| APPROACH %'s : | 0 | 510 | 0 | 0 | 0 | 769 | 0 | 0 | 0 | 0 | 0 | 0 | 12 | 0 | 8 | 0 | 1299 |
| | 0.00% | 100.00% | 0.00% | 0.00% | 0.00% | 100.00% | 0.00% | 0.00% | | | | | 60.00% | 0.00% | 40.00% | 0.00% | |
| PEAK HR : | 05:00 PM - 06:00 PM | | | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 0 | 253 | 0 | 0 | 0 | 425 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 5 | 0 | 688 |
| PEAK HR FACTOR : | 0.000 | 0.891 | 0.000 | 0.000 | 0.000 | 0.759 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.625 | 0.000 | 0.625 | 0.000 | 0.873 |
| | 0.891 | | | | 0.759 | | | | | | | | 0.625 | | | | |

National Data & Surveying Services

Intersection Turning Movement Count

Location: Lake Helen Osteen Rd & New Hope Baptist Church N Dwy
City: Deltona
Control: 1-Way Stop(WB)

Project ID: 24-130025-003
Date: 1/18/2024

Data - HT

| NS/EW Streets: | Lake Helen Osteen Rd | | | | Lake Helen Osteen Rd | | | | New Hope Baptist Church N Dwy | | | | New Hope Baptist Church N Dwy | | | | |
|------------------|----------------------|---------|---------|---------|----------------------|---------|---------|---------|-------------------------------|---------|---------|---------|-------------------------------|---------|---------|---------|-------|
| AM | NORTHBOUND | | | | SOUTHBOUND | | | | EASTBOUND | | | | WESTBOUND | | | | TOTAL |
| | 0 NL | 0 NT | 0 NR | 0 NU | 0 SL | 0 ST | 0 SR | 0 SU | 0 EL | 0 ET | 0 ER | 0 EU | 0 WL | 0 WT | 0 WR | 0 WU | |
| 7:00 AM | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 7:15 AM | 0 | 5 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 |
| 7:30 AM | 0 | 3 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| 7:45 AM | 0 | 3 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| 8:00 AM | 0 | 5 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| 8:15 AM | 0 | 1 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 8:30 AM | 0 | 2 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 8:45 AM | 0 | 3 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 |
| TOTAL VOLUMES : | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| APPROACH %'s : | 0 | 23 | 0 | 0 | 0 | 23 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 46 |
| | 0.00% | 100.00% | 0.00% | 0.00% | 0.00% | 100.00% | 0.00% | 0.00% | | | | | | | | | |
| PEAK HR : | 07:00 AM - 08:00 AM | | | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 0 | 12 | 0 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 22 |
| PEAK HR FACTOR : | 0.000 | 0.600 | 0.000 | 0.000 | 0.000 | 0.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.688 |
| | 0.600 | | | | 0.500 | | | | | | | | | | | | |
| PM | NORTHBOUND | | | | SOUTHBOUND | | | | EASTBOUND | | | | WESTBOUND | | | | TOTAL |
| | 0 NL | 0 NT | 0 NR | 0 NU | 0 SL | 0 ST | 0 SR | 0 SU | 0 EL | 0 ET | 0 ER | 0 EU | 0 WL | 0 WT | 0 WR | 0 WU | |
| 4:00 PM | 0 | 3 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 |
| 4:15 PM | 0 | 4 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| 4:30 PM | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 4:45 PM | 0 | 3 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 5:00 PM | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 3 |
| 5:15 PM | 0 | 2 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 |
| 5:30 PM | 0 | 2 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| TOTAL VOLUMES : | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| APPROACH %'s : | 0 | 16 | 0 | 0 | 0 | 19 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 36 |
| | 0.00% | 100.00% | 0.00% | 0.00% | 0.00% | 100.00% | 0.00% | 0.00% | | | | | 0.00% | 0.00% | 100.00% | 0.00% | |
| PEAK HR : | 05:00 PM - 06:00 PM | | | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 0 | 5 | 0 | 0 | 0 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 17 |
| PEAK HR FACTOR : | 0.000 | 0.625 | 0.000 | 0.000 | 0.000 | 0.550 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.250 | 0.000 | 0.607 |
| | 0.625 | | | | 0.550 | | | | | | | | 0.250 | | | | |

Location: Lake Helen Osteen Rd & New Hope Baptist Church N Dwy
City: Deltona
Control: 1-Way Stop(WB)

Project ID: 24-130025-003
Date: 1/18/2024

| NS/EW Streets: | Lake Helen Osten Rd | | | | Lake Helen Osten Rd | | | | New Hope Baptist Church N Dwy | | | | New Hope Baptist Church N Dwy | | | | | |
|-----------------------------------|---------------------|---------|---------|---------|----------------------------------|---------|---------|---------|----------------------------------|---------|---------|---------|----------------------------------|---------|---------|---------|------------|---|
| <div>AM</div> | NORTHBOUND | | | | SOUTHBOUND | | | | EASTBOUND | | | | WESTBOUND | | | | TOTAL | |
| | O NL | O NT | O NR | O NU | O SL | O ST | O SR | O SU | O EL | O ET | O ER | O EU | O WL | O WT | O WR | O WU | | |
| | 7:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | 0 |
| | 7:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | 0 |
| | 7:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | 0 |
| | 7:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | 0 |
| | 8:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | 0 |
| | 8:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | 0 |
| | 8:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | 0 |
| 8:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| TOTAL VOLUMES : APPROACH %'s : | NL 0 | NT 0 | NR 0 | NU 0 | SL 0 | ST 0 | SR 0 | SU 0 | EL 0 | ET 0 | ER 0 | EU 0 | WL 0 | WT 0 | WR 0 | WU 0 | TOTAL 0 | |
| PEAK HR : | 07:00 AM - 08:00 AM | | | | | | | | | | | | | | | | TOTAL 0 | |
| PEAK HR VOL : | 0 | 0 | 0 | 0 | | | | | | | | | | | | | | |
| PEAK HR FACTOR : | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 0.000 0.000 0.000 | | | | 0.000 0.000 0.000 0.000 | | | | 0.000 0.000 0.000 0.000 | | | | | |
| <div>PM</div> | NORTHBOUND | | | | SOUTHBOUND | | | | EASTBOUND | | | | WESTBOUND | | | | TOTAL | |
| | O NL | O NT | O NR | O NU | O SL | O ST | O SR | O SU | O EL | O ET | O ER | O EU | O WL | O WT | O WR | O WU | | |
| | 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | 0 |
| | 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | 0 |
| | 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | 0 |
| | 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | 0 |
| | 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | 0 |
| | 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | 0 |
| | 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | 0 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| TOTAL VOLUMES : APPROACH %'s : | NL 0 | NT 0 | NR 0 | NU 0 | SL 0 | ST 0 | SR 0 | SU 0 | EL 0 | ET 0 | ER 0 | EU 0 | WL 0 | WT 0 | WR 0 | WU 0 | TOTAL 0 | |
| PEAK HR : | 05:00 PM - 06:00 PM | | | | | | | | | | | | | | | | TOTAL 0 | |
| PEAK HR VOL : | 0 | 0 | 0 | 0 | | | | | | | | | | | | | | |
| PEAK HR FACTOR : | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 0.000 0.000 0.000 | | | | 0.000 0.000 0.000 0.000 | | | | 0.000 0.000 0.000 0.000 | | | | | |

National Data & Surveying Services

Location: Lake Helen Osteen Rd & New Hope Baptist Church N Dwy
City: Deltona

Project ID: 24-130025-003
Date: 1/18/2024

Data - Pedestrians (Crosswalks)

| NS/EW Streets: | Lake Helen Osteen Rd | | Lake Helen Osteen Rd | | New Hope Baptist Church N Dwy | | New Hope Baptist Church N Dwy | | |
|------------------|----------------------|----|----------------------|----|----------------------------------|----|----------------------------------|----|-------|
| AM | NORTH LEG | | SOUTH LEG | | EAST LEG | | WEST LEG | | TOTAL |
| | EB | WB | EB | WB | NB | SB | NB | SB | |
| 7:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| TOTAL VOLUMES : | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| APPROACH %'s : | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PEAK HR : | 07:00 AM - 08:00 AM | | | | | | | | TOTAL |
| PEAK HR VOL : | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PEAK HR FACTOR : | | | | | | | | | |

| PM | NORTH LEG | | SOUTH LEG | | EAST LEG | | WEST LEG | | TOTAL |
|-----------------------------------|---------------------|---------|-----------|---------|----------|---------|----------|---------|------------|
| | EB | WB | EB | WB | NB | SB | NB | SB | |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| TOTAL VOLUMES : APPROACH %'s : | EB 0 | WB 0 | EB 0 | WB 0 | NB 0 | SB 0 | NB 0 | SB 0 | TOTAL 0 |
| PEAK HR : | 05:00 PM - 06:00 PM | | | | | | | | TOTAL |
| PEAK HR VOL : | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PEAK HR FACTOR : | | | | | | | | | |

Lake Helen Osteen Rd & New Hope Baptist Church N Dwy

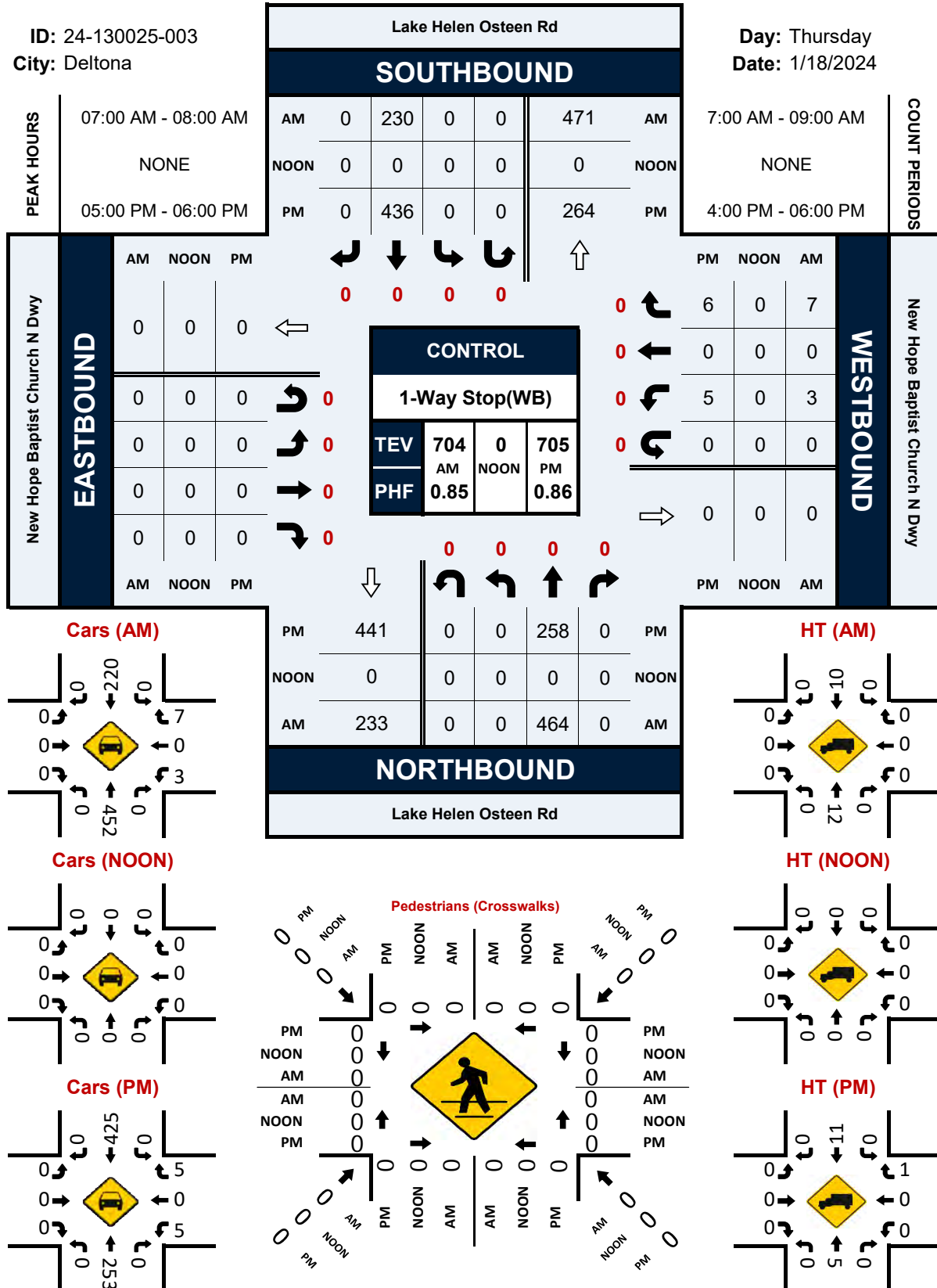
Peak Hour Turning Movement Count

ID: 24-130025-003

City: Deltona

Day: Thursday

Date: 1/18/2024



PROJECT ID: 24-130025-003
DATE: Thu, Jan 18, 2024

[illegible]

PROJECT ID: 24-130025-003
DATE: Thu, Jan 18, 2024

[illegible]

National Data & Surveying Services

Intersection Turning Movement Count

Location: Lake Helen Osteen Rd & New Hope Baptist Church S Dwy
City: Deltona
Control: No Control

Project ID: 24-130025-002
Date: 1/18/2024

Data - Cars

| NS/EW Streets: | Lake Helen Osteen Rd | | | | Lake Helen Osteen Rd | | | | New Hope Baptist Church S Dwy | | | | New Hope Baptist Church S Dwy | | | | |
|------------------|----------------------|---------|---------|---------|----------------------|---------|---------|---------|-------------------------------|---------|---------|---------|-------------------------------|---------|---------|---------|-------|
| AM | NORTHBOUND | | | | SOUTHBOUND | | | | EASTBOUND | | | | WESTBOUND | | | | TOTAL |
| | 0 NL | 0 NT | 0 NR | 0 NU | 0 SL | 0 ST | 0 SR | 0 SU | 0 EL | 0 ET | 0 ER | 0 EU | 0 WL | 0 WT | 0 WR | 0 WU | |
| 7:00 AM | 0 | 107 | 1 | 0 | 0 | 39 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 147 |
| 7:15 AM | 0 | 115 | 1 | 0 | 1 | 38 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 155 |
| 7:30 AM | 0 | 136 | 1 | 0 | 5 | 59 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 201 |
| 7:45 AM | 0 | 94 | 2 | 0 | 1 | 78 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 175 |
| 8:00 AM | 0 | 76 | 0 | 0 | 1 | 42 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 119 |
| 8:15 AM | 0 | 56 | 6 | 0 | 7 | 47 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 116 |
| 8:30 AM | 0 | 65 | 2 | 0 | 0 | 46 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 113 |
| 8:45 AM | 0 | 58 | 1 | 0 | 1 | 31 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 91 |
| TOTAL VOLUMES : | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| APPROACH %'s : | 0 | 707 | 14 | 0 | 16 | 380 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1117 |
| | 0.00% | 98.06% | 1.94% | 0.00% | 4.04% | 95.96% | 0.00% | 0.00% | | | | | | | | | |
| PEAK HR : | 07:00 AM - 08:00 AM | | | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 0 | 452 | 5 | 0 | 7 | 214 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 678 |
| PEAK HR FACTOR : | 0.000 | 0.831 | 0.625 | 0.000 | 0.350 | 0.686 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.843 |
| | 0.834 | | | | 0.699 | | | | | | | | | | | | |
| PM | NORTHBOUND | | | | SOUTHBOUND | | | | EASTBOUND | | | | WESTBOUND | | | | TOTAL |
| | 0 NL | 0 NT | 0 NR | 0 NU | 0 SL | 0 ST | 0 SR | 0 SU | 0 EL | 0 ET | 0 ER | 0 EU | 0 WL | 0 WT | 0 WR | 0 WU | |
| 4:00 PM | 0 | 66 | 1 | 0 | 0 | 67 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 134 |
| 4:15 PM | 0 | 65 | 1 | 0 | 3 | 107 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 176 |
| 4:30 PM | 0 | 66 | 1 | 0 | 3 | 81 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 151 |
| 4:45 PM | 0 | 60 | 1 | 0 | 0 | 90 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 151 |
| 5:00 PM | 0 | 67 | 1 | 0 | 1 | 86 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 155 |
| 5:15 PM | 0 | 52 | 1 | 0 | 4 | 139 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 196 |
| 5:30 PM | 0 | 70 | 0 | 0 | 0 | 107 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 177 |
| 5:45 PM | 0 | 65 | 0 | 0 | 0 | 93 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 158 |
| TOTAL VOLUMES : | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| APPROACH %'s : | 0 | 511 | 6 | 0 | 11 | 770 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1298 |
| | 0.00% | 98.84% | 1.16% | 0.00% | 1.41% | 98.59% | 0.00% | 0.00% | | | | | | | | | |
| PEAK HR : | 05:00 PM - 06:00 PM | | | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 0 | 254 | 2 | 0 | 5 | 425 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 686 |
| PEAK HR FACTOR : | 0.000 | 0.907 | 0.500 | 0.000 | 0.313 | 0.764 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.875 |
| | 0.914 | | | | 0.752 | | | | | | | | | | | | |

National Data & Surveying Services

Intersection Turning Movement Count

Location: Lake Helen Osteen Rd & New Hope Baptist Church S Dwy
City: Deltona
Control: No Control

Project ID: 24-130025-002
Date: 1/18/2024

Data - HT

| NS/EW Streets: | Lake Helen Osteen Rd | | | | Lake Helen Osteen Rd | | | | New Hope Baptist Church S Dwy | | | | New Hope Baptist Church S Dwy | | | | |
|------------------|----------------------|---------|---------|---------|----------------------|---------|---------|---------|-------------------------------|---------|---------|---------|-------------------------------|---------|---------|---------|-------|
| AM | NORTHBOUND | | | | SOUTHBOUND | | | | EASTBOUND | | | | WESTBOUND | | | | TOTAL |
| | 0 NL | 0 NT | 0 NR | 0 NU | 0 SL | 0 ST | 0 SR | 0 SU | 0 EL | 0 ET | 0 ER | 0 EU | 0 WL | 0 WT | 0 WR | 0 WU | |
| 7:00 AM | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 7:15 AM | 0 | 4 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| 7:30 AM | 0 | 3 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| 7:45 AM | 0 | 4 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| 8:00 AM | 0 | 4 | 0 | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| 8:15 AM | 0 | 1 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 8:30 AM | 0 | 2 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 8:45 AM | 0 | 3 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 |
| TOTAL VOLUMES : | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| APPROACH %'s : | 0 | 23 | 0 | 0 | 1 | 22 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 46 |
| | 0.00% | 100.00% | 0.00% | 0.00% | 4.35% | 95.65% | 0.00% | 0.00% | | | | | | | | | |
| PEAK HR : | 07:00 AM - 08:00 AM | | | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 0 | 13 | 0 | 0 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 22 |
| PEAK HR FACTOR : | 0.000 | 0.813 | 0.000 | 0.000 | 0.000 | 0.563 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.688 |
| | 0.813 | | | | 0.563 | | | | | | | | | | | | |
| PM | NORTHBOUND | | | | SOUTHBOUND | | | | EASTBOUND | | | | WESTBOUND | | | | TOTAL |
| | 0 NL | 0 NT | 0 NR | 0 NU | 0 SL | 0 ST | 0 SR | 0 SU | 0 EL | 0 ET | 0 ER | 0 EU | 0 WL | 0 WT | 0 WR | 0 WU | |
| 4:00 PM | 0 | 2 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| 4:15 PM | 0 | 4 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| 4:30 PM | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 4:45 PM | 0 | 3 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 5:00 PM | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 5:15 PM | 0 | 2 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 |
| 5:30 PM | 0 | 2 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| TOTAL VOLUMES : | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| APPROACH %'s : | 0 | 15 | 0 | 0 | 0 | 19 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 34 |
| | 0.00% | 100.00% | 0.00% | 0.00% | 0.00% | 100.00% | 0.00% | 0.00% | | | | | | | | | |
| PEAK HR : | 05:00 PM - 06:00 PM | | | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 0 | 5 | 0 | 0 | 0 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16 |
| PEAK HR FACTOR : | 0.000 | 0.625 | 0.000 | 0.000 | 0.000 | 0.550 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.571 |
| | 0.625 | | | | 0.550 | | | | | | | | | | | | |

Location: Lake Helen Osteen Rd & New Hope Baptist Church S Dwy
City: Deltona
Control: No Control

Project ID: 24-130025-002
Date: 1/18/2024

[illegible]

National Data & Surveying Services

Location: Lake Helen Osteen Rd & New Hope Baptist Church S Dwy
City: Deltona

Project ID: 24-130025-002
Date: 1/18/2024

Data - Pedestrians (Crosswalks)

| NS/EW Streets: | Lake Helen Osteen Rd | | Lake Helen Osteen Rd | | New Hope Baptist Church S Dwy | | New Hope Baptist Church S Dwy | | |
|------------------|----------------------|----|----------------------|----|----------------------------------|----|----------------------------------|----|-------|
| AM | NORTH LEG | | SOUTH LEG | | EAST LEG | | WEST LEG | | TOTAL |
| | EB | WB | EB | WB | NB | SB | NB | SB | |
| 7:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| TOTAL VOLUMES : | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| APPROACH %'s : | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PEAK HR : | 07:00 AM - 08:00 AM | | | | | | | | TOTAL |
| PEAK HR VOL : | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PEAK HR FACTOR : | | | | | | | | | |

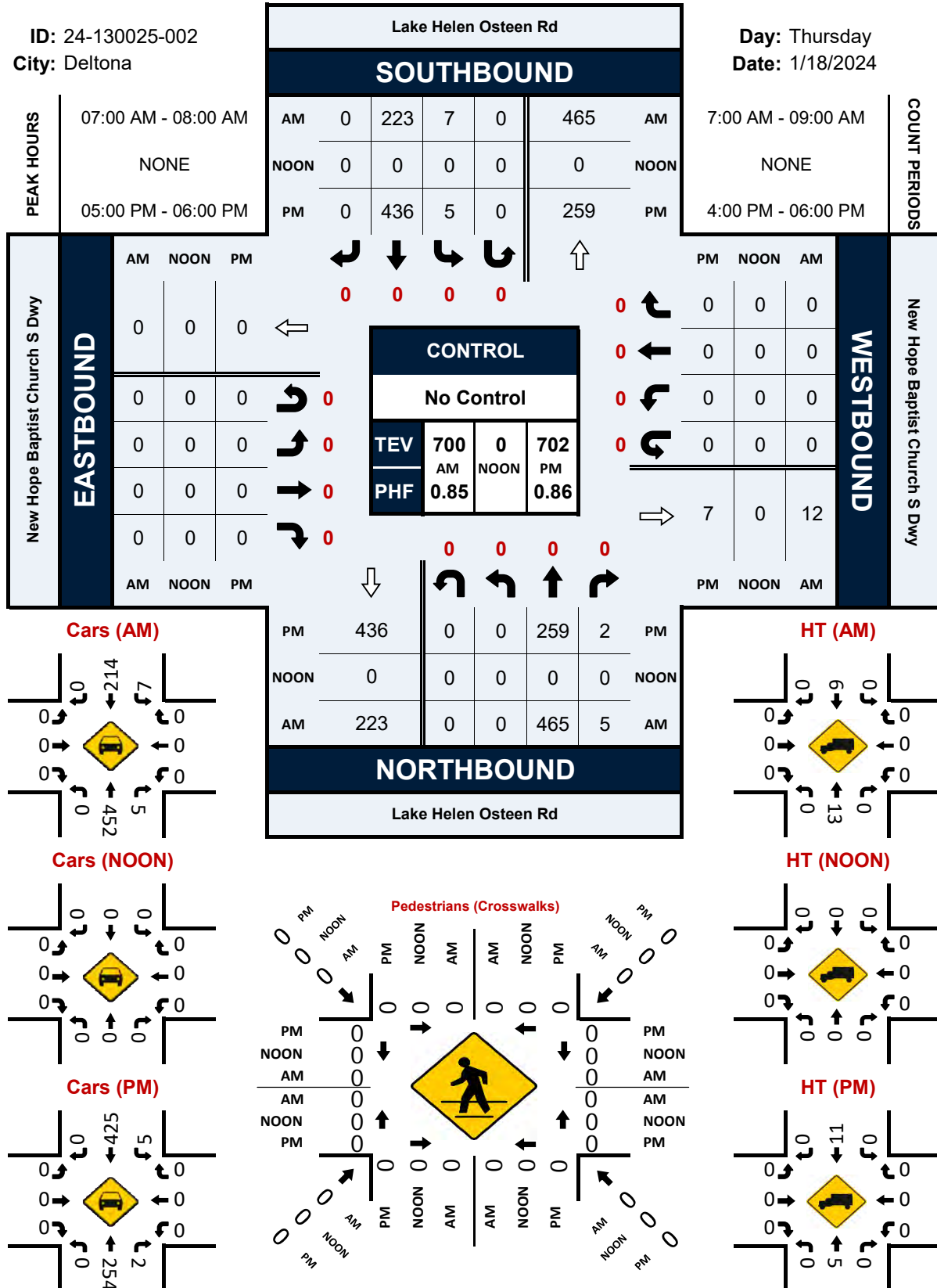
| PM | NORTH LEG | | SOUTH LEG | | EAST LEG | | WEST LEG | | TOTAL |
|-----------------------------------|---------------------|---------|-----------|---------|----------|---------|----------|---------|------------|
| | EB | WB | EB | WB | NB | SB | NB | SB | |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| TOTAL VOLUMES : APPROACH %'s : | EB 0 | WB 0 | EB 0 | WB 0 | NB 0 | SB 0 | NB 0 | SB 0 | TOTAL 0 |
| PEAK HR : | 05:00 PM - 06:00 PM | | | | | | | | TOTAL |
| PEAK HR VOL : | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PEAK HR FACTOR : | | | | | | | | | |

Lake Helen Osteen Rd & New Hope Baptist Church S Dwy

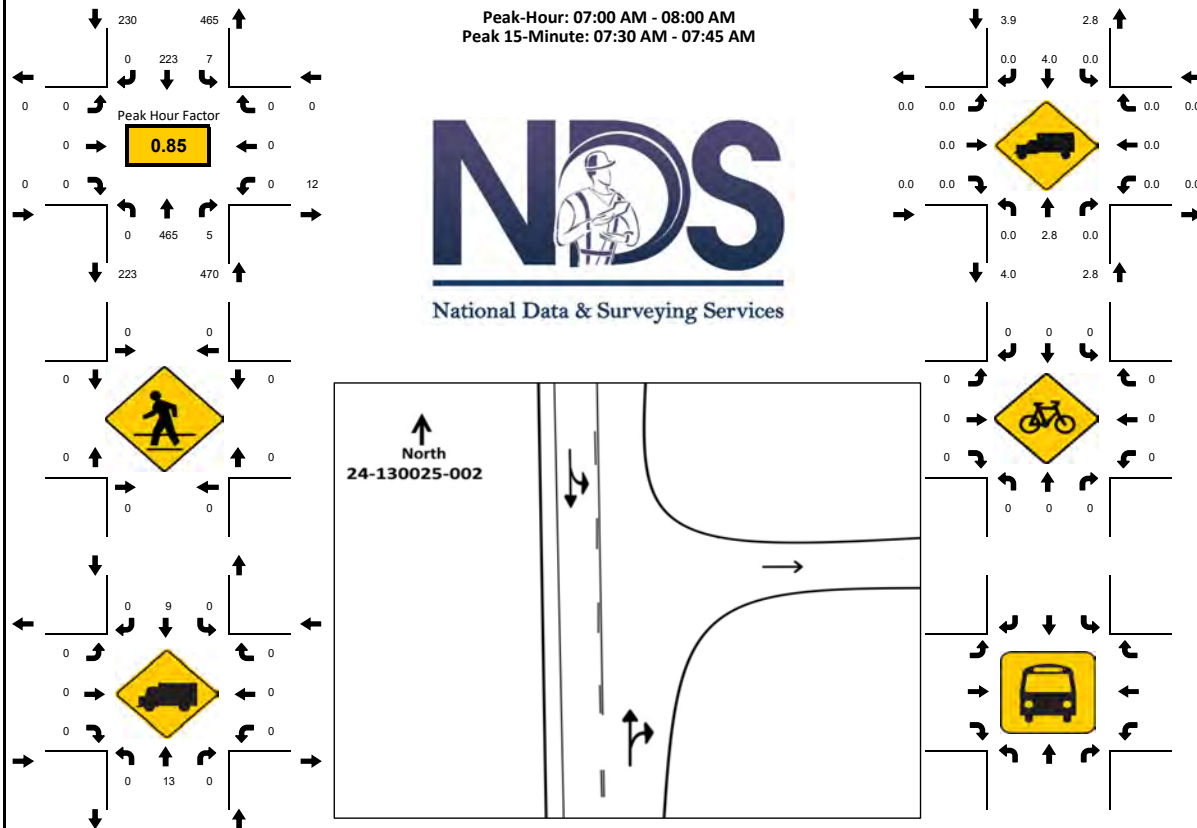
Peak Hour Turning Movement Count

ID: 24-130025-002
City: Deltona

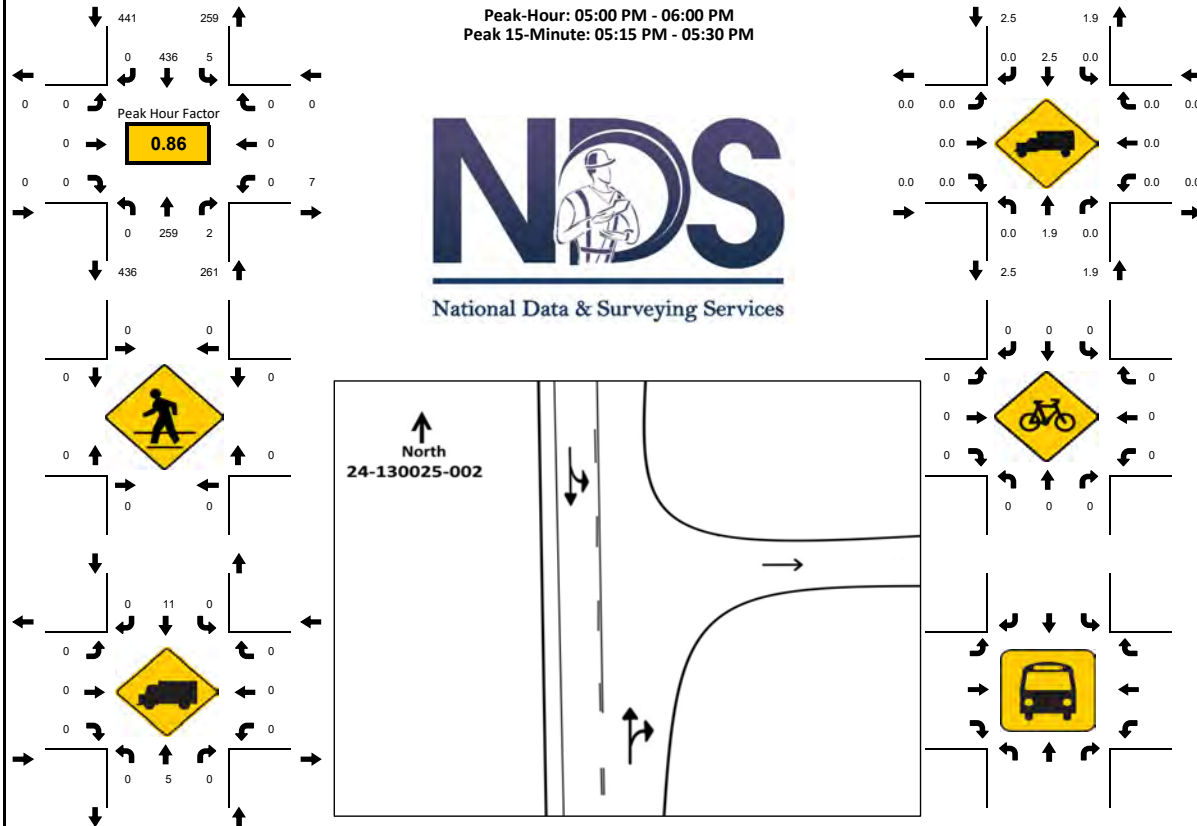
Day: Thursday
Date: 1/18/2024



PROJECT ID: 24-130025-002
DATE: Thu, Jan 18, 2024

[illegible]

PROJECT ID: 24-130025-002
DATE: Thu, Jan 18, 2024

[illegible]

National Data & Surveying Services

Intersection Turning Movement Count

Location: Lake Helen Osteen Rd & Elkcam Blvd
City: Deltona
Control: Signalized

Project ID: 24-130025-001
Date: 1/18/2024

Data - Total

| NS/EW Streets: | Lake Helen Osteen Rd | | | | Lake Helen Osteen Rd | | | | Elkcam Blvd | | | | Elkcam Blvd | | | | |
|------------------|----------------------|---------|---------|---------|----------------------|---------|---------|---------|-------------|---------|---------|---------|-------------|---------|---------|---------|-------|
| AM | NORTHBOUND | | | | SOUTHBOUND | | | | EASTBOUND | | | | WESTBOUND | | | | TOTAL |
| | 0 NL | 0 NT | 0 NR | 0 NU | 0 SL | 0 ST | 0 SR | 0 SU | 0 EL | 0 ET | 0 ER | 0 EU | 0 WL | 0 WT | 0 WR | 0 WU | |
| 7:00 AM | 3 | 45 | 2 | 0 | 2 | 34 | 26 | 0 | 21 | 17 | 0 | 0 | 24 | 64 | 4 | 0 | 242 |
| 7:15 AM | 5 | 67 | 8 | 0 | 0 | 42 | 21 | 0 | 19 | 21 | 3 | 0 | 39 | 77 | 6 | 0 | 308 |
| 7:30 AM | 0 | 61 | 11 | 0 | 2 | 60 | 32 | 0 | 18 | 22 | 3 | 0 | 22 | 63 | 2 | 0 | 296 |
| 7:45 AM | 1 | 50 | 12 | 0 | 1 | 79 | 18 | 0 | 19 | 37 | 3 | 0 | 25 | 46 | 4 | 0 | 295 |
| 8:00 AM | 1 | 24 | 15 | 0 | 3 | 43 | 25 | 0 | 26 | 44 | 5 | 0 | 22 | 67 | 4 | 0 | 279 |
| 8:15 AM | 3 | 28 | 13 | 0 | 3 | 39 | 15 | 0 | 20 | 35 | 1 | 0 | 22 | 51 | 5 | 0 | 235 |
| 8:30 AM | 3 | 34 | 9 | 0 | 1 | 42 | 17 | 0 | 14 | 32 | 4 | 0 | 15 | 51 | 2 | 0 | 224 |
| 8:45 AM | 4 | 30 | 15 | 0 | 0 | 33 | 24 | 0 | 16 | 31 | 2 | 0 | 20 | 63 | 8 | 0 | 246 |
| TOTAL VOLUMES : | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| APPROACH %'s : | 20 | 339 | 85 | 0 | 12 | 372 | 178 | 0 | 153 | 239 | 21 | 0 | 189 | 482 | 35 | 0 | 2125 |
| | 4.50% | 76.35% | 19.14% | 0.00% | 2.14% | 66.19% | 31.67% | 0.00% | 37.05% | 57.87% | 5.08% | 0.00% | 26.77% | 68.27% | 4.96% | 0.00% | |
| PEAK HR : | 07:15 AM - 08:15 AM | | | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 7 | 202 | 46 | 0 | 6 | 224 | 96 | 0 | 82 | 124 | 14 | 0 | 108 | 253 | 16 | 0 | 1178 |
| PEAK HR FACTOR : | 0.350 | 0.754 | 0.767 | 0.000 | 0.500 | 0.709 | 0.750 | 0.000 | 0.788 | 0.705 | 0.700 | 0.000 | 0.692 | 0.821 | 0.667 | 0.000 | 0.956 |
| | 0.797 | | | | 0.832 | | | | 0.733 | | | | 0.773 | | | | |
| PM | NORTHBOUND | | | | SOUTHBOUND | | | | EASTBOUND | | | | WESTBOUND | | | | TOTAL |
| | 0 NL | 0 NT | 0 NR | 0 NU | 0 SL | 0 ST | 0 SR | 0 SU | 0 EL | 0 ET | 0 ER | 0 EU | 0 WL | 0 WT | 0 WR | 0 WU | |
| 4:00 PM | 5 | 44 | 33 | 0 | 6 | 54 | 19 | 0 | 25 | 83 | 4 | 0 | 21 | 60 | 7 | 0 | 361 |
| 4:15 PM | 1 | 47 | 28 | 0 | 7 | 57 | 33 | 0 | 36 | 81 | 6 | 0 | 27 | 46 | 3 | 0 | 372 |
| 4:30 PM | 5 | 64 | 31 | 0 | 6 | 47 | 29 | 0 | 45 | 62 | 7 | 0 | 15 | 46 | 3 | 0 | 360 |
| 4:45 PM | 5 | 52 | 30 | 0 | 6 | 35 | 40 | 0 | 42 | 82 | 5 | 0 | 20 | 53 | 1 | 0 | 371 |
| 5:00 PM | 5 | 56 | 27 | 0 | 10 | 67 | 27 | 0 | 40 | 82 | 4 | 0 | 17 | 59 | 6 | 0 | 400 |
| 5:15 PM | 6 | 57 | 35 | 0 | 4 | 73 | 26 | 0 | 32 | 108 | 2 | 0 | 25 | 46 | 3 | 0 | 417 |
| 5:30 PM | 2 | 57 | 33 | 0 | 10 | 76 | 36 | 0 | 47 | 81 | 1 | 0 | 26 | 52 | 3 | 0 | 424 |
| 5:45 PM | 6 | 57 | 40 | 0 | 8 | 64 | 23 | 0 | 35 | 79 | 7 | 0 | 19 | 49 | 2 | 0 | 389 |
| TOTAL VOLUMES : | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| APPROACH %'s : | 35 | 434 | 257 | 0 | 57 | 473 | 233 | 0 | 302 | 658 | 36 | 0 | 170 | 411 | 28 | 0 | 3094 |
| | 4.82% | 59.78% | 35.40% | 0.00% | 7.47% | 61.99% | 30.54% | 0.00% | 30.32% | 66.06% | 3.61% | 0.00% | 27.91% | 67.49% | 4.60% | 0.00% | |
| PEAK HR : | 05:00 PM - 06:00 PM | | | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 19 | 227 | 135 | 0 | 32 | 280 | 112 | 0 | 154 | 350 | 14 | 0 | 87 | 206 | 14 | 0 | 1630 |
| PEAK HR FACTOR : | 0.792 | 0.996 | 0.844 | 0.000 | 0.800 | 0.921 | 0.778 | 0.000 | 0.819 | 0.810 | 0.500 | 0.000 | 0.837 | 0.873 | 0.583 | 0.000 | 0.961 |
| | 0.925 | | | | 0.869 | | | | 0.912 | | | | 0.936 | | | | |
| | 0% | 3% | 4% | #DIV/0! | 0% | 4% | 4% | #DIV/0! | 2% | 2% | 21% | #DIV/0! | 3% | 2% | 6% | #DIV/0! | |
| | 0% | 2% | 1% | #DIV/0! | 3% | 1% | 2% | #DIV/0! | 0% | 1% | 0% | #DIV/0! | 0% | 1% | 0% | #DIV/0! | |

National Data & Surveying Services

Intersection Turning Movement Count

Location: Lake Helen Osteen Rd & Elkcam Blvd
City: Deltona
Control: Signalized

Project ID: 24-130025-001
Date: 1/18/2024

Data - Cars

| NS/EW Streets: | Lake Helen Osteen Rd | | | | Lake Helen Osteen Rd | | | | Elkcam Blvd | | | | Elkcam Blvd | | | | |
|------------------|----------------------|-----------|----------|---------|----------------------|-----------|-----------|---------|-------------|-----------|----------|---------|-------------|-----------|----------|---------|---------------|
| AM | NORTHBOUND | | | | SOUTHBOUND | | | | EASTBOUND | | | | WESTBOUND | | | | TOTAL |
| | 0 NL | 0 NT | 0 NR | 0 NU | 0 SL | 0 ST | 0 SR | 0 SU | 0 EL | 0 ET | 0 ER | 0 EU | 0 WL | 0 WT | 0 WR | 0 WU | |
| 7:00 AM | 2 | 44 | 2 | 0 | 1 | 33 | 26 | 0 | 21 | 17 | 0 | 0 | 24 | 63 | 3 | 0 | 236 |
| 7:15 AM | 5 | 66 | 7 | 0 | 0 | 40 | 21 | 0 | 19 | 21 | 2 | 0 | 39 | 75 | 6 | 0 | 301 |
| 7:30 AM | 0 | 61 | 11 | 0 | 2 | 58 | 28 | 0 | 17 | 22 | 3 | 0 | 22 | 62 | 2 | 0 | 288 |
| 7:45 AM | 1 | 46 | 11 | 0 | 1 | 76 | 18 | 0 | 19 | 34 | 3 | 0 | 24 | 46 | 4 | 0 | 283 |
| 8:00 AM | 1 | 22 | 15 | 0 | 3 | 41 | 25 | 0 | 25 | 44 | 3 | 0 | 20 | 66 | 3 | 0 | 268 |
| 8:15 AM | 3 | 26 | 11 | 0 | 2 | 37 | 14 | 0 | 18 | 31 | 1 | 0 | 22 | 48 | 5 | 0 | 218 |
| 8:30 AM | 3 | 33 | 8 | 0 | 1 | 39 | 17 | 0 | 14 | 30 | 4 | 0 | 14 | 49 | 1 | 0 | 213 |
| 8:45 AM | 4 | 29 | 13 | 0 | 0 | 30 | 23 | 0 | 16 | 30 | 1 | 0 | 19 | 60 | 8 | 0 | 233 |
| TOTAL VOLUMES : | NL 19 | NT 327 | NR 78 | NU 0 | SL 10 | ST 354 | SR 172 | SU 0 | EL 149 | ET 229 | ER 17 | EU 0 | WL 184 | WT 469 | WR 32 | WU 0 | TOTAL 2040 |
| APPROACH %'s : | 4.48% | 77.12% | 18.40% | 0.00% | 1.87% | 66.04% | 32.09% | 0.00% | 37.72% | 57.97% | 4.30% | 0.00% | 26.86% | 68.47% | 4.67% | 0.00% | |
| PEAK HR : | 07:15 AM - 08:15 AM | | | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 7 | 195 | 44 | 0 | 6 | 215 | 92 | 0 | 80 | 121 | 11 | 0 | 105 | 249 | 15 | 0 | 1140 |
| PEAK HR FACTOR : | 0.350 | 0.739 | 0.733 | 0.000 | 0.500 | 0.707 | 0.821 | 0.000 | 0.800 | 0.688 | 0.917 | 0.000 | 0.673 | 0.830 | 0.625 | 0.000 | 0.947 |
| | 0.788 | | | | 0.824 | | | | 0.736 | | | | 0.769 | | | | |

| PM | NORTHBOUND | | | | SOUTHBOUND | | | | EASTBOUND | | | | WESTBOUND | | | | TOTAL |
|------------------|---------------------|-----------|-----------|---------|------------|-----------|-----------|---------|-----------|-----------|----------|---------|-----------|-----------|----------|---------|---------------|
| | 0 NL | 0 NT | 0 NR | 0 NU | 0 SL | 0 ST | 0 SR | 0 SU | 0 EL | 0 ET | 0 ER | 0 EU | 0 WL | 0 WT | 0 WR | 0 WU | |
| 4:00 PM | 5 | 43 | 33 | 0 | 6 | 52 | 19 | 0 | 25 | 83 | 3 | 0 | 20 | 59 | 7 | 0 | 355 |
| 4:15 PM | 1 | 46 | 27 | 0 | 6 | 57 | 32 | 0 | 35 | 79 | 6 | 0 | 26 | 44 | 3 | 0 | 362 |
| 4:30 PM | 5 | 62 | 30 | 0 | 6 | 47 | 29 | 0 | 45 | 60 | 6 | 0 | 15 | 46 | 3 | 0 | 354 |
| 4:45 PM | 5 | 51 | 29 | 0 | 4 | 34 | 40 | 0 | 40 | 81 | 5 | 0 | 19 | 52 | 1 | 0 | 361 |
| 5:00 PM | 5 | 55 | 26 | 0 | 9 | 67 | 27 | 0 | 40 | 81 | 4 | 0 | 17 | 58 | 6 | 0 | 395 |
| 5:15 PM | 6 | 55 | 35 | 0 | 4 | 70 | 24 | 0 | 32 | 108 | 2 | 0 | 25 | 45 | 3 | 0 | 409 |
| 5:30 PM | 2 | 56 | 32 | 0 | 10 | 75 | 36 | 0 | 47 | 79 | 1 | 0 | 26 | 52 | 3 | 0 | 419 |
| 5:45 PM | 6 | 57 | 40 | 0 | 8 | 64 | 23 | 0 | 35 | 78 | 7 | 0 | 19 | 49 | 2 | 0 | 388 |
| TOTAL VOLUMES : | NL 35 | NT 425 | NR 252 | NU 0 | SL 53 | ST 466 | SR 230 | SU 0 | EL 299 | ET 649 | ER 34 | EU 0 | WL 167 | WT 405 | WR 28 | WU 0 | TOTAL 3043 |
| APPROACH %'s : | 4.92% | 59.69% | 35.39% | 0.00% | 7.08% | 62.22% | 30.71% | 0.00% | 30.45% | 66.09% | 3.46% | 0.00% | 27.83% | 67.50% | 4.67% | 0.00% | |
| PEAK HR : | 05:00 PM - 06:00 PM | | | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 19 | 223 | 133 | 0 | 31 | 276 | 110 | 0 | 154 | 346 | 14 | 0 | 87 | 204 | 14 | 0 | 1611 |
| PEAK HR FACTOR : | 0.792 | 0.978 | 0.831 | 0.000 | 0.775 | 0.920 | 0.764 | 0.000 | 0.819 | 0.801 | 0.500 | 0.000 | 0.837 | 0.879 | 0.583 | 0.000 | 0.961 |
| | 0.910 | | | | 0.862 | | | | 0.905 | | | | 0.941 | | | | |

National Data & Surveying Services

Intersection Turning Movement Count

Location: Lake Helen Osteen Rd & Elkcam Blvd
City: Deltona
Control: Signalized

Project ID: 24-130025-001
Date: 1/18/2024

Data - HT

| NS/EW Streets: | Lake Helen Osteen Rd | | | | Lake Helen Osteen Rd | | | | Elkcam Blvd | | | | Elkcam Blvd | | | | |
|------------------|----------------------|---------|---------|---------|----------------------|---------|---------|---------|-------------|---------|---------|---------|-------------|---------|---------|---------|-------|
| AM | NORTHBOUND | | | | SOUTHBOUND | | | | EASTBOUND | | | | WESTBOUND | | | | TOTAL |
| | 0 NL | 0 NT | 0 NR | 0 NU | 0 SL | 0 ST | 0 SR | 0 SU | 0 EL | 0 ET | 0 ER | 0 EU | 0 WL | 0 WT | 0 WR | 0 WU | |
| 7:00 AM | 1 | 1 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 6 |
| 7:15 AM | 0 | 1 | 1 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 2 | 0 | 0 | 7 |
| 7:30 AM | 0 | 0 | 0 | 0 | 0 | 2 | 4 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 8 |
| 7:45 AM | 0 | 4 | 1 | 0 | 0 | 3 | 0 | 0 | 0 | 3 | 0 | 0 | 1 | 0 | 0 | 0 | 12 |
| 8:00 AM | 0 | 2 | 0 | 0 | 0 | 2 | 0 | 0 | 1 | 0 | 2 | 0 | 2 | 1 | 1 | 0 | 11 |
| 8:15 AM | 0 | 2 | 2 | 0 | 1 | 2 | 1 | 0 | 2 | 4 | 0 | 0 | 0 | 3 | 0 | 0 | 17 |
| 8:30 AM | 0 | 1 | 1 | 0 | 0 | 3 | 0 | 0 | 0 | 2 | 0 | 0 | 1 | 2 | 1 | 0 | 11 |
| 8:45 AM | 0 | 1 | 2 | 0 | 0 | 3 | 1 | 0 | 0 | 1 | 1 | 0 | 1 | 3 | 0 | 0 | 13 |
| TOTAL VOLUMES : | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| APPROACH %'s : | 1 | 12 | 7 | 0 | 2 | 18 | 6 | 0 | 4 | 10 | 4 | 0 | 5 | 13 | 3 | 0 | 85 |
| | 5.00% | 60.00% | 35.00% | 0.00% | 7.69% | 69.23% | 23.08% | 0.00% | 22.22% | 55.56% | 22.22% | 0.00% | 23.81% | 61.90% | 14.29% | 0.00% | |
| PEAK HR : | 07:15 AM - 08:15 AM | | | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 0 | 7 | 2 | 0 | 0 | 9 | 4 | 0 | 2 | 3 | 3 | 0 | 3 | 4 | 1 | 0 | 38 |
| PEAK HR FACTOR : | 0.000 | 0.438 | 0.500 | 0.000 | 0.000 | 0.750 | 0.250 | 0.000 | 0.500 | 0.250 | 0.375 | 0.000 | 0.375 | 0.500 | 0.250 | 0.000 | 0.792 |
| | | | 0.450 | | | | 0.542 | | | | 0.667 | | | | 0.500 | | |
| PM | NORTHBOUND | | | | SOUTHBOUND | | | | EASTBOUND | | | | WESTBOUND | | | | TOTAL |
| | 0 NL | 0 NT | 0 NR | 0 NU | 0 SL | 0 ST | 0 SR | 0 SU | 0 EL | 0 ET | 0 ER | 0 EU | 0 WL | 0 WT | 0 WR | 0 WU | |
| 4:00 PM | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 0 | 6 |
| 4:15 PM | 0 | 1 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | 2 | 0 | 0 | 1 | 2 | 0 | 0 | 10 |
| 4:30 PM | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 6 |
| 4:45 PM | 0 | 1 | 1 | 0 | 2 | 1 | 0 | 0 | 2 | 1 | 0 | 0 | 1 | 1 | 0 | 0 | 10 |
| 5:00 PM | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 5 |
| 5:15 PM | 0 | 2 | 0 | 0 | 0 | 3 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 8 |
| 5:30 PM | 0 | 1 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| TOTAL VOLUMES : | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| APPROACH %'s : | 0 | 9 | 5 | 0 | 4 | 7 | 3 | 0 | 3 | 9 | 2 | 0 | 3 | 6 | 0 | 0 | 51 |
| | 0.00% | 64.29% | 35.71% | 0.00% | 28.57% | 50.00% | 21.43% | 0.00% | 21.43% | 64.29% | 14.29% | 0.00% | 33.33% | 66.67% | 0.00% | 0.00% | |
| PEAK HR : | 05:00 PM - 06:00 PM | | | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 0 | 4 | 2 | 0 | 1 | 4 | 2 | 0 | 0 | 4 | 0 | 0 | 0 | 2 | 0 | 0 | 19 |
| PEAK HR FACTOR : | 0.000 | 0.500 | 0.500 | 0.000 | 0.250 | 0.333 | 0.250 | 0.000 | 0.000 | 0.500 | 0.000 | 0.000 | 0.000 | 0.500 | 0.000 | 0.000 | 0.594 |
| | | | 0.750 | | | | 0.350 | | | | 0.500 | | | | 0.500 | | |

Location: Lake Helen Osteen Rd & Elkcam Blvd
City: Deltona
Control: Signalized

Project ID: 24-130025-001
Date: 1/18/2024

| NS/EW Streets: | | Lake Helen Osten Rd | | | | Lake Helen Osten Rd | | | | Elkcam Blvd | | | | Elkcam Blvd | | | | |
|-----------------------------------|---------|---------------------|------------------|------------------|------------------|---------------------|------------------|--------------------|------------------|------------------|------------------|------------------|------------------|------------------|-------------------|-------------------|------------------|------------|
| AM | | NORTHBOUND | | | | SOUTHBOUND | | | | EASTBOUND | | | | WESTBOUND | | | | |
| | | O | O | O | O | O | O | O | O | O | O | O | O | O | O | O | | |
| | | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| | 7:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 |
| | 7:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 7:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 7:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 8:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 8:15 AM | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 5 |
| | 8:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| | 8:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| TOTAL VOLUMES : APPROACH %'s : | | NL 1 100.00% | NT 0 0.00% | NR 0 0.00% | NU 0 0.00% | SL 0 0.00% | ST 0 0.00% | SR 2 100.00% | SU 0 0.00% | EL 0 0.00% | ET 0 0.00% | ER 0 0.00% | EU 0 0.00% | WL 0 0.00% | WT 3 75.00% | WR 1 25.00% | WU 0 0.00% | TOTAL 7 |
| PEAK HR : | | 07:15 AM - 08:15 AM | | | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | | 0 | | | | 0 | | | | 0 | | | | 0 | | | | 0 |
| PEAK HR FACTOR : | | 0.000 | | | | 0.000 | | | | 0.000 | | | | 0.000 | | | | 0.000 |

| PM | | NORTHBOUND | | | | SOUTHBOUND | | | | EASTBOUND | | | | WESTBOUND | | | | |
|-----------------------------------|---------|---------------------|------------------|------------------|------------------|------------------|------------------|--------------------|------------------|-------------------|-------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------|
| | | O | O | O | O | O | O | O | O | O | O | O | O | O | O | O | | |
| | | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| | 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| | 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| | 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| TOTAL VOLUMES : APPROACH %'s : | | NL 0 0.00% | NT 0 0.00% | NR 0 0.00% | NU 0 0.00% | SL 0 0.00% | ST 0 0.00% | SR 1 100.00% | SU 0 0.00% | EL 1 50.00% | ET 1 50.00% | ER 0 0.00% | EU 0 0.00% | WL 0 0.00% | WT 0 0.00% | WR 0 0.00% | WU 0 0.00% | TOTAL 3 |
| PEAK HR : | | 05:00 PM - 06:00 PM | | | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | | 0 | | | | 0 | | | | 0 | | | | 0 | | | | 0 |
| PEAK HR FACTOR : | | 0.000 | | | | 0.000 | | | | 0.000 | | | | 0.000 | | | | 0.000 |

Project ID: 24-130025-001
Date: 1/18/2024

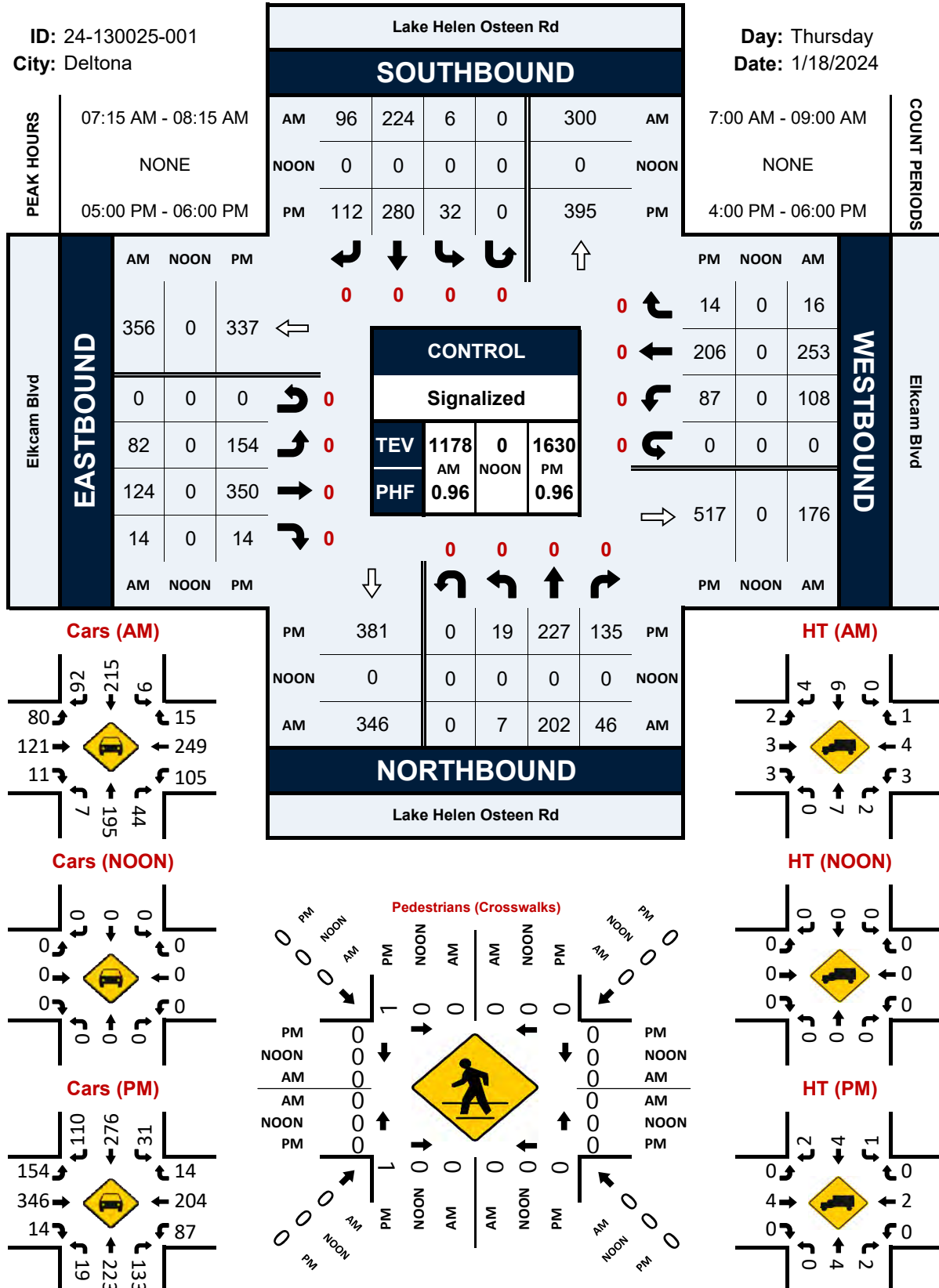
| PM | NORTH LEG | | SOUTH LEG | | EAST LEG | | WEST LEG | | TOTAL |
|------------------|---------------------|-------|-----------|-------|----------|----|----------|--------|-------|
| | EB | WB | EB | WB | NB | SB | NB | SB | |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 5:45 PM | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 |
| TOTAL VOLUMES : | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| APPROACH %'s : | 1 | 0 | 1 | 0 | 0 | 0 | 1 | 1 | 4 |
| | 100.00% | 0.00% | 100.00% | 0.00% | | | 50.00% | 50.00% | |
| PEAK HR : | 05:00 PM - 06:00 PM | | | | | | | | TOTAL |
| PEAK HR VOL : | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 |
| PEAK HR FACTOR : | 0.250 | | 0.250 | | | | | | 0.500 |
| | 0.250 | | 0.250 | | | | | | |

Lake Helen Osteen Rd & Elkcarn Blvd

Peak Hour Turning Movement Count

ID: 24-130025-001
City: Deltona

Day: Thursday
Date: 1/18/2024



PROJECT ID: 24-130025-001
DATE: Thu, Jan 18, 2024

[illegible]

PROJECT ID: 24-130025-001
DATE: Thu, Jan 18, 2024

[illegible]

2022 PEAK SEASON FACTOR CATEGORY REPORT - REPORT TYPE: ALL
 CATEGORY: 7900 VOLUSIA COUNTYWIDE

| WEEK | DATES | SF | MOCF: 0.94 PSCF |
|------|-------------------------|------|--------------------|
| 1 | 01/01/2022 - 01/01/2022 | 1.02 | 1.09 |
| 2 | 01/02/2022 - 01/08/2022 | 1.03 | 1.10 |
| 3 | 01/09/2022 - 01/15/2022 | 1.04 | 1.11 |
| 4 | 01/16/2022 - 01/22/2022 | 1.02 | 1.09 |
| 5 | 01/23/2022 - 01/29/2022 | 1.01 | 1.07 |
| 6 | 01/30/2022 - 02/05/2022 | 0.99 | 1.05 |
| * 7 | 02/06/2022 - 02/12/2022 | 0.97 | 1.03 |
| * 8 | 02/13/2022 - 02/19/2022 | 0.95 | 1.01 |
| * 9 | 02/20/2022 - 02/26/2022 | 0.94 | 1.00 |
| *10 | 02/27/2022 - 03/05/2022 | 0.93 | 0.99 |
| *11 | 03/06/2022 - 03/12/2022 | 0.92 | 0.98 |
| *12 | 03/13/2022 - 03/19/2022 | 0.91 | 0.97 |
| *13 | 03/20/2022 - 03/26/2022 | 0.92 | 0.98 |
| *14 | 03/27/2022 - 04/02/2022 | 0.93 | 0.99 |
| *15 | 04/03/2022 - 04/09/2022 | 0.94 | 1.00 |
| *16 | 04/10/2022 - 04/16/2022 | 0.96 | 1.02 |
| *17 | 04/17/2022 - 04/23/2022 | 0.96 | 1.02 |
| *18 | 04/24/2022 - 04/30/2022 | 0.97 | 1.03 |
| *19 | 05/01/2022 - 05/07/2022 | 0.98 | 1.04 |
| 20 | 05/08/2022 - 05/14/2022 | 0.98 | 1.04 |
| 21 | 05/15/2022 - 05/21/2022 | 0.99 | 1.05 |
| 22 | 05/22/2022 - 05/28/2022 | 1.00 | 1.06 |
| 23 | 05/29/2022 - 06/04/2022 | 1.02 | 1.09 |
| 24 | 06/05/2022 - 06/11/2022 | 1.03 | 1.10 |
| 25 | 06/12/2022 - 06/18/2022 | 1.04 | 1.11 |
| 26 | 06/19/2022 - 06/25/2022 | 1.05 | 1.12 |
| 27 | 06/26/2022 - 07/02/2022 | 1.06 | 1.13 |
| 28 | 07/03/2022 - 07/09/2022 | 1.06 | 1.13 |
| 29 | 07/10/2022 - 07/16/2022 | 1.07 | 1.14 |
| 30 | 07/17/2022 - 07/23/2022 | 1.06 | 1.13 |
| 31 | 07/24/2022 - 07/30/2022 | 1.05 | 1.12 |
| 32 | 07/31/2022 - 08/06/2022 | 1.04 | 1.11 |
| 33 | 08/07/2022 - 08/13/2022 | 1.03 | 1.10 |
| 34 | 08/14/2022 - 08/20/2022 | 1.02 | 1.09 |
| 35 | 08/21/2022 - 08/27/2022 | 1.04 | 1.11 |
| 36 | 08/28/2022 - 09/03/2022 | 1.05 | 1.12 |
| 37 | 09/04/2022 - 09/10/2022 | 1.06 | 1.13 |
| 38 | 09/11/2022 - 09/17/2022 | 1.07 | 1.14 |
| 39 | 09/18/2022 - 09/24/2022 | 1.05 | 1.12 |
| 40 | 09/25/2022 - 10/01/2022 | 1.02 | 1.09 |
| 41 | 10/02/2022 - 10/08/2022 | 0.99 | 1.05 |
| 42 | 10/09/2022 - 10/15/2022 | 0.97 | 1.03 |
| 43 | 10/16/2022 - 10/22/2022 | 0.98 | 1.04 |
| 44 | 10/23/2022 - 10/29/2022 | 0.99 | 1.05 |
| 45 | 10/30/2022 - 11/05/2022 | 1.01 | 1.07 |
| 46 | 11/06/2022 - 11/12/2022 | 1.02 | 1.09 |
| 47 | 11/13/2022 - 11/19/2022 | 1.04 | 1.11 |
| 48 | 11/20/2022 - 11/26/2022 | 1.03 | 1.10 |
| 49 | 11/27/2022 - 12/03/2022 | 1.03 | 1.10 |
| 50 | 12/04/2022 - 12/10/2022 | 1.02 | 1.09 |
| 51 | 12/11/2022 - 12/17/2022 | 1.02 | 1.09 |
| 52 | 12/18/2022 - 12/24/2022 | 1.03 | 1.10 |
| 53 | 12/25/2022 - 12/31/2022 | 1.04 | 1.11 |

* PEAK SEASON

23-FEB-2023 09:11:23

830UPD

5_7900_PKSEASON.TXT

Appendix D

Existing Conditions Synchro Printouts



Timings

101: Catalina Blvd & Howland Blvd

02/29/2024



| Lane Group | SEL | SET | NWL | NWT | NEL | NET | SWL | SWT | SWR |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | | | |
| Traffic Volume (vph) | 118 | 523 | 30 | 997 | 108 | 108 | 126 | 99 | 497 |
| Future Volume (vph) | 118 | 523 | 30 | 997 | 108 | 108 | 126 | 99 | 497 |
| Turn Type | pm+pt | NA | pm+pt | NA | pm+pt | NA | Perm | NA | Perm |
| Protected Phases | 1 | 6 | 5 | 2 | 7 | 4 | | 8 | |
| Permitted Phases | 6 | | 2 | | 4 | | 8 | | 8 |
| Detector Phase | 1 | 6 | 5 | 2 | 7 | 4 | 8 | 8 | 8 |
| Switch Phase | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 11.0 | 5.0 | 11.0 | 5.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Minimum Split (s) | 13.5 | 19.5 | 13.5 | 19.5 | 12.0 | 14.0 | 14.0 | 14.0 | 14.0 |
| Total Split (s) | 24.0 | 65.0 | 18.0 | 59.0 | 24.0 | 67.0 | 43.0 | 43.0 | 43.0 |
| Total Split (%) | 16.0% | 43.3% | 12.0% | 39.3% | 16.0% | 44.7% | 28.7% | 28.7% | 28.7% |
| Yellow Time (s) | 5.0 | 5.0 | 5.0 | 5.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 8.5 | 8.5 | 8.5 | 8.5 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Lead/Lag | Lead | Lag | Lead | Lag | Lead | | Lag | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | | Yes | Yes | Yes |
| Recall Mode | None | Max | None | Max | None | None | None | None | None |
| Act Effect Green (s) | 69.5 | 62.1 | 58.2 | 51.4 | 49.3 | 49.3 | 28.9 | 28.9 | 28.9 |
| Actuated g/C Ratio | 0.51 | 0.46 | 0.43 | 0.38 | 0.36 | 0.36 | 0.21 | 0.21 | 0.21 |
| v/c Ratio | 0.59 | 0.38 | 0.08 | 0.86 | 0.25 | 0.23 | 0.51 | 0.26 | 0.93 |
| Control Delay | 33.1 | 28.2 | 19.9 | 48.4 | 30.5 | 27.8 | 55.1 | 46.8 | 47.5 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 33.1 | 28.2 | 19.9 | 48.4 | 30.5 | 27.8 | 55.1 | 46.8 | 47.5 |
| LOS | C | C | B | D | C | C | E | D | D |
| Approach Delay | | 29.0 | | 47.6 | | 29.0 | | 48.7 | |
| Approach LOS | | C | | D | | C | | D | |

Intersection Summary

Cycle Length: 150

Actuated Cycle Length: 136

Natural Cycle: 90

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.93

Intersection Signal Delay: 41.6

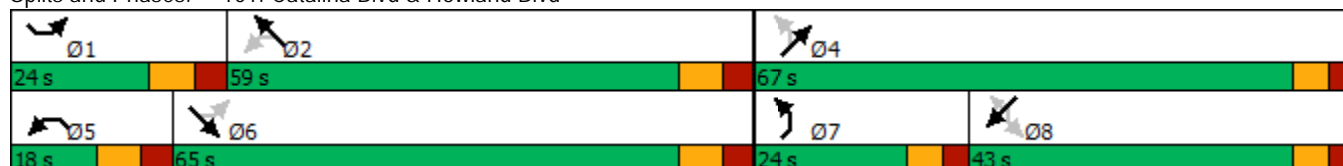
Intersection LOS: D

Intersection Capacity Utilization 85.5%

ICU Level of Service E

Analysis Period (min) 15






















Splits and Phases: 101: Catalina Blvd & Howland Blvd



HCM 6th Signalized Intersection Summary

101: Catalina Blvd & Howland Blvd

02/29/2024

| |  |  |  |  |  |  |  |  |  |  |  |  |
|------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | SEL | SET | SER | NWL | NWT | NWR | NEL | NET | NER | SWL | SWT | SWR |
| Lane Configurations |  |  | |  |  | |  |  | |  |  |  |
| Traffic Volume (veh/h) | 118 | 523 | 32 | 30 | 997 | 77 | 108 | 108 | 35 | 126 | 99 | 497 |
| Future Volume (veh/h) | 118 | 523 | 32 | 30 | 997 | 77 | 108 | 108 | 35 | 126 | 99 | 497 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | No | | | | No | | | | No | | | |
| Adj Sat Flow, veh/h/ln | 1841 | 1826 | 1856 | 1870 | 1856 | 1856 | 1885 | 1885 | 1856 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 124 | 551 | 34 | 32 | 1049 | 81 | 114 | 114 | 37 | 133 | 104 | 472 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh, % | 4 | 5 | 3 | 2 | 3 | 3 | 1 | 1 | 3 | 2 | 2 | 2 |
| Cap, veh/h | 205 | 1388 | 86 | 350 | 1282 | 99 | 349 | 515 | 167 | 383 | 498 | 422 |
| Arrive On Green | 0.06 | 0.42 | 0.42 | 0.03 | 0.39 | 0.39 | 0.06 | 0.38 | 0.38 | 0.27 | 0.27 | 0.27 |
| Sat Flow, veh/h | 1753 | 3319 | 204 | 1781 | 3316 | 256 | 1795 | 1363 | 442 | 1236 | 1870 | 1585 |
| Grp Volume(v), veh/h | 124 | 288 | 297 | 32 | 557 | 573 | 114 | 0 | 151 | 133 | 104 | 472 |
| Grp Sat Flow(s),veh/h/ln | 1753 | 1735 | 1789 | 1781 | 1763 | 1809 | 1795 | 0 | 1806 | 1236 | 1870 | 1585 |
| Q Serve(g_s), s | 5.7 | 15.6 | 15.7 | 1.5 | 38.3 | 38.4 | 6.0 | 0.0 | 7.7 | 11.9 | 5.8 | 36.0 |
| Cycle Q Clear(g_c), s | 5.7 | 15.6 | 15.7 | 1.5 | 38.3 | 38.4 | 6.0 | 0.0 | 7.7 | 11.9 | 5.8 | 36.0 |
| Prop In Lane | 1.00 | | 0.11 | 1.00 | | 0.14 | 1.00 | | 0.25 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 205 | 726 | 748 | 350 | 681 | 699 | 349 | 0 | 683 | 383 | 498 | 422 |
| V/C Ratio(X) | 0.61 | 0.40 | 0.40 | 0.09 | 0.82 | 0.82 | 0.33 | 0.00 | 0.22 | 0.35 | 0.21 | 1.12 |
| Avail Cap(c_a), veh/h | 305 | 726 | 748 | 430 | 681 | 699 | 468 | 0 | 802 | 383 | 498 | 422 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 29.7 | 27.4 | 27.4 | 24.3 | 37.2 | 37.2 | 31.6 | 0.0 | 28.5 | 40.7 | 38.5 | 49.5 |
| Incr Delay (d2), s/veh | 2.9 | 1.6 | 1.6 | 0.1 | 10.5 | 10.3 | 0.5 | 0.0 | 0.2 | 0.5 | 0.2 | 79.7 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 2.5 | 6.6 | 6.8 | 0.6 | 17.9 | 18.3 | 2.7 | 0.0 | 3.4 | 3.7 | 2.7 | 23.5 |
| Unsig. Movement Delay, s/veh | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 32.6 | 29.0 | 29.0 | 24.4 | 47.7 | 47.5 | 32.1 | 0.0 | 28.7 | 41.3 | 38.7 | 129.2 |
| LnGrp LOS | C | C | C | C | D | D | C | A | C | D | D | F |
| Approach Vol, veh/h | 709 | | | | 1162 | | | | 265 | | | |
| Approach Delay, s/veh | 29.6 | | | | 47.0 | | | | 30.1 | | | |
| Approach LOS | C | | | | D | | | | C | | | |
| Timer - Assigned Phs | 1 | 2 | | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 16.3 | 60.7 | | 58.1 | 12.0 | 65.0 | 15.1 | 43.0 | | | | |
| Change Period (Y+Rc), s | 8.5 | 8.5 | | 7.0 | 8.5 | 8.5 | 7.0 | 7.0 | | | | |
| Max Green Setting (Gmax), s | 15.5 | 50.5 | | 60.0 | 9.5 | 56.5 | 17.0 | 36.0 | | | | |
| Max Q Clear Time (g_c+I1), s | 7.7 | 40.4 | | 9.7 | 3.5 | 17.7 | 8.0 | 38.0 | | | | |
| Green Ext Time (p_c), s | 0.2 | 4.8 | | 1.0 | 0.0 | 3.4 | 0.2 | 0.0 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | 54.2 | | | | | | | | | | | |
| HCM 6th LOS | D | | | | | | | | | | | |

Timings

102: Lake Helen Osteen & Catalina Blvd

02/29/2024



| Lane Group | EBL | EBR | NBL | NBT | SBT |
|----------------------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | |
| Traffic Volume (vph) | 55 | 109 | 426 | 392 | 203 |
| Future Volume (vph) | 55 | 109 | 426 | 392 | 203 |
| Turn Type | Prot | Prot | pm+pt | NA | NA |
| Protected Phases | 8 | 8 | 1 | 6 | 2 |
| Permitted Phases | | | 6 | | |
| Detector Phase | 8 | 8 | 1 | 6 | 2 |
| Switch Phase | | | | | |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 15.0 | 15.0 |
| Minimum Split (s) | 11.5 | 11.5 | 11.5 | 21.5 | 21.5 |
| Total Split (s) | 26.5 | 26.5 | 26.5 | 63.0 | 36.5 |
| Total Split (%) | 29.6% | 29.6% | 29.6% | 70.4% | 40.8% |
| Yellow Time (s) | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.5 | 6.5 | 6.5 | 6.5 | 6.5 |
| Lead/Lag | | | Lead | | Lag |
| Lead-Lag Optimize? | | | Yes | | Yes |
| Recall Mode | None | None | None | Min | Min |
| Act Effect Green (s) | 8.0 | 8.0 | 41.7 | 43.9 | 20.9 |
| Actuated g/C Ratio | 0.13 | 0.13 | 0.70 | 0.74 | 0.35 |
| v/c Ratio | 0.25 | 0.38 | 0.71 | 0.32 | 0.67 |
| Control Delay | 30.9 | 10.8 | 12.3 | 5.0 | 22.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 30.9 | 10.8 | 12.3 | 5.0 | 22.2 |
| LOS | C | B | B | A | C |
| Approach Delay | 17.5 | | | 8.8 | 22.2 |
| Approach LOS | B | | | A | C |

Intersection Summary

Cycle Length: 89.5

Actuated Cycle Length: 59.7

Natural Cycle: 60

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.71

Intersection Signal Delay: 13.6

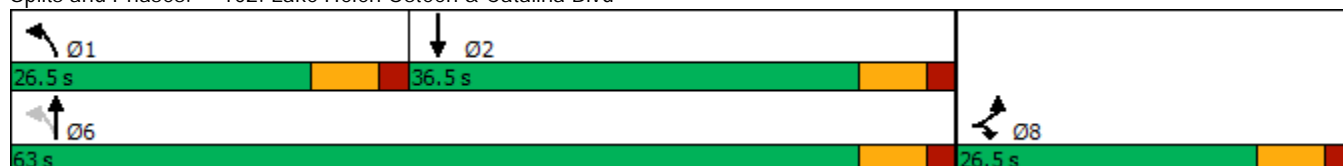
Intersection LOS: B

Intersection Capacity Utilization 65.9%

ICU Level of Service C

Analysis Period (min) 15

Splits and Phases: 102: Lake Helen Osteen & Catalina Blvd



HCM 6th Signalized Intersection Summary

102: Lake Helen Osteen & Catalina Blvd

02/29/2024






| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
|------------------------------|------|------|------|------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 55 | 109 | 426 | 392 | 203 | 183 |
| Future Volume (veh/h) | 55 | 109 | 426 | 392 | 203 | 183 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | No | | | No | No | |
| Adj Sat Flow, veh/h/ln | 1870 | 1856 | 1870 | 1856 | 1826 | 1870 |
| Adj Flow Rate, veh/h | 60 | 120 | 468 | 431 | 223 | 201 |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Percent Heavy Veh, % | 2 | 3 | 2 | 3 | 5 | 2 |
| Cap, veh/h | 197 | 174 | 591 | 1199 | 275 | 248 |
| Arrive On Green | 0.11 | 0.11 | 0.21 | 0.65 | 0.31 | 0.31 |
| Sat Flow, veh/h | 1781 | 1572 | 1781 | 1856 | 885 | 798 |
| Grp Volume(v), veh/h | 60 | 120 | 468 | 431 | 0 | 424 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 1572 | 1781 | 1856 | 0 | 1682 |
| Q Serve(g_s), s | 1.7 | 3.9 | 8.3 | 5.7 | 0.0 | 12.4 |
| Cycle Q Clear(g_c), s | 1.7 | 3.9 | 8.3 | 5.7 | 0.0 | 12.4 |
| Prop In Lane | 1.00 | 1.00 | 1.00 | | | 0.47 |
| Lane Grp Cap(c), veh/h | 197 | 174 | 591 | 1199 | 0 | 523 |
| V/C Ratio(X) | 0.30 | 0.69 | 0.79 | 0.36 | 0.00 | 0.81 |
| Avail Cap(c_a), veh/h | 667 | 589 | 878 | 1963 | 0 | 945 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 21.9 | 22.9 | 9.9 | 4.4 | 0.0 | 17.0 |
| Incr Delay (d2), s/veh | 0.9 | 4.8 | 3.0 | 0.2 | 0.0 | 3.1 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 0.7 | 1.5 | 2.3 | 1.0 | 0.0 | 4.2 |
| Unsig. Movement Delay, s/veh | | | | | | |
| LnGrp Delay(d),s/veh | 22.7 | 27.7 | 12.9 | 4.5 | 0.0 | 20.0 |
| LnGrp LOS | C | C | B | A | A | C |
| Approach Vol, veh/h | 180 | | | 899 | 424 | |
| Approach Delay, s/veh | 26.0 | | | 8.9 | 20.0 | |
| Approach LOS | C | | | A | C | |
| Timer - Assigned Phs | 1 | 2 | | | 6 | 8 |
| Phs Duration (G+Y+Rc), s | 17.9 | 23.1 | | | 41.0 | 12.4 |
| Change Period (Y+Rc), s | 6.5 | 6.5 | | | 6.5 | 6.5 |
| Max Green Setting (Gmax), s | 20.0 | 30.0 | | | 56.5 | 20.0 |
| Max Q Clear Time (g_c+I1), s | 10.3 | 14.4 | | | 7.7 | 5.9 |
| Green Ext Time (p_c), s | 1.1 | 2.2 | | | 2.6 | 0.4 |

Intersection Summary

| | |
|--------------------|------|
| HCM 6th Ctrl Delay | 14.1 |
| HCM 6th LOS | B |




HCM 6th TWSC
103: Lake Helen Osteen & Driveway #1

02/29/2024

| Intersection | | | | | | |
|--------------------------|---|--------|---|------|------|---|
| Int Delay, s/veh | 0.2 | | | | | |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations |  | |  | | |  |
| Traffic Vol, veh/h | 3 | 7 | 473 | 0 | 0 | 235 |
| Future Vol, veh/h | 3 | 7 | 473 | 0 | 0 | 235 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, # | 0 | - | 0 | - | - | 0 |
| Grade, % | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 85 | 85 | 85 | 85 | 85 | 85 |
| Heavy Vehicles, % | 2 | 2 | 3 | 2 | 2 | 4 |
| Mvmt Flow | 4 | 8 | 556 | 0 | 0 | 276 |
| Major/Minor | Minor1 | Major1 | Major2 | | | |
| Conflicting Flow All | 832 | 556 | 0 | - | - | - |
| Stage 1 | 556 | - | - | - | - | - |
| Stage 2 | 276 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | - | - | - | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | - | - | - | - |
| Pot Cap-1 Maneuver | 339 | 531 | - | 0 | 0 | - |
| Stage 1 | 574 | - | - | 0 | 0 | - |
| Stage 2 | 771 | - | - | 0 | 0 | - |
| Platoon blocked, % | | | - | | | - |
| Mov Cap-1 Maneuver | 339 | 531 | - | - | - | - |
| Mov Cap-2 Maneuver | 339 | - | - | - | - | - |
| Stage 1 | 574 | - | - | - | - | - |
| Stage 2 | 771 | - | - | - | - | - |
| Approach | WB | NB | SB | | | |
| HCM Control Delay, s | 13.1 | 0 | 0 | | | |
| HCM LOS | B | | | | | |
| Minor Lane/Major Mvmt | NBTWBLn1 | | SBT | | | |
| Capacity (veh/h) | - 454 | | - | | | |
| HCM Lane V/C Ratio | - 0.026 | | - | | | |
| HCM Control Delay (s) | - 13.1 | | - | | | |
| HCM Lane LOS | - B | | - | | | |
| HCM 95th %tile Q(veh) | - 0.1 | | - | | | |

HCM 6th TWSC
104: Lake Helen Osteen & Driveway #2

02/29/2024

| Intersection | | | | | | |
|--------------------------|---|----------|---|--------|-------|---|
| Int Delay, s/veh | 0.1 | | | | | |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations |  | |  | | |  |
| Traffic Vol, veh/h | 0 | 0 | 474 | 5 | 7 | 227 |
| Future Vol, veh/h | 0 | 0 | 474 | 5 | 7 | 227 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, # | 0 | - | 0 | - | - | 0 |
| Grade, % | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 85 | 85 | 85 | 85 | 85 | 85 |
| Heavy Vehicles, % | 2 | 2 | 3 | 2 | 2 | 4 |
| Mvmt Flow | 0 | 0 | 558 | 6 | 8 | 267 |
| Major/Minor | Minor1 | Major1 | | Major2 | | |
| Conflicting Flow All | 844 | 561 | 0 | 0 | 564 | 0 |
| Stage 1 | 561 | - | - | - | - | - |
| Stage 2 | 283 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.12 | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | - | - | 2.218 | - |
| Pot Cap-1 Maneuver | 334 | 527 | - | - | 1008 | - |
| Stage 1 | 571 | - | - | - | - | - |
| Stage 2 | 765 | - | - | - | - | - |
| Platoon blocked, % | | | - | - | | - |
| Mov Cap-1 Maneuver | 331 | 527 | - | - | 1008 | - |
| Mov Cap-2 Maneuver | 331 | - | - | - | - | - |
| Stage 1 | 571 | - | - | - | - | - |
| Stage 2 | 758 | - | - | - | - | - |
| Approach | WB | NB | | SB | | |
| HCM Control Delay, s | 0 | 0 | | 0.3 | | |
| HCM LOS | A | | | | | |
| Minor Lane/Major Mvmt | NBT | NBRWBLn1 | | SBL | SBT | |
| Capacity (veh/h) | - | - | | 1008 | - | |
| HCM Lane V/C Ratio | - | - | | 0.008 | - | |
| HCM Control Delay (s) | - | - | | 0 | 8.6 | |
| HCM Lane LOS | - | - | | A | A | |
| HCM 95th %tile Q(veh) | - | - | | 0 | - | |

Timings

105: Elkcarn Blvd & Lake Helen Osteen

02/29/2024



| Lane Group | SEL | SET | NWL | NWT | NEL | NET | SWL | SWT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | LT | RT | LT | RT | LT | RT | LT | RT |
| Traffic Volume (vph) | 6 | 228 | 7 | 206 | 84 | 126 | 110 | 258 |
| Future Volume (vph) | 6 | 228 | 7 | 206 | 84 | 126 | 110 | 258 |
| Turn Type | pm+pt | NA | pm+pt | NA | pm+pt | NA | pm+pt | NA |
| Protected Phases | 5 | 2 | 1 | 6 | 3 | 8 | 7 | 4 |
| Permitted Phases | 2 | | 6 | | 8 | | 4 | |
| Detector Phase | 5 | 2 | 1 | 6 | 3 | 8 | 7 | 4 |
| Switch Phase | | | | | | | | |
| Minimum Initial (s) | 5.0 | 16.0 | 5.0 | 16.0 | 5.0 | 6.0 | 5.0 | 6.0 |
| Minimum Split (s) | 14.0 | 25.0 | 14.0 | 25.0 | 13.5 | 13.0 | 13.5 | 13.0 |
| Total Split (s) | 29.0 | 49.0 | 29.0 | 49.0 | 28.5 | 32.0 | 28.5 | 32.0 |
| Total Split (%) | 20.9% | 35.4% | 20.9% | 35.4% | 20.6% | 23.1% | 20.6% | 23.1% |
| Yellow Time (s) | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 4.0 | 5.5 | 4.0 |
| All-Red Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 9.0 | 9.0 | 9.0 | 9.0 | 8.5 | 7.0 | 8.5 | 7.0 |
| Lead/Lag | Lead | Lag | Lead | Lag | Lead | Lag | Lead | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | Min | None | Min | None | None | None | None |
| Act Effect Green (s) | 22.3 | 21.4 | 22.3 | 21.4 | 22.6 | 16.2 | 28.2 | 22.0 |
| Actuated g/C Ratio | 0.30 | 0.28 | 0.30 | 0.28 | 0.30 | 0.22 | 0.37 | 0.29 |
| v/c Ratio | 0.02 | 0.68 | 0.02 | 0.52 | 0.23 | 0.38 | 0.24 | 0.54 |
| Control Delay | 18.5 | 32.2 | 18.6 | 28.0 | 16.9 | 30.2 | 16.3 | 30.9 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 18.5 | 32.2 | 18.6 | 28.0 | 16.9 | 30.2 | 16.3 | 30.9 |
| LOS | B | C | B | C | B | C | B | C |
| Approach Delay | | 31.9 | | 27.7 | | 25.2 | | 26.7 |
| Approach LOS | | C | | C | | C | | C |

Intersection Summary

Cycle Length: 138.5

Actuated Cycle Length: 75.3

Natural Cycle: 75

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.68

Intersection Signal Delay: 28.1

Intersection LOS: C

Intersection Capacity Utilization 57.6%

ICU Level of Service B

Analysis Period (min) 15





















Splits and Phases: 105: Elkcarn Blvd & Lake Helen Osteen

| | | | |
|------|------|--------|------|
| Ø1 | Ø2 | Ø3 | Ø4 |
| 29 s | 49 s | 28.5 s | 32 s |
| Ø5 | Ø6 | Ø7 | Ø8 |
| 29 s | 49 s | 28.5 s | 32 s |

HCM 6th Signalized Intersection Summary

105: Elkcarn Blvd & Lake Helen Osteen

02/29/2024

| |  |  |  |  |  |  |  |  |  |  |  |  |
|------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | SEL | SET | SER | NWL | NWT | NWR | NEL | NET | NER | SWL | SWT | SWR |
| Lane Configurations |  |  | |  |  | |  |  | |  |  | |
| Traffic Volume (veh/h) | 6 | 228 | 98 | 7 | 206 | 47 | 84 | 126 | 14 | 110 | 258 | 16 |
| Future Volume (veh/h) | 6 | 228 | 98 | 7 | 206 | 47 | 84 | 126 | 14 | 110 | 258 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1870 | 1841 | 1841 | 1870 | 1856 | 1841 | 1870 | 1870 | 1604 | 1856 | 1870 | 1811 |
| Adj Flow Rate, veh/h | 6 | 240 | 103 | 7 | 217 | 49 | 88 | 133 | 15 | 116 | 272 | 17 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh, % | 2 | 4 | 4 | 2 | 3 | 4 | 2 | 2 | 20 | 3 | 2 | 6 |
| Cap, veh/h | 247 | 299 | 128 | 184 | 360 | 81 | 263 | 298 | 34 | 372 | 342 | 21 |
| Arrive On Green | 0.01 | 0.24 | 0.24 | 0.01 | 0.25 | 0.25 | 0.06 | 0.18 | 0.18 | 0.08 | 0.20 | 0.20 |
| Sat Flow, veh/h | 1781 | 1222 | 524 | 1781 | 1465 | 331 | 1781 | 1651 | 186 | 1767 | 1742 | 109 |
| Grp Volume(v), veh/h | 6 | 0 | 343 | 7 | 0 | 266 | 88 | 0 | 148 | 116 | 0 | 289 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 0 | 1746 | 1781 | 0 | 1796 | 1781 | 0 | 1837 | 1767 | 0 | 1851 |
| Q Serve(g_s), s | 0.2 | 0.0 | 12.6 | 0.2 | 0.0 | 9.0 | 2.7 | 0.0 | 4.9 | 3.6 | 0.0 | 10.2 |
| Cycle Q Clear(g_c), s | 0.2 | 0.0 | 12.6 | 0.2 | 0.0 | 9.0 | 2.7 | 0.0 | 4.9 | 3.6 | 0.0 | 10.2 |
| Prop In Lane | 1.00 | | 0.30 | 1.00 | | 0.18 | 1.00 | | 0.10 | 1.00 | | 0.06 |
| Lane Grp Cap(c), veh/h | 247 | 0 | 427 | 184 | 0 | 442 | 263 | 0 | 332 | 372 | 0 | 364 |
| V/C Ratio(X) | 0.02 | 0.00 | 0.80 | 0.04 | 0.00 | 0.60 | 0.33 | 0.00 | 0.45 | 0.31 | 0.00 | 0.79 |
| Avail Cap(c_a), veh/h | 755 | 0 | 1022 | 689 | 0 | 1051 | 679 | 0 | 672 | 756 | 0 | 677 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 19.7 | 0.0 | 24.3 | 20.3 | 0.0 | 22.8 | 21.4 | 0.0 | 25.0 | 20.4 | 0.0 | 26.1 |
| Incr Delay (d2), s/veh | 0.0 | 0.0 | 3.6 | 0.1 | 0.0 | 1.3 | 0.7 | 0.0 | 0.9 | 0.5 | 0.0 | 4.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 0.1 | 0.0 | 5.2 | 0.1 | 0.0 | 3.7 | 1.1 | 0.0 | 2.1 | 1.4 | 0.0 | 4.6 |
| Unsig. Movement Delay, s/veh | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 19.8 | 0.0 | 27.8 | 20.4 | 0.0 | 24.1 | 22.2 | 0.0 | 25.9 | 20.9 | 0.0 | 30.1 |
| LnGrp LOS | B | A | C | C | A | C | C | A | C | C | A | C |
| Approach Vol, veh/h | | 349 | | | 273 | | | 236 | | | 405 | |
| Approach Delay, s/veh | | 27.7 | | | 24.0 | | | 24.5 | | | 27.5 | |
| Approach LOS | | C | | | C | | | C | | | C | |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 9.6 | 25.7 | 12.6 | 20.4 | 9.5 | 25.8 | 13.7 | 19.3 | | | | |
| Change Period (Y+Rc), s | 9.0 | 9.0 | 8.5 | 7.0 | 9.0 | 9.0 | 8.5 | 7.0 | | | | |
| Max Green Setting (Gmax), s | 20.0 | 40.0 | 20.0 | 25.0 | 20.0 | 40.0 | 20.0 | 25.0 | | | | |
| Max Q Clear Time (g_c+I1), s | 2.2 | 14.6 | 4.7 | 12.2 | 2.2 | 11.0 | 5.6 | 6.9 | | | | |
| Green Ext Time (p_c), s | 0.0 | 2.1 | 0.2 | 1.3 | 0.0 | 1.6 | 0.2 | 0.6 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 26.2 | | | | | | | | | |
| HCM 6th LOS | | | C | | | | | | | | | |

Timings

101: Catalina Blvd & Howland Blvd

02/29/2024



| Lane Group | SEL | SET | NWL | NWT | NEL | NET | SWL | SWT | SWR |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | | | |
| Traffic Volume (vph) | 408 | 1111 | 46 | 623 | 46 | 87 | 126 | 87 | 243 |
| Future Volume (vph) | 408 | 1111 | 46 | 623 | 46 | 87 | 126 | 87 | 243 |
| Turn Type | pm+pt | NA | pm+pt | NA | pm+pt | NA | Perm | NA | Perm |
| Protected Phases | 1 | 6 | 5 | 2 | 7 | 4 | | 8 | |
| Permitted Phases | 6 | | 2 | | 4 | | 8 | | 8 |
| Detector Phase | 1 | 6 | 5 | 2 | 7 | 4 | 8 | 8 | 8 |
| Switch Phase | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 11.0 | 5.0 | 11.0 | 5.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Minimum Split (s) | 13.5 | 19.5 | 13.5 | 19.5 | 12.0 | 14.0 | 14.0 | 14.0 | 14.0 |
| Total Split (s) | 30.0 | 65.0 | 20.0 | 55.0 | 20.0 | 60.0 | 45.0 | 45.0 | 45.0 |
| Total Split (%) | 20.0% | 43.3% | 13.3% | 36.7% | 13.3% | 40.0% | 30.0% | 30.0% | 30.0% |
| Yellow Time (s) | 5.0 | 5.0 | 5.0 | 5.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 8.5 | 8.5 | 8.5 | 8.5 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Lead/Lag | Lead | Lag | Lead | Lag | Lead | | Lag | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | | Yes | Yes | Yes |
| Recall Mode | None | Max | None | Max | None | None | None | None | None |
| Act Effect Green (s) | 77.3 | 65.2 | 54.0 | 47.0 | 31.4 | 31.4 | 18.7 | 18.7 | 18.7 |
| Actuated g/C Ratio | 0.62 | 0.52 | 0.43 | 0.38 | 0.25 | 0.25 | 0.15 | 0.15 | 0.15 |
| v/c Ratio | 0.85 | 0.67 | 0.21 | 0.55 | 0.16 | 0.24 | 0.69 | 0.33 | 0.57 |
| Control Delay | 33.1 | 28.2 | 17.0 | 33.9 | 34.4 | 33.3 | 69.8 | 51.0 | 10.6 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 33.1 | 28.2 | 17.0 | 33.9 | 34.4 | 33.3 | 69.8 | 51.0 | 10.6 |
| LOS | C | C | B | C | C | C | E | D | B |
| Approach Delay | | 29.4 | | 32.9 | | 33.6 | | 34.7 | |
| Approach LOS | | C | | C | | C | | C | |

Intersection Summary

Cycle Length: 150

Actuated Cycle Length: 124.4

Natural Cycle: 90

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.85

Intersection Signal Delay: 31.3

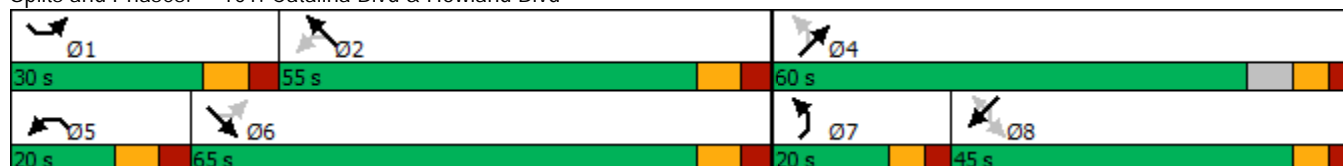
Intersection LOS: C

Intersection Capacity Utilization 75.6%

ICU Level of Service D

Analysis Period (min) 15






















Splits and Phases: 101: Catalina Blvd & Howland Blvd



HCM 6th Signalized Intersection Summary

101: Catalina Blvd & Howland Blvd

02/29/2024

| |  |  |  |  |  |  |  |  |  |  |  |  |
|------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | SEL | SET | SER | NWL | NWT | NWR | NEL | NET | NER | SWL | SWT | SWR |
| Lane Configurations |  |  | |  |  | |  |  | |  |  |  |
| Traffic Volume (veh/h) | 408 | 1111 | 61 | 46 | 623 | 67 | 46 | 87 | 19 | 126 | 87 | 243 |
| Future Volume (veh/h) | 408 | 1111 | 61 | 46 | 623 | 67 | 46 | 87 | 19 | 126 | 87 | 243 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | No | | | No | | | No | | | No | | |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1826 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1856 |
| Adj Flow Rate, veh/h | 429 | 1169 | 64 | 48 | 656 | 71 | 48 | 92 | 20 | 133 | 92 | 205 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh, % | 2 | 2 | 5 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 3 |
| Cap, veh/h | 514 | 1767 | 97 | 240 | 1265 | 137 | 242 | 371 | 81 | 261 | 293 | 246 |
| Arrive On Green | 0.16 | 0.52 | 0.52 | 0.03 | 0.39 | 0.39 | 0.03 | 0.25 | 0.25 | 0.16 | 0.16 | 0.16 |
| Sat Flow, veh/h | 1781 | 3426 | 187 | 1781 | 3235 | 350 | 1781 | 1489 | 324 | 1281 | 1870 | 1572 |
| Grp Volume(v), veh/h | 429 | 606 | 627 | 48 | 360 | 367 | 48 | 0 | 112 | 133 | 92 | 205 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 1777 | 1837 | 1781 | 1777 | 1807 | 1781 | 0 | 1812 | 1281 | 1870 | 1572 |
| Q Serve(g_s), s | 16.4 | 29.8 | 29.9 | 1.9 | 18.4 | 18.5 | 2.6 | 0.0 | 5.9 | 11.6 | 5.2 | 15.0 |
| Cycle Q Clear(g_c), s | 16.4 | 29.8 | 29.9 | 1.9 | 18.4 | 18.5 | 2.6 | 0.0 | 5.9 | 11.6 | 5.2 | 15.0 |
| Prop In Lane | 1.00 | | 0.10 | 1.00 | | 0.19 | 1.00 | | 0.18 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 514 | 917 | 947 | 240 | 695 | 707 | 242 | 0 | 451 | 261 | 293 | 246 |
| V/C Ratio(X) | 0.83 | 0.66 | 0.66 | 0.20 | 0.52 | 0.52 | 0.20 | 0.00 | 0.25 | 0.51 | 0.31 | 0.83 |
| Avail Cap(c_a), veh/h | 554 | 917 | 947 | 352 | 695 | 707 | 378 | 0 | 808 | 470 | 598 | 502 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 19.0 | 21.2 | 21.2 | 21.3 | 27.7 | 27.7 | 38.7 | 0.0 | 35.8 | 47.2 | 44.5 | 48.6 |
| Incr Delay (d2), s/veh | 10.1 | 3.7 | 3.6 | 0.4 | 2.8 | 2.7 | 0.4 | 0.0 | 0.3 | 1.5 | 0.6 | 7.1 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 7.5 | 12.4 | 12.8 | 0.8 | 8.0 | 8.2 | 1.2 | 0.0 | 2.7 | 3.8 | 2.5 | 6.4 |
| Unsig. Movement Delay, s/veh | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 29.1 | 24.9 | 24.8 | 21.7 | 30.4 | 30.4 | 39.1 | 0.0 | 36.0 | 48.7 | 45.1 | 55.8 |
| LnGrp LOS | C | C | C | C | C | C | D | A | D | D | D | E |
| Approach Vol, veh/h | 1662 | | | 775 | | | 160 | | | 430 | | |
| Approach Delay, s/veh | 25.9 | | | 29.9 | | | 36.9 | | | 51.3 | | |
| Approach LOS | C | | | C | | | D | | | D | | |
| Timer - Assigned Phs | 1 | 2 | | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 27.3 | 55.0 | | 36.6 | 12.5 | 69.8 | 11.0 | 25.6 | | | | |
| Change Period (Y+Rc), s | 8.5 | 8.5 | | 7.0 | 8.5 | 8.5 | 7.0 | 7.0 | | | | |
| Max Green Setting (Gmax), s | 21.5 | 46.5 | | 53.0 | 11.5 | 56.5 | 13.0 | 38.0 | | | | |
| Max Q Clear Time (g_c+I1), s | 18.4 | 20.5 | | 7.9 | 3.9 | 31.9 | 4.6 | 17.0 | | | | |
| Green Ext Time (p_c), s | 0.5 | 4.3 | | 0.7 | 0.0 | 8.4 | 0.0 | 1.6 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | | 31.1 | | | | | | | | |
| HCM 6th LOS | | | | C | | | | | | | | |

Timings

102: Lake Helen Osteen & Catalina Blvd

02/29/2024



| Lane Group | EBL | EBR | NBL | NBT | SBT |
|----------------------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | |
| Traffic Volume (vph) | 172 | 343 | 199 | 169 | 362 |
| Future Volume (vph) | 172 | 343 | 199 | 169 | 362 |
| Turn Type | Prot | Prot | pm+pt | NA | NA |
| Protected Phases | 8 | 8 | 1 | 6 | 2 |
| Permitted Phases | | | 6 | | |
| Detector Phase | 8 | 8 | 1 | 6 | 2 |
| Switch Phase | | | | | |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 15.0 | 15.0 |
| Minimum Split (s) | 11.5 | 11.5 | 11.5 | 21.5 | 21.5 |
| Total Split (s) | 26.5 | 26.5 | 26.5 | 63.0 | 36.5 |
| Total Split (%) | 29.6% | 29.6% | 29.6% | 70.4% | 40.8% |
| Yellow Time (s) | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.5 | 6.5 | 6.5 | 6.5 | 6.5 |
| Lead/Lag | | | Lead | | Lag |
| Lead-Lag Optimize? | | | Yes | | Yes |
| Recall Mode | None | None | None | Min | Min |
| Act Effect Green (s) | 12.6 | 12.6 | 39.4 | 39.4 | 23.1 |
| Actuated g/C Ratio | 0.19 | 0.19 | 0.60 | 0.60 | 0.35 |
| v/c Ratio | 0.54 | 0.61 | 0.49 | 0.16 | 0.77 |
| Control Delay | 31.8 | 8.1 | 10.3 | 6.6 | 28.1 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 31.8 | 8.1 | 10.3 | 6.6 | 28.1 |
| LOS | C | A | B | A | C |
| Approach Delay | 16.0 | | | 8.6 | 28.1 |
| Approach LOS | B | | | A | C |

Intersection Summary

Cycle Length: 89.5

Actuated Cycle Length: 65.5

Natural Cycle: 60

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.77

Intersection Signal Delay: 18.1

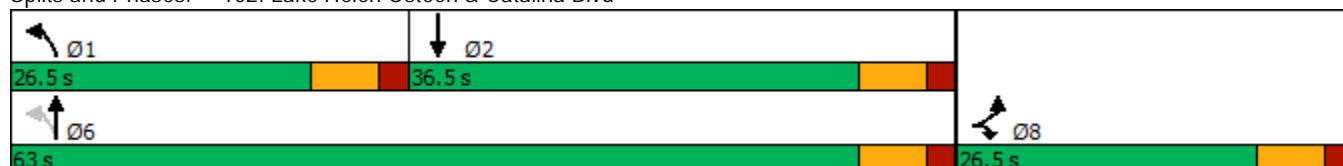
Intersection LOS: B

Intersection Capacity Utilization 61.6%

ICU Level of Service B

Analysis Period (min) 15

Splits and Phases: 102: Lake Helen Osteen & Catalina Blvd



HCM 6th Signalized Intersection Summary 102: Lake Helen Osteen & Catalina Blvd

02/29/2024






| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
|------------------------------|------|------|------|------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 172 | 343 | 199 | 169 | 362 | 95 |
| Future Volume (veh/h) | 172 | 343 | 199 | 169 | 362 | 95 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | No | | | No | No | |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1826 | 1870 | 1856 | 1841 |
| Adj Flow Rate, veh/h | 185 | 369 | 214 | 182 | 389 | 102 |
| Peak Hour Factor | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Percent Heavy Veh, % | 2 | 2 | 5 | 2 | 3 | 4 |
| Cap, veh/h | 473 | 421 | 362 | 997 | 456 | 120 |
| Arrive On Green | 0.27 | 0.27 | 0.11 | 0.53 | 0.32 | 0.32 |
| Sat Flow, veh/h | 1781 | 1585 | 1739 | 1870 | 1417 | 372 |
| Grp Volume(v), veh/h | 185 | 369 | 214 | 182 | 0 | 491 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 1585 | 1739 | 1870 | 0 | 1789 |
| Q Serve(g_s), s | 5.5 | 14.4 | 4.9 | 3.2 | 0.0 | 16.6 |
| Cycle Q Clear(g_c), s | 5.5 | 14.4 | 4.9 | 3.2 | 0.0 | 16.6 |
| Prop In Lane | 1.00 | 1.00 | 1.00 | | | 0.21 |
| Lane Grp Cap(c), veh/h | 473 | 421 | 362 | 997 | 0 | 575 |
| V/C Ratio(X) | 0.39 | 0.88 | 0.59 | 0.18 | 0.00 | 0.85 |
| Avail Cap(c_a), veh/h | 552 | 491 | 708 | 1637 | 0 | 831 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 19.4 | 22.7 | 14.0 | 7.8 | 0.0 | 20.5 |
| Incr Delay (d2), s/veh | 0.5 | 14.7 | 1.5 | 0.1 | 0.0 | 6.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 2.2 | 6.5 | 1.6 | 1.0 | 0.0 | 6.8 |
| Unsig. Movement Delay, s/veh | | | | | | |
| LnGrp Delay(d),s/veh | 20.0 | 37.4 | 15.6 | 7.9 | 0.0 | 26.5 |
| LnGrp LOS | B | D | B | A | A | C |
| Approach Vol, veh/h | 554 | | | 396 | 491 | |
| Approach Delay, s/veh | 31.6 | | | 12.0 | 26.5 | |
| Approach LOS | C | | | B | C | |
| Timer - Assigned Phs | 1 | 2 | | | 6 | 8 |
| Phs Duration (G+Y+Rc), s | 13.7 | 27.3 | | | 40.9 | 23.6 |
| Change Period (Y+Rc), s | 6.5 | 6.5 | | | 6.5 | 6.5 |
| Max Green Setting (Gmax), s | 20.0 | 30.0 | | | 56.5 | 20.0 |
| Max Q Clear Time (g_c+I1), s | 6.9 | 18.6 | | | 5.2 | 16.4 |
| Green Ext Time (p_c), s | 0.5 | 2.2 | | | 1.0 | 0.7 |

Intersection Summary

| | |
|--------------------|------|
| HCM 6th Ctrl Delay | 24.5 |
| HCM 6th LOS | C |

HCM 6th TWSC
103: Lake Helen Osteen & Driveway #1

02/29/2024

| Intersection | | | | | | |
|--------------------------|---|------|---|------|------|---|
| Int Delay, s/veh | 0.2 | | | | | |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations |  | |  | | |  |
| Traffic Vol, veh/h | 5 | 6 | 263 | 0 | 0 | 445 |
| Future Vol, veh/h | 5 | 6 | 263 | 0 | 0 | 445 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, # | 0 | - | 0 | - | - | 0 |
| Grade, % | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 86 | 86 | 86 | 86 | 86 | 86 |
| Heavy Vehicles, % | 2 | 17 | 2 | 2 | 2 | 3 |
| Mvmt Flow | 6 | 7 | 306 | 0 | 0 | 517 |




| Major/Minor | Minor1 | Major1 | Major2 | | | |
|----------------------|--------|--------|--------|---|---|---|
| Conflicting Flow All | 823 | 306 | 0 | - | - | - |
| Stage 1 | 306 | - | - | - | - | - |
| Stage 2 | 517 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.37 | - | - | - | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.453 | - | - | - | - |
| Pot Cap-1 Maneuver | 343 | 700 | - | 0 | 0 | - |
| Stage 1 | 747 | - | - | 0 | 0 | - |
| Stage 2 | 598 | - | - | 0 | 0 | - |
| Platoon blocked, % | | | - | | | - |
| Mov Cap-1 Maneuver | 343 | 700 | - | - | - | - |
| Mov Cap-2 Maneuver | 343 | - | - | - | - | - |
| Stage 1 | 747 | - | - | - | - | - |
| Stage 2 | 598 | - | - | - | - | - |

| Approach | WB | NB | SB |
|----------------------|------|----|----|
| HCM Control Delay, s | 12.8 | 0 | 0 |
| HCM LOS | B | | |

| Minor Lane/Major Mvmt | NBTWBLn1 | SBT |
|-----------------------|----------|-----|
| Capacity (veh/h) | - 475 | - |
| HCM Lane V/C Ratio | - 0.027 | - |
| HCM Control Delay (s) | - 12.8 | - |
| HCM Lane LOS | - B | - |
| HCM 95th %tile Q(veh) | - 0.1 | - |

HCM 6th TWSC
104: Lake Helen Osteen & Driveway #2

02/29/2024

| Intersection | | | | | | |
|--------------------------|---|----------|---|-------|-------|---|
| Int Delay, s/veh | 0.1 | | | | | |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations |  | |  | | |  |
| Traffic Vol, veh/h | 0 | 0 | 264 | 2 | 5 | 445 |
| Future Vol, veh/h | 0 | 0 | 264 | 2 | 5 | 445 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, # | 0 | - | 0 | - | - | 0 |
| Grade, % | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 87 | 87 | 87 | 87 | 87 | 87 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 3 |
| Mvmt Flow | 0 | 0 | 303 | 2 | 6 | 511 |
| Major/Minor | Minor1 | Major1 | Major2 | | | |
| Conflicting Flow All | 827 | 304 | 0 | 0 | 305 | 0 |
| Stage 1 | 304 | - | - | - | - | - |
| Stage 2 | 523 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.12 | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | - | - | 2.218 | - |
| Pot Cap-1 Maneuver | 341 | 736 | - | - | 1256 | - |
| Stage 1 | 748 | - | - | - | - | - |
| Stage 2 | 595 | - | - | - | - | - |
| Platoon blocked, % | | | - | - | | - |
| Mov Cap-1 Maneuver | 339 | 736 | - | - | 1256 | - |
| Mov Cap-2 Maneuver | 339 | - | - | - | - | - |
| Stage 1 | 748 | - | - | - | - | - |
| Stage 2 | 591 | - | - | - | - | - |
| Approach | WB | NB | SB | | | |
| HCM Control Delay, s | 0 | 0 | 0.1 | | | |
| HCM LOS | A | | | | | |
| Minor Lane/Major Mvmt | NBT | NBRWBLn1 | SBL | SBT | | |
| Capacity (veh/h) | - | - | - | 1256 | - | |
| HCM Lane V/C Ratio | - | - | - | 0.005 | - | |
| HCM Control Delay (s) | - | - | 0 | 7.9 | 0 | |
| HCM Lane LOS | - | - | A | A | A | |
| HCM 95th %tile Q(veh) | - | - | - | 0 | - | |

Timings

105: Elkcarn Blvd & Lake Helen Osteen

02/29/2024



| Lane Group | SEL | SET | NWL | NWT | NEL | NET | SWL | SWT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | | |
| Traffic Volume (vph) | 33 | 286 | 19 | 232 | 157 | 357 | 89 | 210 |
| Future Volume (vph) | 33 | 286 | 19 | 232 | 157 | 357 | 89 | 210 |
| Turn Type | pm+pt | NA | pm+pt | NA | pm+pt | NA | pm+pt | NA |
| Protected Phases | 5 | 2 | 1 | 6 | 3 | 8 | 7 | 4 |
| Permitted Phases | 2 | | 6 | | 8 | | 4 | |
| Detector Phase | 5 | 2 | 1 | 6 | 3 | 8 | 7 | 4 |
| Switch Phase | | | | | | | | |
| Minimum Initial (s) | 5.0 | 16.0 | 5.0 | 16.0 | 5.0 | 6.0 | 5.0 | 6.0 |
| Minimum Split (s) | 14.0 | 25.0 | 14.0 | 25.0 | 13.5 | 13.0 | 13.5 | 13.0 |
| Total Split (s) | 29.0 | 49.0 | 29.0 | 49.0 | 28.5 | 32.0 | 28.5 | 32.0 |
| Total Split (%) | 20.9% | 35.4% | 20.9% | 35.4% | 20.6% | 23.1% | 20.6% | 23.1% |
| Yellow Time (s) | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 4.0 | 5.5 | 4.0 |
| All-Red Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 9.0 | 9.0 | 9.0 | 9.0 | 8.5 | 7.0 | 8.5 | 7.0 |
| Lead/Lag | Lead | Lag | Lead | Lag | Lead | Lag | Lead | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | Min | None | Min | None | None | None | None |
| Act Effect Green (s) | 33.2 | 30.7 | 30.7 | 27.3 | 35.7 | 28.0 | 29.0 | 21.1 |
| Actuated g/C Ratio | 0.35 | 0.32 | 0.32 | 0.29 | 0.38 | 0.30 | 0.31 | 0.22 |
| v/c Ratio | 0.12 | 0.72 | 0.07 | 0.75 | 0.40 | 0.71 | 0.31 | 0.57 |
| Control Delay | 19.4 | 36.9 | 18.9 | 40.8 | 23.9 | 44.0 | 24.3 | 43.1 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 19.4 | 36.9 | 18.9 | 40.8 | 23.9 | 44.0 | 24.3 | 43.1 |
| LOS | B | D | B | D | C | D | C | D |
| Approach Delay | | 35.6 | | 39.7 | | 38.1 | | 37.7 |
| Approach LOS | | D | | D | | D | | D |

Intersection Summary

Cycle Length: 138.5

Actuated Cycle Length: 94.9

Natural Cycle: 80

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.75

Intersection Signal Delay: 37.7

Intersection LOS: D

Intersection Capacity Utilization 72.4%

ICU Level of Service C

Analysis Period (min) 15





















Splits and Phases: 105: Elkcarn Blvd & Lake Helen Osteen

| | | | |
|------|------|--------|------|
| Ø1 | Ø2 | Ø3 | Ø4 |
| 29 s | 49 s | 28.5 s | 32 s |
| Ø5 | Ø6 | Ø7 | Ø8 |
| 29 s | 49 s | 28.5 s | 32 s |

HCM 6th Signalized Intersection Summary

105: Elkcarn Blvd & Lake Helen Osteen

02/29/2024

| |  |  |  |  |  |  |  |  |  |  |  |  |
|------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | SEL | SET | SER | NWL | NWT | NWR | NEL | NET | NER | SWL | SWT | SWR |
| Lane Configurations |  |  | |  |  | |  |  | |  |  | |
| Traffic Volume (veh/h) | 33 | 286 | 114 | 19 | 232 | 138 | 157 | 357 | 14 | 89 | 210 | 14 |
| Future Volume (veh/h) | 33 | 286 | 114 | 19 | 232 | 138 | 157 | 357 | 14 | 89 | 210 | 14 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1856 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1885 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 35 | 301 | 120 | 20 | 244 | 145 | 165 | 376 | 15 | 94 | 221 | 15 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh, % | 3 | 2 | 2 | 2 | 2 | 2 | 2 | 1 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 202 | 353 | 141 | 178 | 293 | 174 | 356 | 430 | 17 | 230 | 349 | 24 |
| Arrive On Green | 0.03 | 0.28 | 0.28 | 0.02 | 0.27 | 0.27 | 0.10 | 0.24 | 0.24 | 0.06 | 0.20 | 0.20 |
| Sat Flow, veh/h | 1767 | 1272 | 507 | 1781 | 1099 | 653 | 1781 | 1800 | 72 | 1781 | 1732 | 118 |
| Grp Volume(v), veh/h | 35 | 0 | 421 | 20 | 0 | 389 | 165 | 0 | 391 | 94 | 0 | 236 |
| Grp Sat Flow(s),veh/h/ln | 1767 | 0 | 1779 | 1781 | 0 | 1753 | 1781 | 0 | 1872 | 1781 | 0 | 1849 |
| Q Serve(g_s), s | 1.2 | 0.0 | 18.7 | 0.7 | 0.0 | 17.5 | 6.0 | 0.0 | 16.8 | 3.4 | 0.0 | 9.7 |
| Cycle Q Clear(g_c), s | 1.2 | 0.0 | 18.7 | 0.7 | 0.0 | 17.5 | 6.0 | 0.0 | 16.8 | 3.4 | 0.0 | 9.7 |
| Prop In Lane | 1.00 | | 0.29 | 1.00 | | 0.37 | 1.00 | | 0.04 | 1.00 | | 0.06 |
| Lane Grp Cap(c), veh/h | 202 | 0 | 494 | 178 | 0 | 467 | 356 | 0 | 447 | 230 | 0 | 372 |
| V/C Ratio(X) | 0.17 | 0.00 | 0.85 | 0.11 | 0.00 | 0.83 | 0.46 | 0.00 | 0.87 | 0.41 | 0.00 | 0.63 |
| Avail Cap(c_a), veh/h | 567 | 0 | 853 | 565 | 0 | 840 | 610 | 0 | 561 | 551 | 0 | 554 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 22.7 | 0.0 | 28.5 | 23.3 | 0.0 | 28.8 | 23.3 | 0.0 | 30.5 | 25.3 | 0.0 | 30.5 |
| Incr Delay (d2), s/veh | 0.4 | 0.0 | 4.3 | 0.3 | 0.0 | 3.9 | 0.9 | 0.0 | 12.1 | 1.2 | 0.0 | 1.8 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 0.5 | 0.0 | 8.1 | 0.3 | 0.0 | 7.4 | 2.5 | 0.0 | 8.7 | 1.5 | 0.0 | 4.4 |
| Unsig. Movement Delay, s/veh | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 23.2 | 0.0 | 32.8 | 23.5 | 0.0 | 32.8 | 24.2 | 0.0 | 42.6 | 26.5 | 0.0 | 32.3 |
| LnGrp LOS | C | A | C | C | A | C | C | A | D | C | A | C |
| Approach Vol, veh/h | | 456 | | | 409 | | | 556 | | | 330 | |
| Approach Delay, s/veh | | 32.0 | | | 32.3 | | | 37.1 | | | 30.6 | |
| Approach LOS | | C | | | C | | | D | | | C | |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 10.9 | 32.2 | 16.6 | 23.8 | 11.8 | 31.2 | 13.5 | 26.9 | | | | |
| Change Period (Y+Rc), s | 9.0 | 9.0 | 8.5 | 7.0 | 9.0 | 9.0 | 8.5 | 7.0 | | | | |
| Max Green Setting (Gmax), s | 20.0 | 40.0 | 20.0 | 25.0 | 20.0 | 40.0 | 20.0 | 25.0 | | | | |
| Max Q Clear Time (g_c+I1), s | 2.7 | 20.7 | 8.0 | 11.7 | 3.2 | 19.5 | 5.4 | 18.8 | | | | |
| Green Ext Time (p_c), s | 0.0 | 2.5 | 0.3 | 1.0 | 0.0 | 2.3 | 0.2 | 1.2 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 33.5 | | | | | | | | | |
| HCM 6th LOS | | | C | | | | | | | | | |

Volusia County, FL



MOVING TRAFFIC FORWARD

400 - Lake Helen Osteen @ Catalina Blvd. - ASC - [REDACTED] - Econolite Type - ASC/3

Controller Timing Plan (MM) 2-1

Plan 1

| Phase | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
|---------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| Direction | | | | | | | | | | | | | | | | |
| Min Green | 5 | 15 | 0 | 0 | 0 | 15 | 0 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 |
| Bk Min Green | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| CS Min Green | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Delay Green | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Walk | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 0 | 10 | 0 | 10 | 0 | 10 |
| Walk2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Walk Max | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped Clear | 0 | 15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16 | 0 | 16 | 0 | 16 | 0 | 16 |
| Ped Clear 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped Clear Max | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped CO | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Vehicle Ext | 5.0 | 5.0 | 0.0 | 0.0 | 0.0 | 5.0 | 0.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Vehicle Ext 2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Max1 | 20 | 30 | 0 | 0 | 0 | 30 | 0 | 20 | 35 | 35 | 35 | 35 | 35 | 35 | 35 | 35 |
| Max2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 40 | 40 | 40 | 40 | 40 | 40 | 40 | 40 |
| Max3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| DYM Max | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Dym Step | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Yellow | 4.5 | 4.5 | 0.0 | 0.0 | 0.0 | 4.5 | 0.0 | 4.5 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Red Clear | 2.0 | 2.0 | 0.0 | 0.0 | 0.0 | 2.0 | 0.0 | 2.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Red Max | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Red Revert | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Act B4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sec/Act | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Max Int | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Time B4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Cars Wt | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| STPTDuc | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| TTReduc | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Min Gap | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |



Volusia County, FL

MOVING TRAFFIC FORWARD

400 - Lake Helen Osteen @ Catalina Blvd. - ASC - [REDACTED] - Econolite Type - ASC/3

Time Base Day Plan/Schedule**Day Plan (MM) 5-3****Day Plan #1**

| Event | Action Plan | Start Time |
|-------|-------------|------------|
| 1 | 11 | 00:00 |

Schedule (MM) 5-4**Schedule Number - 1**

Day Plan No.: 1

| Month | JAN | FEB | MAR | APR | MAY | JUN | JUL | AUG | SEP | OCT | NOV | DEC |
|-------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| | X | X | X | X | X | X | X | X | X | X | X | X |

| Day (DOW) | SUN | MON | TUE | WED | THU | FRI | SAT |
|-----------|-----|-----|-----|-----|-----|-----|-----|
| | X | X | X | X | X | X | X |

| Day (DOM) | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 |
|-----------|----|----|----|----|----|----|----|----|----|----|----|
| | X | X | X | X | X | X | X | X | X | X | X |
| | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 |
| | X | X | X | X | X | X | X | X | X | X | X |
| | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | | |
| | X | X | X | X | X | X | X | X | X | | |

Volusia County, FL



MOVING TRAFFIC FORWARD

339 - Elkcam @ Lake Helen Osteen - ASC-3 - [REDACTED] - Econolite Type - Cobalt

Controller Timing Plan (MM) 2-1

Plan 1 - ""

| Phase | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
|---------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| Direction | N-L | S-T | E-L | W-T | S-L | N-T | W-L | E-T | N | N | N | N | N | N | N | N |
| Min Green | 5 | 16 | 5 | 6 | 5 | 16 | 5 | 6 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 |
| Bk Min Green | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| CS Min Green | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Delay Green | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Walk | 0 | 7 | 0 | 7 | 0 | 7 | 0 | 7 | 0 | 10 | 0 | 10 | 0 | 10 | 0 | 10 |
| Walk2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Walk Max | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped Clear | 0 | 24 | 0 | 20 | 0 | 24 | 0 | 20 | 0 | 16 | 0 | 16 | 0 | 16 | 0 | 16 |
| Ped Clear 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped Clear Max | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped CO | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Vehicle Ext | 3.0 | 4.0 | 3.0 | 4.0 | 3.0 | 4.0 | 3.0 | 4.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Vehicle Ext 2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Max1 | 20 | 40 | 20 | 25 | 20 | 40 | 20 | 25 | 35 | 35 | 35 | 35 | 35 | 35 | 35 | 35 |
| Max2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 40 | 40 | 40 | 40 | 40 | 40 | 40 | 40 |
| Max3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| DYM Max | 0 | 60 | 0 | 60 | 0 | 60 | 0 | 60 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Dym Step | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Yellow | 5.5 | 5.5 | 5.5 | 4.0 | 5.5 | 5.5 | 5.5 | 4.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Red Clear | 3.5 | 3.5 | 3.0 | 3.0 | 3.5 | 3.5 | 3.0 | 3.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Red Max | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Red Revert | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Act B4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sec/Act | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Max Int | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Time B4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Cars Wt | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| STPTDuc | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| TTReduc | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Min Gap | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |



Volusia County, FL

MOVING TRAFFIC FORWARD

339 - Elkcarn @ Lake Helen Osteen - ASC-3 - [REDACTED] - Econolite Type - Cobalt

Time Base Day Plan/Schedule
Day Plan (MM) 5-3

Schedule (MM) 5-4

Volusia County, FL



MOVING TRAFFIC FORWARD

250 -Howland Blvd @ Catalina Blvd. - ASC/3 - [REDACTED] - Econolite Type - ASC/3

Controller Timing Plan (MM) 2-1

Plan 1

| Phase | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
|---------------|-----|------|-----|-----|-----|-----|-----|------|-----|-----|-----|-----|-----|-----|-----|-----|
| Direction | | | | | | | | | | | | | | | | |
| Min Green | 5 | 11 | 0 | 7 | 5 | 11 | 5 | 7 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 |
| Bk Min Green | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| CS Min Green | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Delay Green | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Walk | 0 | 7 | 0 | 7 | 0 | 7 | 0 | 7 | 0 | 10 | 0 | 10 | 0 | 10 | 0 | 10 |
| Walk2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Walk Max | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped Clear | 0 | 23 | 0 | 23 | 0 | 23 | 0 | 26 | 0 | 16 | 0 | 16 | 0 | 16 | 0 | 16 |
| Ped Clear 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped Clear Max | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped CO | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Vehicle Ext | 3.0 | 4.0 | 0.0 | 3.0 | 3.0 | 4.0 | 3.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Vehicle Ext 2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Max1 | 30 | 45 | 0 | 25 | 20 | 45 | 20 | 35 | 35 | 35 | 35 | 35 | 35 | 35 | 35 | 35 |
| Max2 | 30 | 45 | 0 | 25 | 20 | 45 | 20 | 20 | 20 | 40 | 40 | 40 | 40 | 40 | 40 | 40 |
| Max3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| DYM Max | 0 | 90 | 0 | 0 | 0 | 0 | 0 | 50 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Dym Step | 0.0 | 10.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 10.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Yellow | 5.0 | 5.0 | 0.0 | 4.0 | 5.0 | 5.0 | 4.0 | 4.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Red Clear | 3.5 | 3.5 | 0.0 | 3.0 | 3.5 | 3.5 | 3.0 | 3.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Red Max | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Red Revert | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Act B4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sec/Act | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Max Int | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Time B4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Cars Wt | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| STPTDuc | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| TTReduc | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Min Gap | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

Volusia County, FL



MOVING TRAFFIC FORWARD

250 -Howland Blvd @ Catalina Blvd. - ASC/3 - [REDACTED] - Econolite Type - ASC/3

Coordination Options**Options (MM) 3-1**

| | | | |
|---------------------|---------|--------------------|---------|
| Manual Pattern | Auto | ECPI Coord | Yes |
| System Source | SYS | System Format | PTN |
| Splits In | Seconds | Offsets In | Seconds |
| Transition | Smooth | Max Select | MAXINH |
| Dwell / Add Time | 0 | | |
| Delay Coord Wk-LZ | No | Force Off | Float |
| Offset Reference | Yellow | Use Ped Time | Yes |
| Ped Recall | No | Ped Reservice | No |
| Local Zero Override | No | FO Added Ini Green | No |
| Re-sync Count | 0 | Multisync | No |

Auto Perm Minimum Green (Seconds) (MM) 3-4

| Phase | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
|---------------|---|---|---|---|---|---|---|---|---|----|----|----|----|----|----|----|
| Minimum Green | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

Split Demand (MM) 3-5

| Phase | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
|----------|---|---|---|---|---|---|---|---|---|----|----|----|----|----|----|----|
| Demand 1 | | | | | | | | | | | | | | | | |
| Demand 2 | | | | | | | | | | | | | | | | |

| Demand | 1 | 2 |
|-----------------|---|---|
| Detector | 0 | 0 |
| Call Time (Sec) | 0 | 0 |
| Cycle Count | 0 | 0 |

Volusia County, FL



MOVING TRAFFIC FORWARD

250 -Howland Blvd @ Catalina Blvd. - ASC/3 - [REDACTED] - Econolite Type - ASC/3

Coordination Pattern Data

Coordinator Pattern Data (MM) 3-2

Coordinator Pattern # 1

| | | | | | |
|--------------------|------|----------------|------|------------|---------|
| Split Pattern | 1 | TS2 (Pat-Off) | 0-1 | Splits In | Seconds |
| Cycle | 150 | Std (COS) | 9 | Offsets In | Seconds |
| Offset Value | 0s | Dwell/Add Time | 0 | | |
| Actuated Coord | Yes | Timing Plan | 0 | | |
| Actuated Walk Rest | No | Sequence | 0 | | |
| Phase Reserve | No | Action Plan | 0 | | |
| Max Select | None | Force Off | None | | |

Split Preference Phases

| Phase | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
|----------------------|----|----|---|----|----|----|----|----|---|----|----|----|----|----|----|----|
| Description | | | | | | | | | | | | | | | | |
| Splits (Split Pat 1) | 24 | 59 | 0 | 67 | 18 | 65 | 24 | 43 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pref 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pref 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

| Ring | 1 | 2 | 3 | 4 |
|-------------------|------|------|----|----|
| Ring Split Ext | 0 | 0 | 0 | 0 |
| Ring Displacement | - | 0 | 0 | 0 |
| Split Sum | 150s | 150s | 0s | 0s |

Misc. Data

| | | | | | |
|--------------------|---|--------------------|---|-----------------------|---|
| Veh Perm 1 | 0 | Veh Perm 2 | 0 | Veh Perm 2 Disp | 0 |
| Split Demand Pat 1 | 0 | Split Demand Pat 2 | 0 | Crossing Arterial Pat | 0 |

Split Pattern

| Phase | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
|--------------------------|---|---|---|---|---|---|---|---|---|----|----|----|----|----|----|----|
| Coord Phase | | X | | | | X | | | | | | | | | | |
| Vehicle Recall | | | | | | | | | | | | | | | | |
| Pedestrian Recall | | | | | | | | | | | | | | | | |
| Recall to Max. Time | | | | | | | | | | | | | | | | |
| Omit Phase | | | | | | | | | X | X | X | X | X | X | X | X |
| Special Function Outputs | | | | | | | | | | | | | | | | |

Coordinator Pattern # 2

| | | | | | |
|--------------------|------|----------------|------|------------|---------|
| Split Pattern | 2 | TS2 (Pat-Off) | 0-2 | Splits In | Seconds |
| Cycle | 150 | Std (COS) | 17 | Offsets In | Seconds |
| Offset Value | 0s | Dwell/Add Time | 0 | | |
| Actuated Coord | Yes | Timing Plan | 0 | | |
| Actuated Walk Rest | No | Sequence | 0 | | |
| Phase Reservice | No | Action Plan | 0 | | |
| Max Select | None | Force Off | None | | |

Split Preference Phases

| Phase | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
|----------------------|----|----|---|----|----|----|----|----|---|----|----|----|----|----|----|----|
| Description | | | | | | | | | | | | | | | | |
| Splits (Split Pat 2) | 31 | 59 | 0 | 60 | 20 | 65 | 25 | 40 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pref 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pref 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

| Ring | 1 | 2 | 3 | 4 |
|-------------------|------|------|----|----|
| Ring Split Ext | 0 | 0 | 0 | 0 |
| Ring Displacement | - | 0 | 0 | 0 |
| Split Sum | 150s | 150s | 0s | 0s |

Misc. Data

| | | | | | |
|--------------------|---|--------------------|---|-----------------------|---|
| Veh Perm 1 | 0 | Veh Perm 2 | 0 | Veh Perm 2 Disp | 0 |
| Split Demand Pat 1 | 0 | Split Demand Pat 2 | 0 | Crossing Arterial Pat | 0 |

Split Pattern

| Phase | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
|--------------------------|---|---|---|---|---|---|---|---|---|----|----|----|----|----|----|----|
| Coord Phase | | X | | | | X | | | | | | | | | | |
| Vehicle Recall | | | | | | | | | | | | | | | | |
| Pedestrian Recall | | | | | | | | | | | | | | | | |
| Recall to Max. Time | | | | | | | | | | | | | | | | |
| Omit Phase | | | | | | | | | X | X | X | X | X | X | X | X |
| Special Function Outputs | | | | | | | | | | | | | | | | |

Coordinator Pattern # 3

| | | | | | |
|--------------------|------|----------------|------|------------|---------|
| Split Pattern | 3 | TS2 (Pat-Off) | 0-3 | Splits In | Seconds |
| Cycle | 150 | Std (COS) | 25 | Offsets In | Seconds |
| Offset Value | 0s | Dwell/Add Time | 0 | | |
| Actuated Coord | Yes | Timing Plan | 0 | | |
| Actuated Walk Rest | No | Sequence | 0 | | |
| Phase Reservice | No | Action Plan | 0 | | |
| Max Select | None | Force Off | None | | |

Split Preference Phases

| Phase | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
|----------------------|----|----|---|----|----|----|----|----|---|----|----|----|----|----|----|----|
| Description | | | | | | | | | | | | | | | | |
| Splits (Split Pat 3) | 30 | 60 | 0 | 60 | 20 | 65 | 20 | 45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pref 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pref 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

| Ring | 1 | 2 | 3 | 4 |
|-------------------|------|------|----|----|
| Ring Split Ext | 0 | 0 | 0 | 0 |
| Ring Displacement | - | 0 | 0 | 0 |
| Split Sum | 150s | 150s | 0s | 0s |

Misc. Data

| | | | | | |
|--------------------|---|--------------------|---|-----------------------|---|
| Veh Perm 1 | 0 | Veh Perm 2 | 0 | Veh Perm 2 Disp | 0 |
| Split Demand Pat 1 | 0 | Split Demand Pat 2 | 0 | Crossing Arterial Pat | 0 |

Split Pattern

| Phase | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
|--------------------------|---|---|---|---|---|---|---|---|---|----|----|----|----|----|----|----|
| Coord Phase | | X | | | | X | | | | | | | | | | |
| Vehicle Recall | | | | | | | | | | | | | | | | |
| Pedestrian Recall | | | | | | | | | | | | | | | | |
| Recall to Max. Time | | | | | | | | | | | | | | | | |
| Omit Phase | | | | | | | | | X | X | X | X | X | X | X | X |
| Special Function Outputs | | | | | | | | | | | | | | | | |

Volusia County, FL



MOVING TRAFFIC FORWARD

250 -Howland Blvd @ Catalina Blvd. - ASC/3 - [REDACTED] - Econolite Type - ASC/3

Coordination Split Pattern**Split Pattern Data (MM) 3-3****Split Pattern # 1**

| Phase | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
|---------------------|----|----|---|----|----|----|----|----|---|----|----|----|----|----|----|----|
| Description | | | | | | | | | | | | | | | | |
| Split (seconds) | 24 | 59 | 0 | 67 | 18 | 65 | 24 | 43 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Coord Phase | | X | | | | X | | | | | | | | | | |
| Vehicle Recall | | | | | | | | | | | | | | | | |
| Pedestrian Recall | | | | | | | | | | | | | | | | |
| Recall to Max. Time | | | | | | | | | | | | | | | | |
| Omit Phase | | | | | | | | | X | X | X | X | X | X | X | X |

| Ring | 1 | 2 | 3 | 4 |
|-----------|------|------|----|----|
| Split Sum | 150s | 150s | 0s | 0s |

Split Pattern # 2

| Phase | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
|---------------------|----|----|---|----|----|----|----|----|---|----|----|----|----|----|----|----|
| Description | | | | | | | | | | | | | | | | |
| Split (seconds) | 31 | 59 | 0 | 60 | 20 | 65 | 25 | 40 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Coord Phase | | X | | | | X | | | | | | | | | | |
| Vehicle Recall | | | | | | | | | | | | | | | | |
| Pedestrian Recall | | | | | | | | | | | | | | | | |
| Recall to Max. Time | | | | | | | | | | | | | | | | |
| Omit Phase | | | | | | | | | X | X | X | X | X | X | X | X |

| Ring | 1 | 2 | 3 | 4 |
|-----------|------|------|----|----|
| Split Sum | 150s | 150s | 0s | 0s |

Split Pattern # 3

| Phase | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
|---------------------|----|----|---|----|----|----|----|----|---|----|----|----|----|----|----|----|
| Description | | | | | | | | | | | | | | | | |
| Split (seconds) | 30 | 60 | 0 | 60 | 20 | 65 | 20 | 45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Coord Phase | | X | | | | X | | | | | | | | | | |
| Vehicle Recall | | | | | | | | | | | | | | | | |
| Pedestrian Recall | | | | | | | | | | | | | | | | |
| Recall to Max. Time | | | | | | | | | | | | | | | | |
| Omit Phase | | | | | | | | | X | X | X | X | X | X | X | X |

| Ring | 1 | 2 | 3 | 4 |
|-----------|------|------|----|----|
| Split Sum | 150s | 150s | 0s | 0s |

Volusia County, FL



MOVING TRAFFIC FORWARD

250 -Howland Blvd @ Catalina Blvd. - ASC/3 - [REDACTED] - Econolite Type - ASC/3

Time Base Day Plan/Schedule**Day Plan (MM) 5-3****Day Plan #1**

| Event | Action Plan | Start Time |
|-------|-------------|------------|
| 1 | 1 | 06:30 |
| 2 | 11 | 09:00 |
| 3 | 3 | 14:30 |
| 4 | 11 | 19:00 |

Day Plan #2

| Event | Action Plan | Start Time |
|-------|-------------|------------|
| 1 | 11 | 00:00 |

Schedule (MM) 5-4**Schedule Number - 1**

Day Plan No.: 1

| Month | JAN | FEB | MAR | APR | MAY | JUN | JUL | AUG | SEP | OCT | NOV | DEC |
|-------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| | X | X | X | X | X | X | X | X | X | X | X | X |

| Day (DOW) | SUN | MON | TUE | WED | THU | FRI | SAT |
|-----------|-----|-----|-----|-----|-----|-----|-----|
| | | X | X | X | X | X | |

| Day (DOM) | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 |
|-----------|----|----|----|----|----|----|----|----|----|----|----|
| | X | X | X | X | X | X | X | X | X | X | X |
| | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 |
| | X | X | X | X | X | X | X | X | X | X | X |
| | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | | |
| | X | X | X | X | X | X | X | X | X | | |

Schedule Number - 3

Day Plan No.: 3

| Month | JAN | FEB | MAR | APR | MAY | JUN | JUL | AUG | SEP | OCT | NOV | DEC |
|-------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| | | | | | | | | | | | | |

| Day (DOW) | SUN | MON | TUE | WED | THU | FRI | SAT |
|-----------|-----|-----|-----|-----|-----|-----|-----|
| | | | | | | | |

| Day (DOM) | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 |
|-----------|----|----|----|----|----|----|----|----|----|----|----|
| | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 |
| | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | | |
| | | | | | | | | | | | |

Appendix E

Historical Data/Trends & Applied Annual Growth Rates

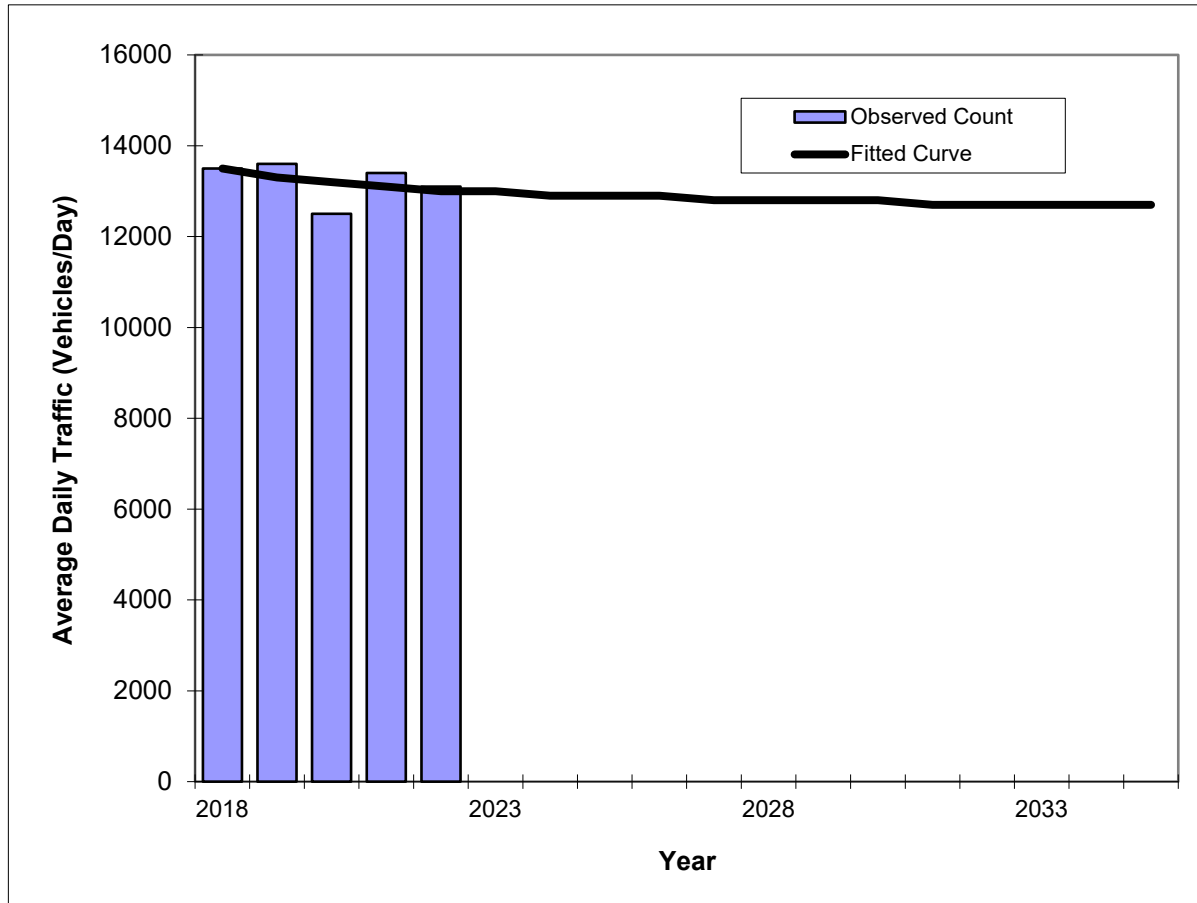


Traffic Trends - V03.a

Providence Blvd, Ft. Smith to Elkcarn --

| | |
|----------|--|
| FIN# | |
| Location | |

| | |
|------------|---------------------------------------|
| County: | Volusia |
| Station #: | 1541 |
| Highway: | Providence Blvd, Ft. Smith to Elkcarn |



| Year | Traffic (ADT/AADT) | |
|---------------------------|--------------------|---------|
| | Count* | Trend** |
| 2018 | 13500 | 13500 |
| 2019 | 13600 | 13300 |
| 2020 | 12500 | 13200 |
| 2021 | 13400 | 13100 |
| 2022 | 13100 | 13000 |
| 2025 Opening Year Trend | | |
| 2025 | N/A | 12900 |
| 2027 Mid-Year Trend | | |
| 2027 | N/A | 12800 |
| 2029 Design Year Trend | | |
| 2029 | N/A | 12800 |
| TRANPLAN Forecasts/Trends | | |
| | | |

| | |
|---|-----------|
| Trend R-squared: | 17.44% |
| Compounded Annual Historic Growth Rate: | -0.94% |
| Compounded Growth Rate (2022 to Design Year): | -0.22% |
| Printed: | 26-Feb-24 |
| Decaying Exponential Growth Option | |

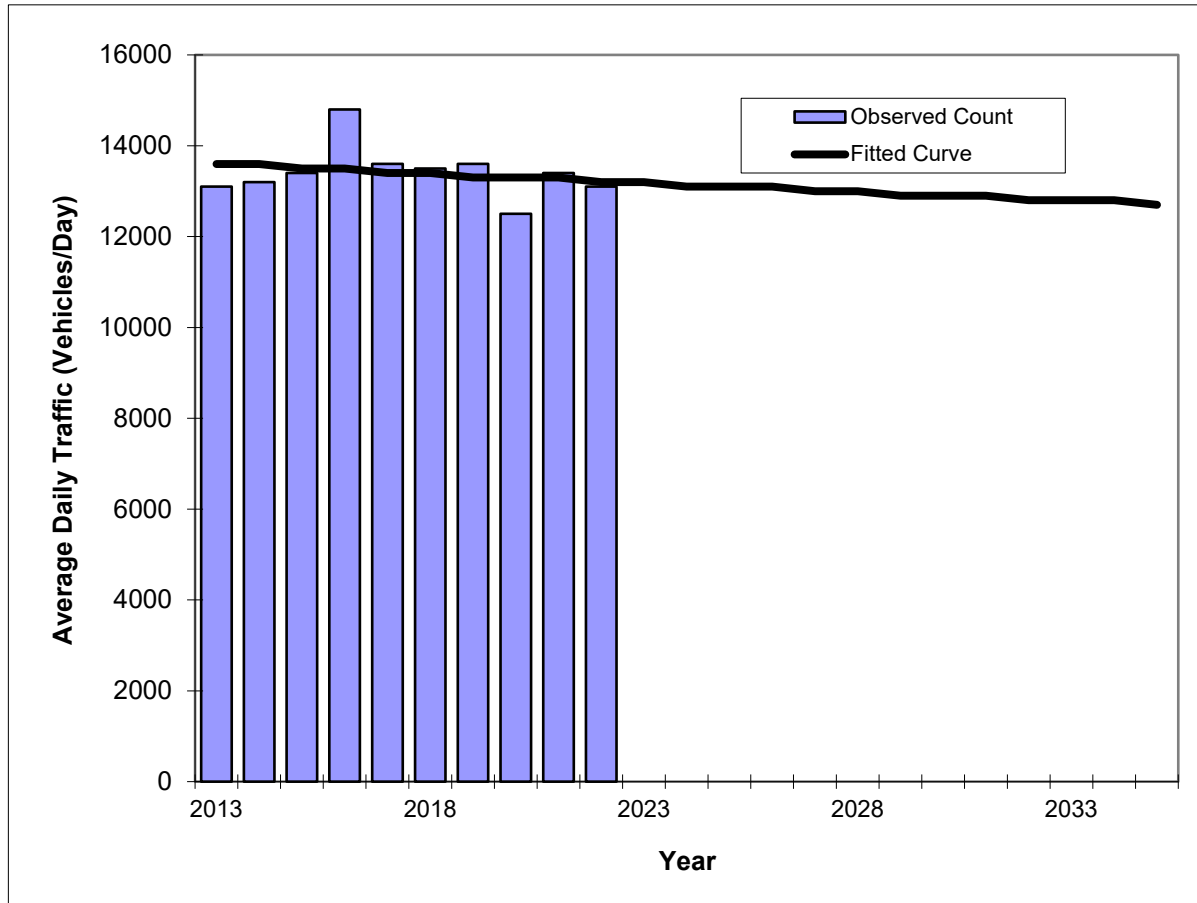
*Axle-Adjusted

Traffic Trends - V03.a

Providence Blvd, Ft. Smith to Elkcam --

| | |
|----------|--|
| FIN# | |
| Location | |

| | |
|------------|--------------------------------------|
| County: | Volusia |
| Station #: | 1541 |
| Highway: | Providence Blvd, Ft. Smith to Elkcam |



| Year | Traffic (ADT/AADT) | |
|---------------------------|--------------------|---------|
| | Count* | Trend** |
| 2013 | 13100 | 13600 |
| 2014 | 13200 | 13600 |
| 2015 | 13400 | 13500 |
| 2016 | 14800 | 13500 |
| 2017 | 13600 | 13400 |
| 2018 | 13500 | 13400 |
| 2019 | 13600 | 13300 |
| 2020 | 12500 | 13300 |
| 2021 | 13400 | 13300 |
| 2022 | 13100 | 13200 |
| 2025 Opening Year Trend | | |
| 2025 | N/A | 13100 |
| 2027 Mid-Year Trend | | |
| 2027 | N/A | 13000 |
| 2029 Design Year Trend | | |
| 2029 | N/A | 12900 |
| TRANPLAN Forecasts/Trends | | |
| | | |

| | |
|---|-----------|
| Trend R-squared: | 4.67% |
| Compounded Annual Historic Growth Rate: | -0.33% |
| Compounded Growth Rate (2022 to Design Year): | -0.33% |
| Printed: | 26-Feb-24 |
| Exponential Growth Option | |

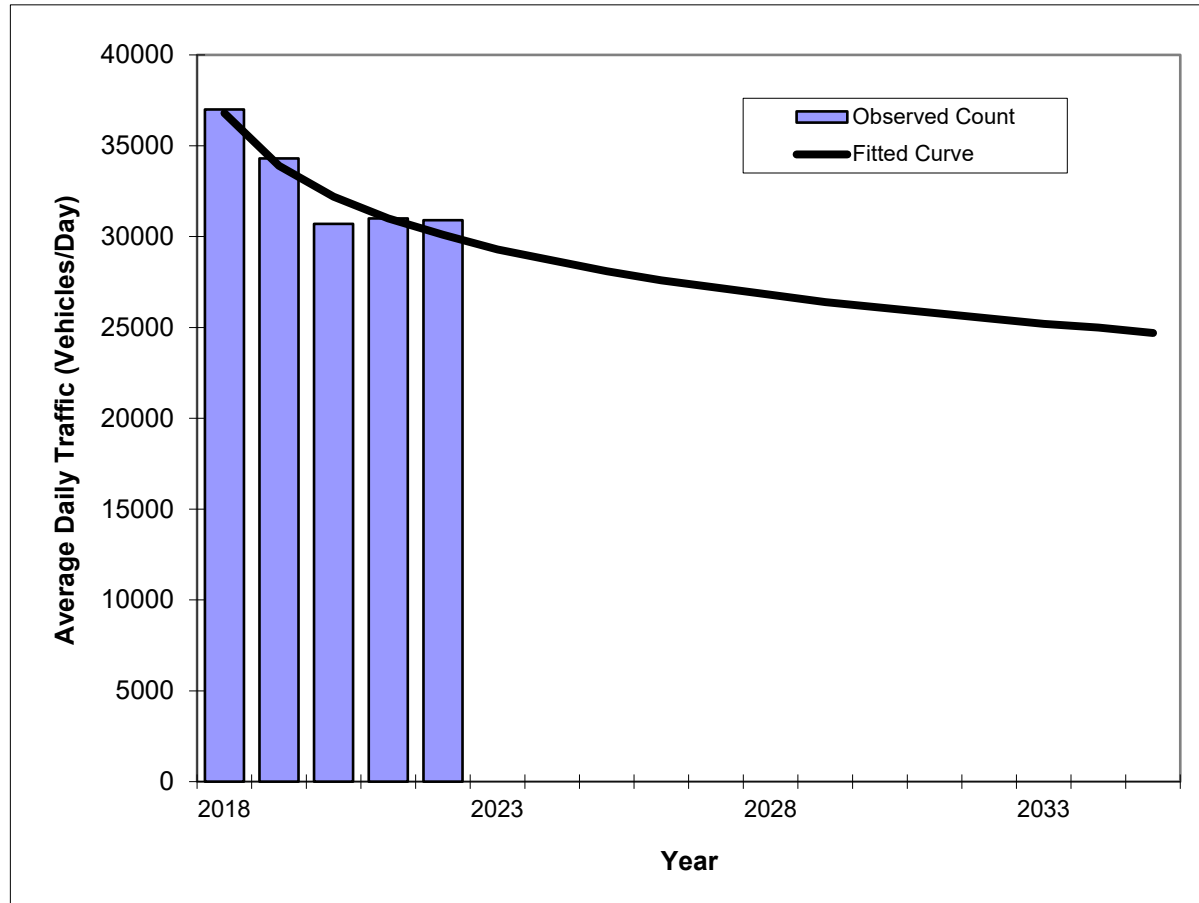
*Axle-Adjusted

Traffic Trends - V03.a

Howland Blvd, I-4 to Wolf Pack Run --

| | |
|----------|--|
| FIN# | |
| Location | |

| | |
|------------|------------------------------------|
| County: | Volusia |
| Station #: | 901 |
| Highway: | Howland Blvd, I-4 to Wolf Pack Run |



| Year | Traffic (ADT/AADT) | |
|---------------------------|--------------------|---------|
| | Count* | Trend** |
| 2018 | 37000 | 36800 |
| 2019 | 34300 | 33900 |
| 2020 | 30700 | 32200 |
| 2021 | 31000 | 31000 |
| 2022 | 30900 | 30100 |
| 2025 Opening Year Trend | | |
| 2025 | N/A | 28100 |
| 2027 Mid-Year Trend | | |
| 2027 | N/A | 27200 |
| 2029 Design Year Trend | | |
| 2029 | N/A | 26400 |
| TRANPLAN Forecasts/Trends | | |
| | | |

| | |
|---|-----------|
| Trend R-squared: | 89.87% |
| Compounded Annual Historic Growth Rate: | -4.90% |
| Compounded Growth Rate (2022 to Design Year): | -1.86% |
| Printed: | 23-Feb-24 |
| Decaying Exponential Growth Option | |

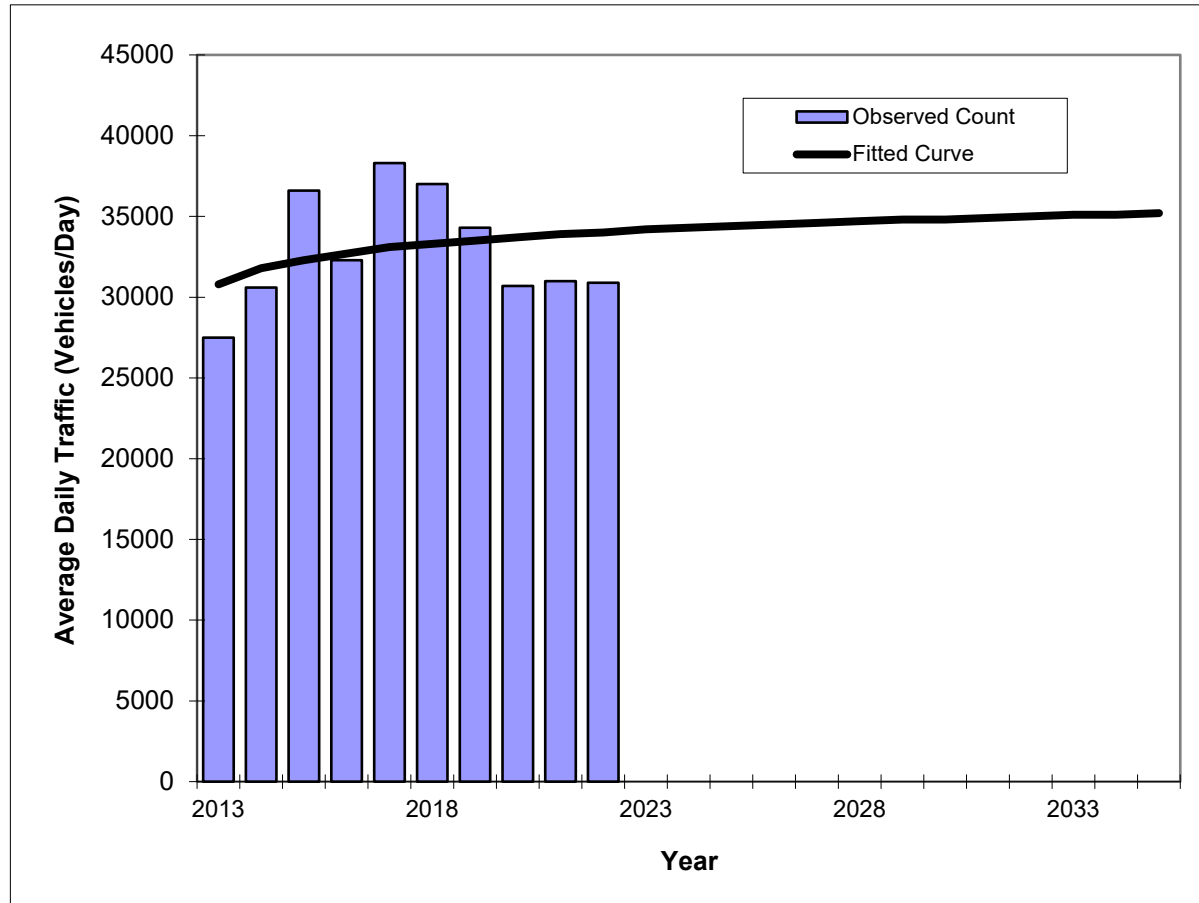
*Axle-Adjusted

Traffic Trends - V03.a

Howland Blvd, I-4 to Wolf Pack Run --

| | |
|----------|--|
| FIN# | |
| Location | |

| | |
|------------|------------------------------------|
| County: | Volusia |
| Station #: | 901 |
| Highway: | Howland Blvd, I-4 to Wolf Pack Run |



| Year | Traffic (ADT/AADT) | |
|---------------------------|--------------------|---------|
| | Count* | Trend** |
| 2013 | 27500 | 30800 |
| 2014 | 30600 | 31800 |
| 2015 | 36600 | 32300 |
| 2016 | 32300 | 32700 |
| 2017 | 38300 | 33100 |
| 2018 | 37000 | 33300 |
| 2019 | 34300 | 33500 |
| 2020 | 30700 | 33700 |
| 2021 | 31000 | 33900 |
| 2022 | 30900 | 34000 |
| 2025 Opening Year Trend | | |
| 2025 | N/A | 34400 |
| 2027 Mid-Year Trend | | |
| 2027 | N/A | 34600 |
| 2029 Design Year Trend | | |
| 2029 | N/A | 34800 |
| TRANPLAN Forecasts/Trends | | |
| | | |

| | |
|---|-----------|
| Trend R-squared: | 8.64% |
| Compounded Annual Historic Growth Rate: | 1.10% |
| Compounded Growth Rate (2022 to Design Year): | 0.33% |
| Printed: | 23-Feb-24 |
| Decaying Exponential Growth Option | |

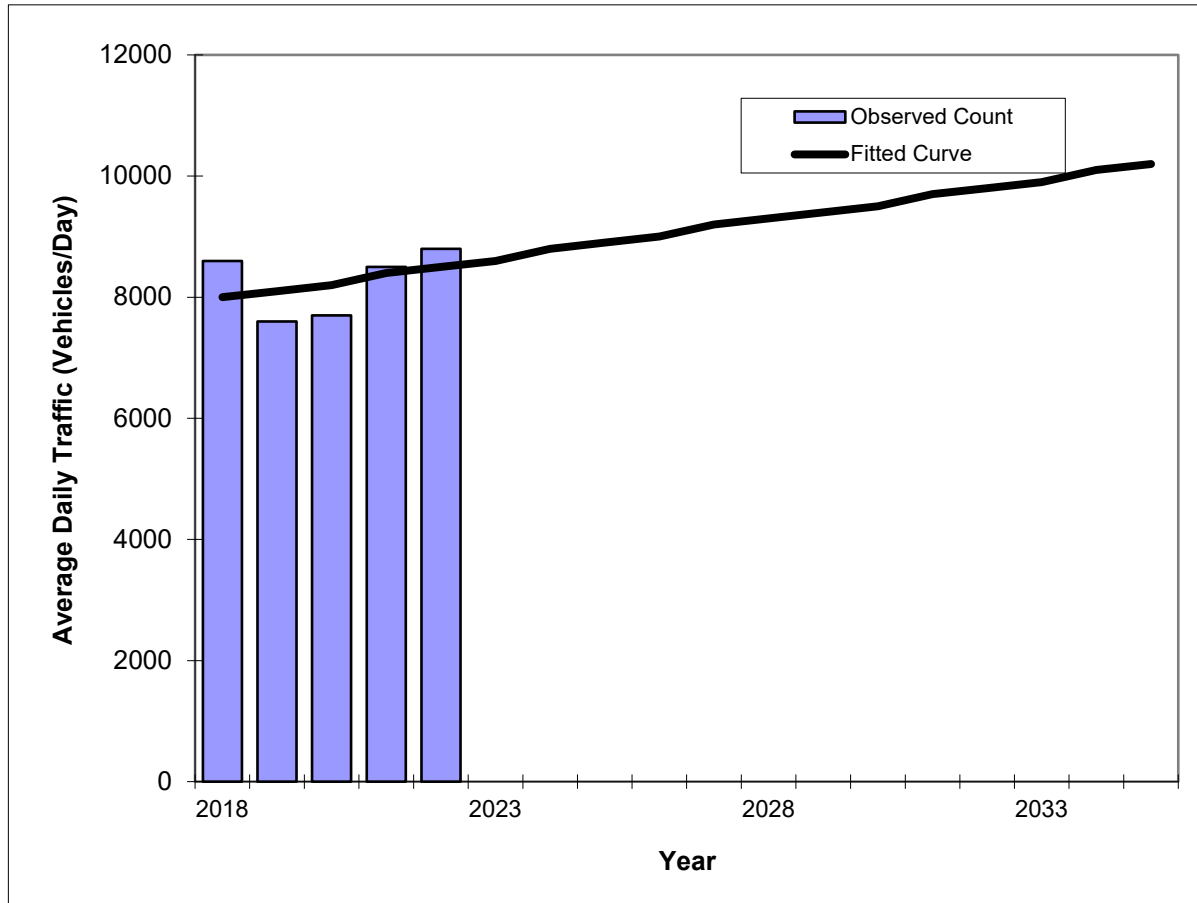
*Axle-Adjusted

Traffic Trends - V03.a

Lake Helen Osteen, Catalina to Captain --

| | |
|----------|--|
| FIN# | |
| Location | |

| | |
|------------|--|
| County: | Volusia |
| Station #: | 1073 |
| Highway: | Lake Helen Osteen, Catalina to Captain |



| Year | Traffic (ADT/AADT) | |
|---------------------------|--------------------|---------|
| | Count* | Trend** |
| 2018 | 8600 | 8000 |
| 2019 | 7600 | 8100 |
| 2020 | 7700 | 8200 |
| 2021 | 8500 | 8400 |
| 2022 | 8800 | 8500 |
| 2025 Opening Year Trend | | |
| 2025 | N/A | 8900 |
| 2027 Mid-Year Trend | | |
| 2027 | N/A | 9200 |
| 2029 Design Year Trend | | |
| 2029 | N/A | 9400 |
| TRANPLAN Forecasts/Trends | | |
| | | |

| | |
|--|-----------|
| ** Annual Trend Increase: | 130 |
| Trend R-squared: | 13.94% |
| Trend Annual Historic Growth Rate: | 1.56% |
| Trend Growth Rate (2022 to Design Year): | 1.51% |
| Printed: | 23-Feb-24 |
| Straight Line Growth Option | |

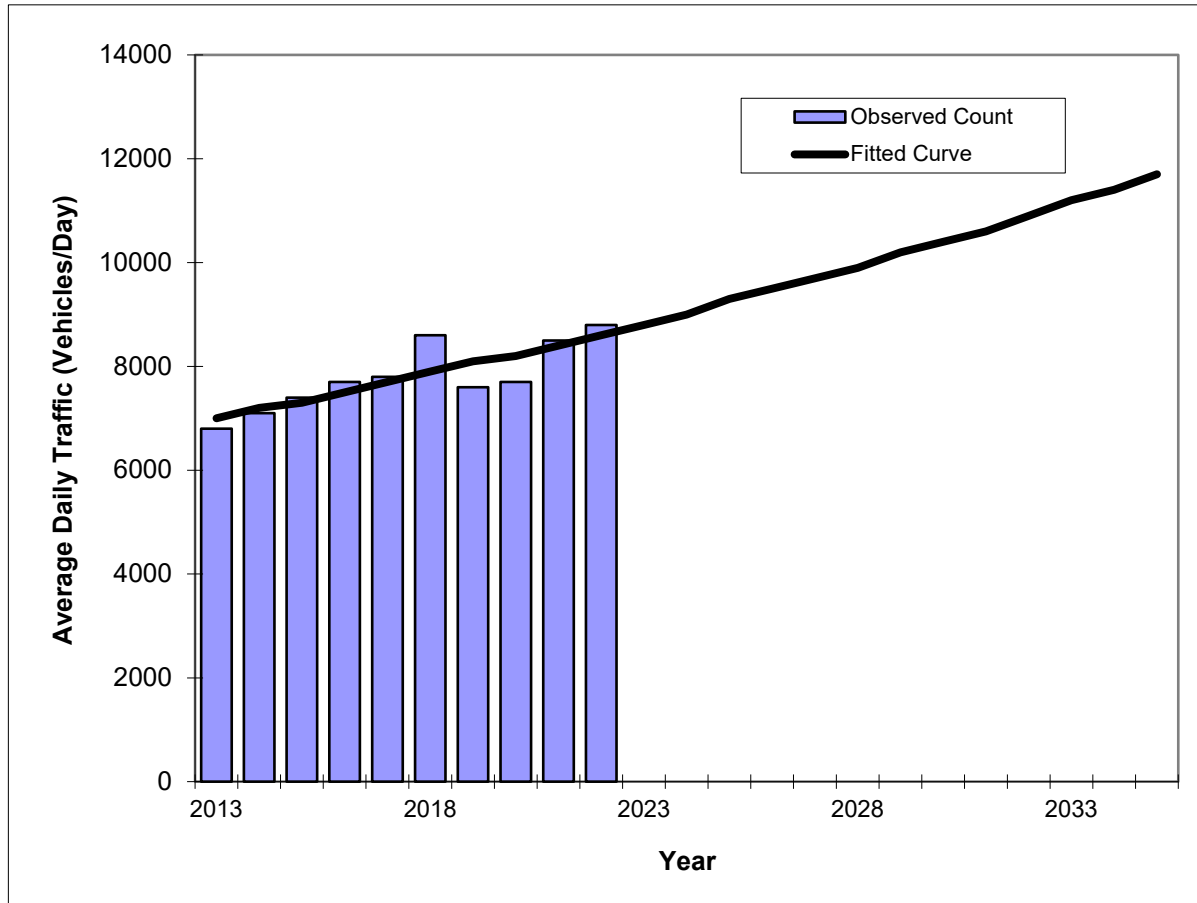
*Axle-Adjusted

Traffic Trends - V03.a

Lake Helen Osteen, Catalina to Captain --

| | |
|----------|--|
| FIN# | |
| Location | |

| | |
|------------|--|
| County: | Volusia |
| Station #: | 1073 |
| Highway: | Lake Helen Osteen, Catalina to Captain |



| Year | Traffic (ADT/AADT) | |
|---------------------------|--------------------|---------|
| | Count* | Trend** |
| 2013 | 6800 | 7000 |
| 2014 | 7100 | 7200 |
| 2015 | 7400 | 7300 |
| 2016 | 7700 | 7500 |
| 2017 | 7800 | 7700 |
| 2018 | 8600 | 7900 |
| 2019 | 7600 | 8100 |
| 2020 | 7700 | 8200 |
| 2021 | 8500 | 8400 |
| 2022 | 8800 | 8600 |
| 2025 Opening Year Trend | | |
| 2025 | N/A | 9300 |
| 2027 Mid-Year Trend | | |
| 2027 | N/A | 9700 |
| 2029 Design Year Trend | | |
| 2029 | N/A | 10200 |
| TRANPLAN Forecasts/Trends | | |
| | | |

| | |
|---|-----------|
| Trend R-squared: | 71.04% |
| Compounded Annual Historic Growth Rate: | 2.31% |
| Compounded Growth Rate (2022 to Design Year): | 2.47% |
| Printed: | 23-Feb-24 |
| Exponential Growth Option | |

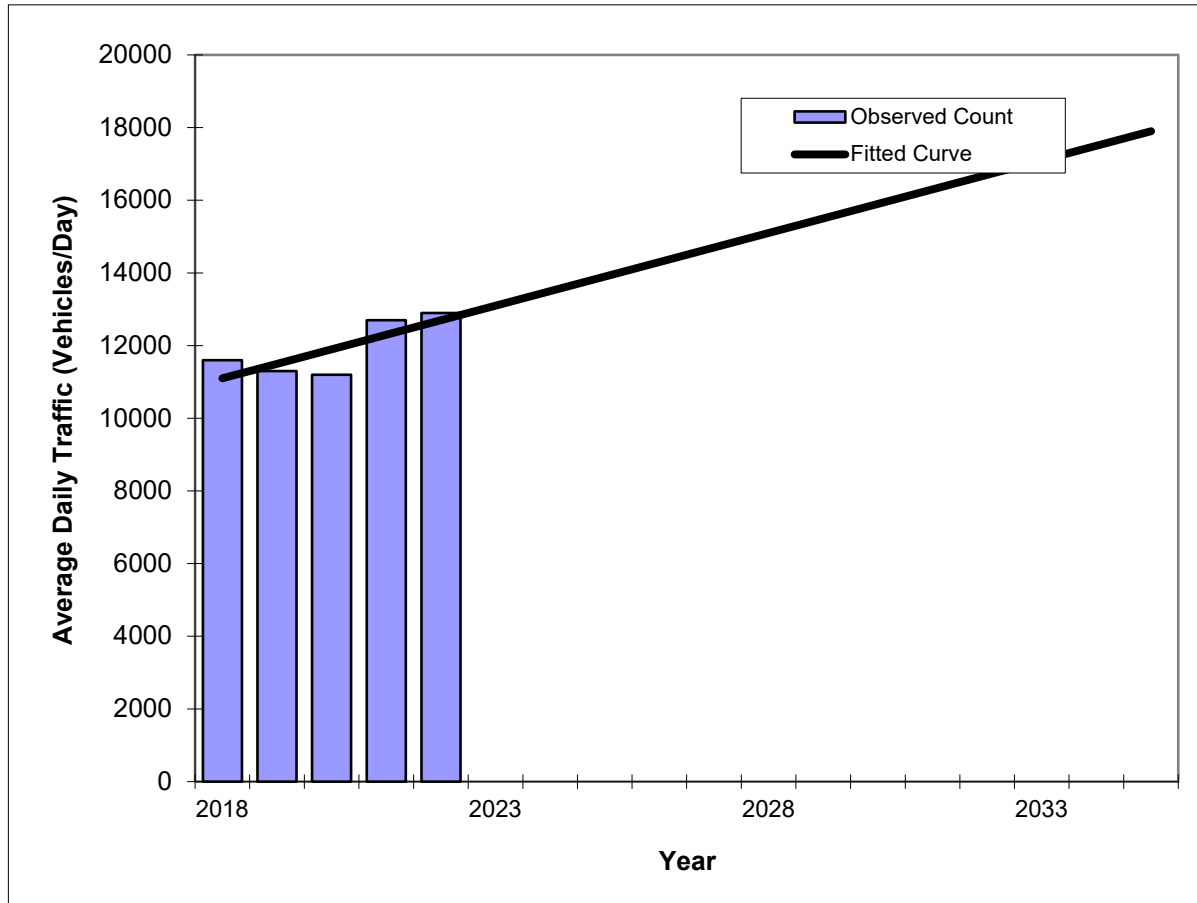
*Axle-Adjusted

Traffic Trends - V03.a

Lake Helen Osteen, Haulover to Catalina --

| | |
|----------|--|
| FIN# | |
| Location | |

| | |
|------------|---|
| County: | Volusia |
| Station #: | 1072 |
| Highway: | Lake Helen Osteen, Haulover to Catalina |



| Year | Traffic (ADT/AADT) | |
|---------------------------|--------------------|---------|
| | Count* | Trend** |
| 2018 | 11600 | 11100 |
| 2019 | 11300 | 11500 |
| 2020 | 11200 | 11900 |
| 2021 | 12700 | 12300 |
| 2022 | 12900 | 12700 |
| 2025 Opening Year Trend | | |
| 2025 | N/A | 13900 |
| 2027 Mid-Year Trend | | |
| 2027 | N/A | 14700 |
| 2029 Design Year Trend | | |
| 2029 | N/A | 15500 |
| TRANPLAN Forecasts/Trends | | |
| | | |

| | |
|--|-----------|
| ** Annual Trend Increase: | 400 |
| Trend R-squared: | 62.21% |
| Trend Annual Historic Growth Rate: | 3.60% |
| Trend Growth Rate (2022 to Design Year): | 3.15% |
| Printed: | 23-Feb-24 |
| Straight Line Growth Option | |

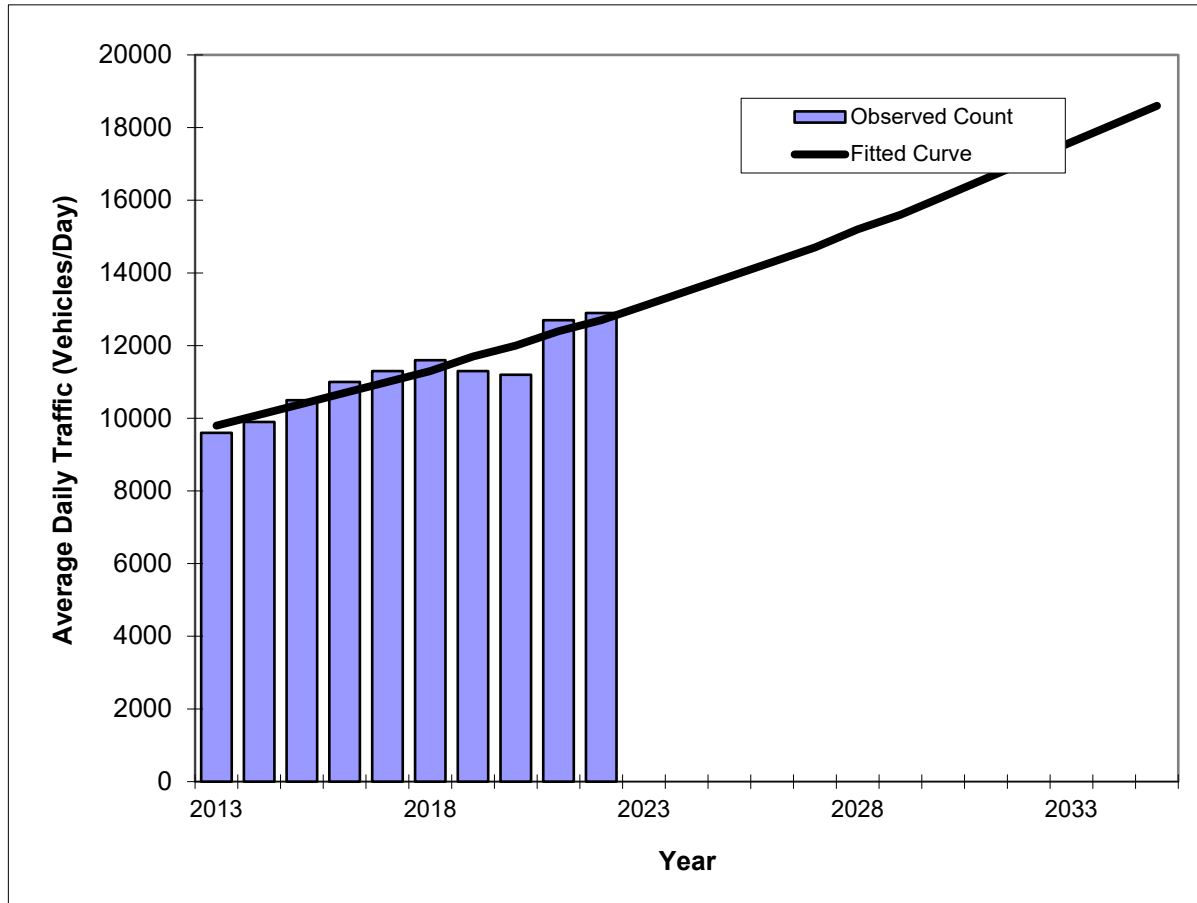
*Axle-Adjusted

Traffic Trends - V03.a

Lake Helen Osteen, Haulover to Catalina --

| | |
|----------|--|
| FIN# | |
| Location | |

| | |
|------------|---|
| County: | Volusia |
| Station #: | 1072 |
| Highway: | Lake Helen Osteen, Haulover to Catalina |



| Year | Traffic (ADT/AADT) | |
|---------------------------|--------------------|---------|
| | Count* | Trend** |
| 2013 | 9600 | 9800 |
| 2014 | 9900 | 10100 |
| 2015 | 10500 | 10400 |
| 2016 | 11000 | 10700 |
| 2017 | 11300 | 11000 |
| 2018 | 11600 | 11300 |
| 2019 | 11300 | 11700 |
| 2020 | 11200 | 12000 |
| 2021 | 12700 | 12400 |
| 2022 | 12900 | 12700 |
| 2025 Opening Year Trend | | |
| 2025 | N/A | 13900 |
| 2027 Mid-Year Trend | | |
| 2027 | N/A | 14700 |
| 2029 Design Year Trend | | |
| 2029 | N/A | 15600 |
| TRANPLAN Forecasts/Trends | | |
| | | |

| | |
|---|-----------|
| Trend R-squared: | 87.93% |
| Compounded Annual Historic Growth Rate: | 2.92% |
| Compounded Growth Rate (2022 to Design Year): | 2.98% |
| Printed: | 23-Feb-24 |
| Exponential Growth Option | |

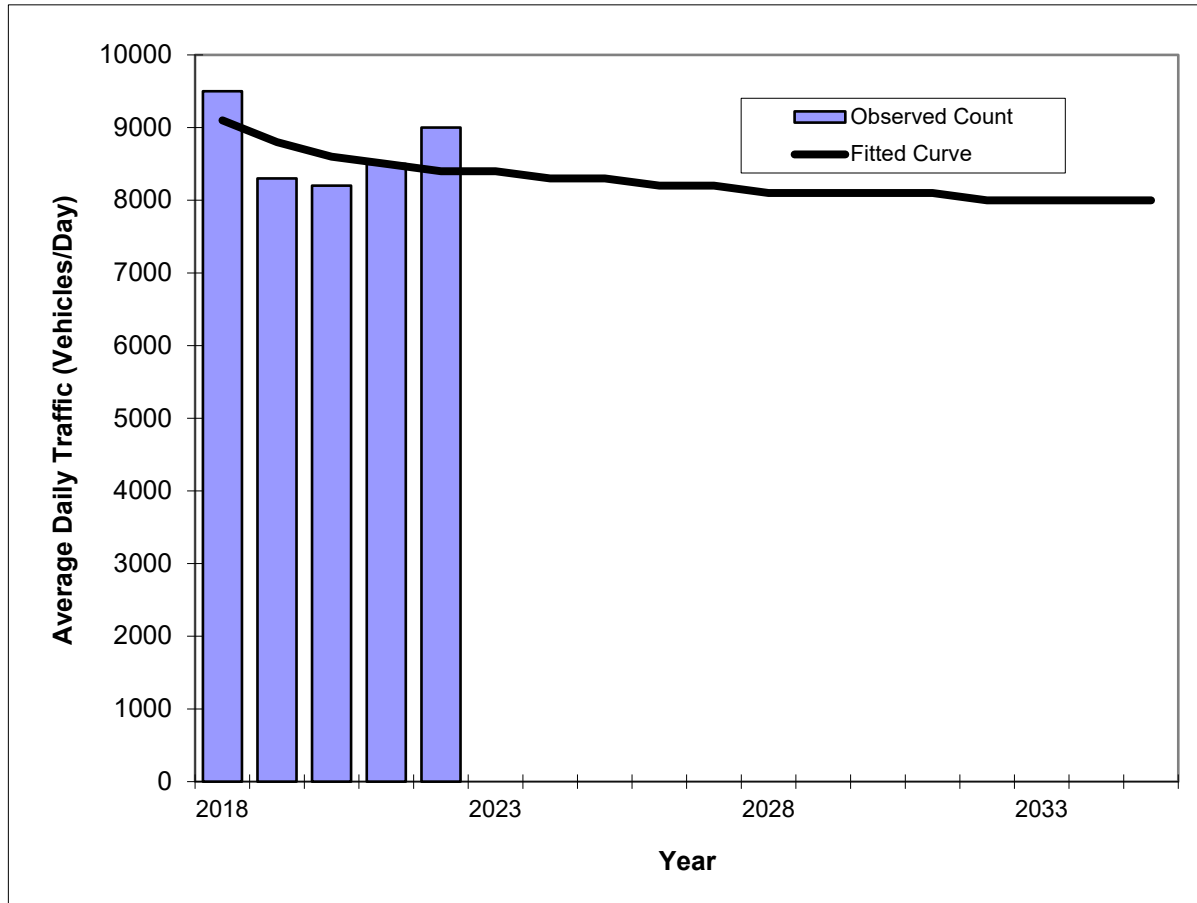
*Axle-Adjusted

Traffic Trends - V03.a

Lake Helen Osteen, Elkcam to Haulover --

| | |
|----------|--|
| FIN# | |
| Location | |

| | |
|------------|---------------------------------------|
| County: | Volusia |
| Station #: | 1071 |
| Highway: | Lake Helen Osteen, Elkcam to Haulover |



| Year | Traffic (ADT/AADT) | |
|---------------------------|--------------------|---------|
| | Count* | Trend** |
| 2018 | 9500 | 9100 |
| 2019 | 8300 | 8800 |
| 2020 | 8200 | 8600 |
| 2021 | 8500 | 8500 |
| 2022 | 9000 | 8400 |
| 2025 Opening Year Trend | | |
| 2025 | N/A | 8300 |
| 2027 Mid-Year Trend | | |
| 2027 | N/A | 8200 |
| 2029 Design Year Trend | | |
| 2029 | N/A | 8100 |
| TRANPLAN Forecasts/Trends | | |
| | | |

| | |
|---|-----------|
| Trend R-squared: | 20.23% |
| Compounded Annual Historic Growth Rate: | -1.98% |
| Compounded Growth Rate (2022 to Design Year): | -0.52% |
| Printed: | 23-Feb-24 |
| Decaying Exponential Growth Option | |

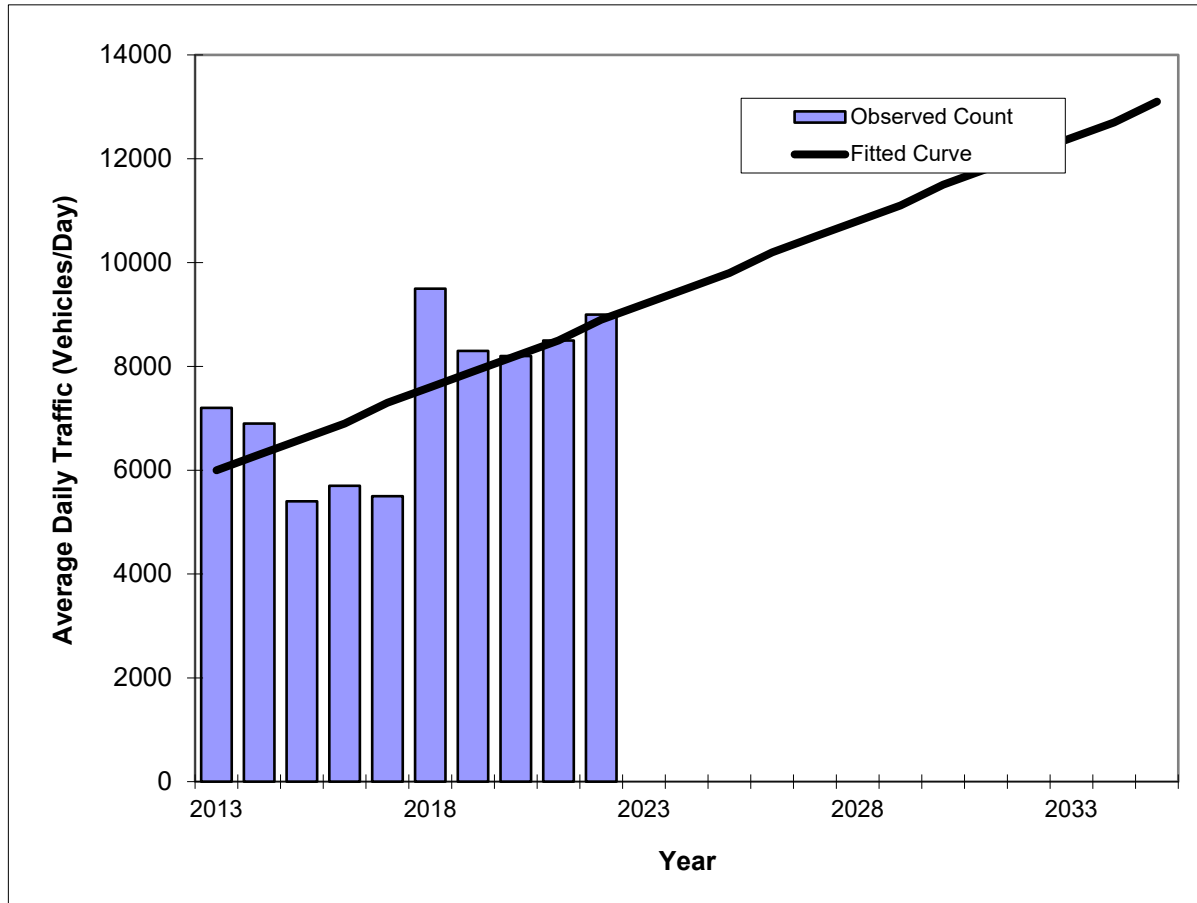
*Axle-Adjusted

Traffic Trends - V03.a

Lake Helen Osteen, Elkcarn to Haulover --

| | |
|----------|--|
| FIN# | |
| Location | |

| | |
|------------|--|
| County: | Volusia |
| Station #: | 1071 |
| Highway: | Lake Helen Osteen, Elkcarn to Haulover |



| Year | Traffic (ADT/AADT) | |
|---------------------------|--------------------|---------|
| | Count* | Trend** |
| 2013 | 7200 | 6000 |
| 2014 | 6900 | 6300 |
| 2015 | 5400 | 6600 |
| 2016 | 5700 | 6900 |
| 2017 | 5500 | 7300 |
| 2018 | 9500 | 7600 |
| 2019 | 8300 | 7900 |
| 2020 | 8200 | 8200 |
| 2021 | 8500 | 8500 |
| 2022 | 9000 | 8900 |
| 2025 Opening Year Trend | | |
| 2025 | N/A | 9800 |
| 2027 Mid-Year Trend | | |
| 2027 | N/A | 10500 |
| 2029 Design Year Trend | | |
| 2029 | N/A | 11100 |
| TRANPLAN Forecasts/Trends | | |
| | | |

| | |
|--|-----------|
| ** Annual Trend Increase: | 322 |
| Trend R-squared: | 42.01% |
| Trend Annual Historic Growth Rate: | 5.37% |
| Trend Growth Rate (2022 to Design Year): | 3.53% |
| Printed: | 23-Feb-24 |
| Straight Line Growth Option | |

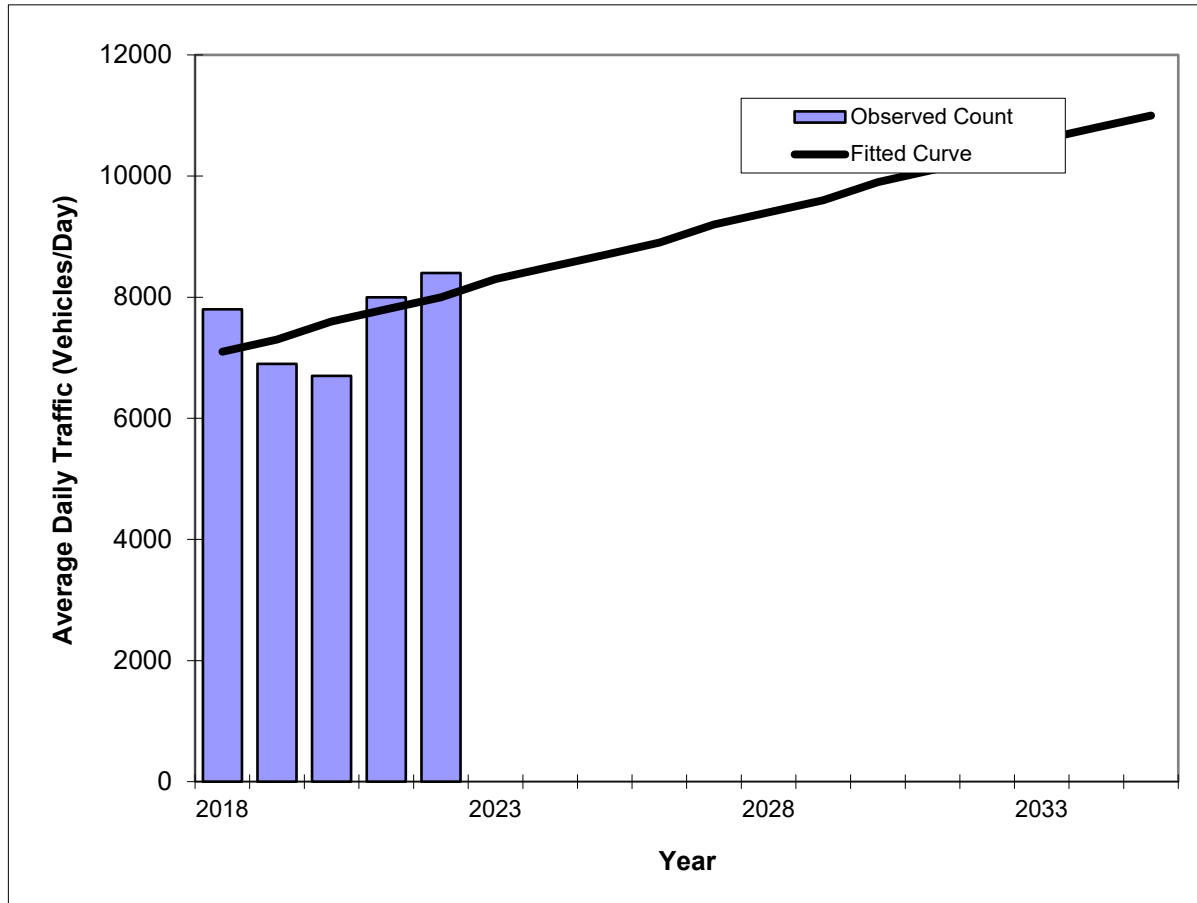
*Axle-Adjusted

Traffic Trends - V03.a

Lake Helen Osteen, Howland to Elkcam --

| | |
|----------|--|
| FIN# | |
| Location | |

| | |
|------------|--------------------------------------|
| County: | Volusia |
| Station #: | 1070 |
| Highway: | Lake Helen Osteen, Howland to Elkcam |



| Year | Traffic (ADT/AADT) | |
|---------------------------|--------------------|---------|
| | Count* | Trend** |
| 2018 | 7800 | 7100 |
| 2019 | 6900 | 7300 |
| 2020 | 6700 | 7600 |
| 2021 | 8000 | 7800 |
| 2022 | 8400 | 8000 |
| 2025 Opening Year Trend | | |
| 2025 | N/A | 8700 |
| 2027 Mid-Year Trend | | |
| 2027 | N/A | 9200 |
| 2029 Design Year Trend | | |
| 2029 | N/A | 9600 |
| TRANPLAN Forecasts/Trends | | |
| | | |

| | |
|--|-----------|
| ** Annual Trend Increase: | 230 |
| Trend R-squared: | 24.81% |
| Trend Annual Historic Growth Rate: | 3.17% |
| Trend Growth Rate (2022 to Design Year): | 2.86% |
| Printed: | 23-Feb-24 |
| Straight Line Growth Option | |

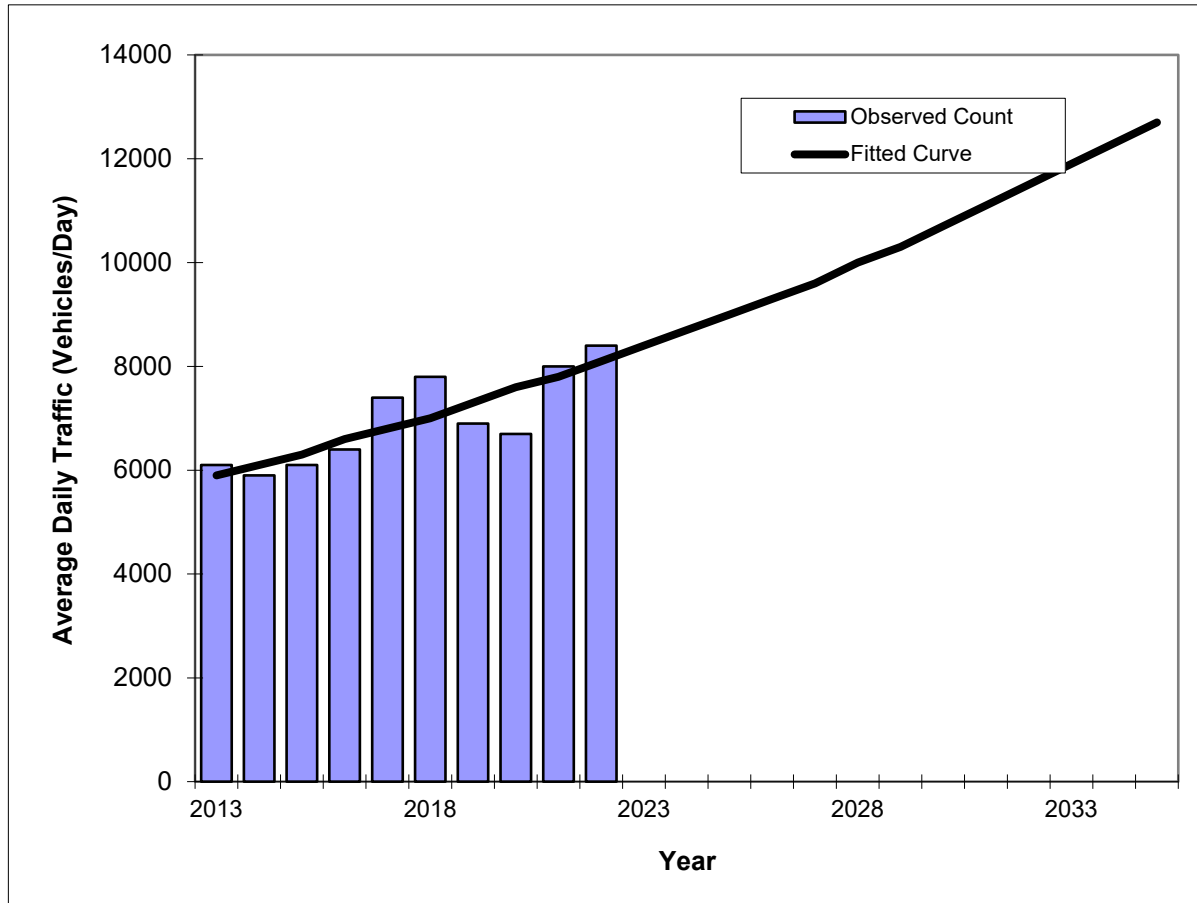
*Axle-Adjusted

Traffic Trends - V03.a

Lake Helen Osteen, Howland to Elkcam --

| | |
|----------|--|
| FIN# | |
| Location | |

| | |
|------------|--------------------------------------|
| County: | Volusia |
| Station #: | 1070 |
| Highway: | Lake Helen Osteen, Howland to Elkcam |



| Year | Traffic (ADT/AADT) | |
|---------------------------|--------------------|---------|
| | Count* | Trend** |
| 2013 | 6100 | 5900 |
| 2014 | 5900 | 6100 |
| 2015 | 6100 | 6300 |
| 2016 | 6400 | 6600 |
| 2017 | 7400 | 6800 |
| 2018 | 7800 | 7000 |
| 2019 | 6900 | 7300 |
| 2020 | 6700 | 7600 |
| 2021 | 8000 | 7800 |
| 2022 | 8400 | 8100 |
| 2025 Opening Year Trend | | |
| 2025 | N/A | 9000 |
| 2027 Mid-Year Trend | | |
| 2027 | N/A | 9600 |
| 2029 Design Year Trend | | |
| 2029 | N/A | 10300 |
| TRANPLAN Forecasts/Trends | | |
| | | |

| | |
|---|-----------|
| Trend R-squared: | 70.85% |
| Compounded Annual Historic Growth Rate: | 3.58% |
| Compounded Growth Rate (2022 to Design Year): | 3.49% |
| Printed: | 23-Feb-24 |
| Exponential Growth Option | |

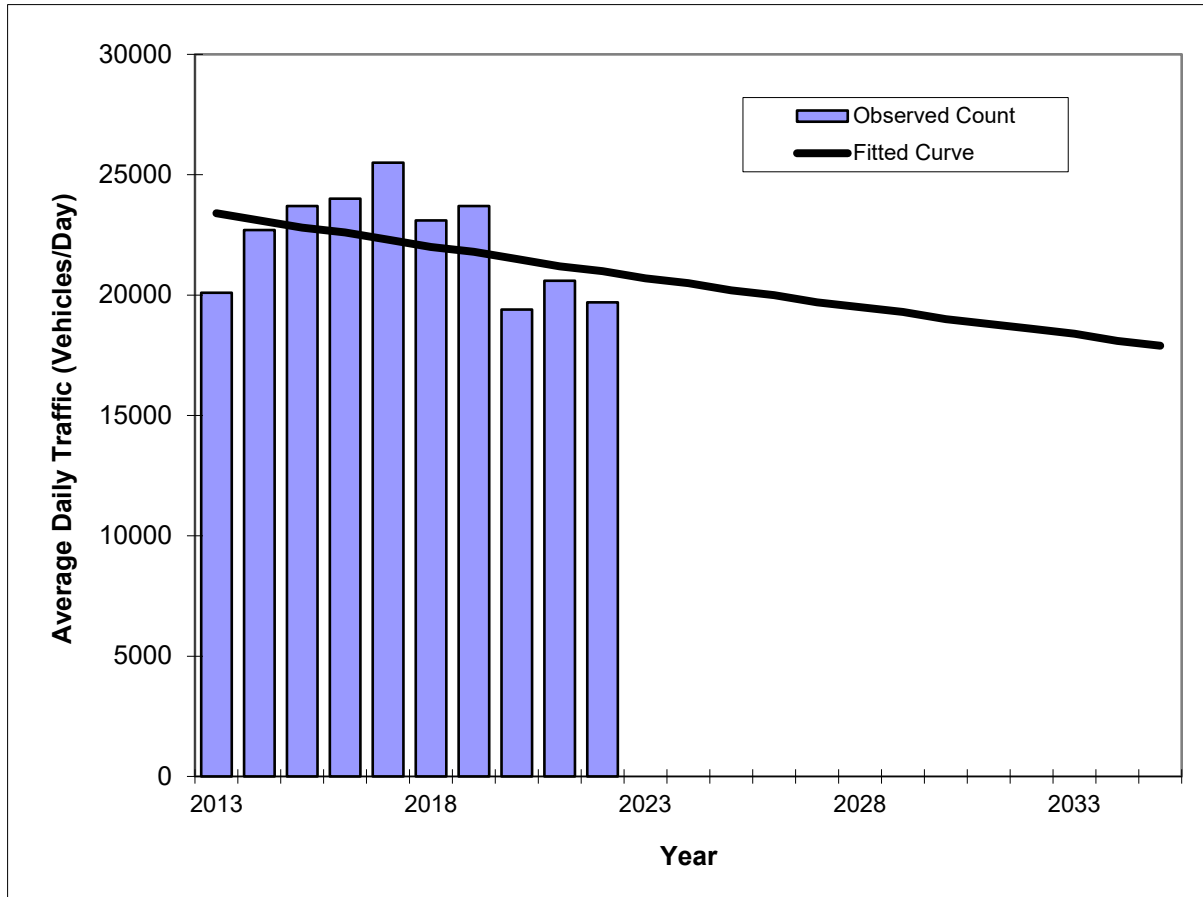
*Axle-Adjusted

Traffic Trends - V03.a

Howland Blvd, Catalina to Providence --

| | |
|----------|--|
| FIN# | |
| Location | |

| | |
|------------|--------------------------------------|
| County: | Volusia |
| Station #: | 905 |
| Highway: | Howland Blvd, Catalina to Providence |



| Year | Traffic (ADT/AADT) | |
|---------------------------|--------------------|---------|
| | Count* | Trend** |
| 2013 | 20100 | 23400 |
| 2014 | 22700 | 23100 |
| 2015 | 23700 | 22800 |
| 2016 | 24000 | 22600 |
| 2017 | 25500 | 22300 |
| 2018 | 23100 | 22000 |
| 2019 | 23700 | 21800 |
| 2020 | 19400 | 21500 |
| 2021 | 20600 | 21200 |
| 2022 | 19700 | 21000 |
| 2025 Opening Year Trend | | |
| 2025 | N/A | 20200 |
| 2027 Mid-Year Trend | | |
| 2027 | N/A | 19700 |
| 2029 Design Year Trend | | |
| 2029 | N/A | 19300 |
| TRANPLAN Forecasts/Trends | | |
| | | |

Trend R-squared: 14.44%
 Compounded Annual Historic Growth Rate: -1.20%
 Compounded Growth Rate (2022 to Design Year): -1.20%
 Printed: 23-Feb-24

Exponential Growth Option

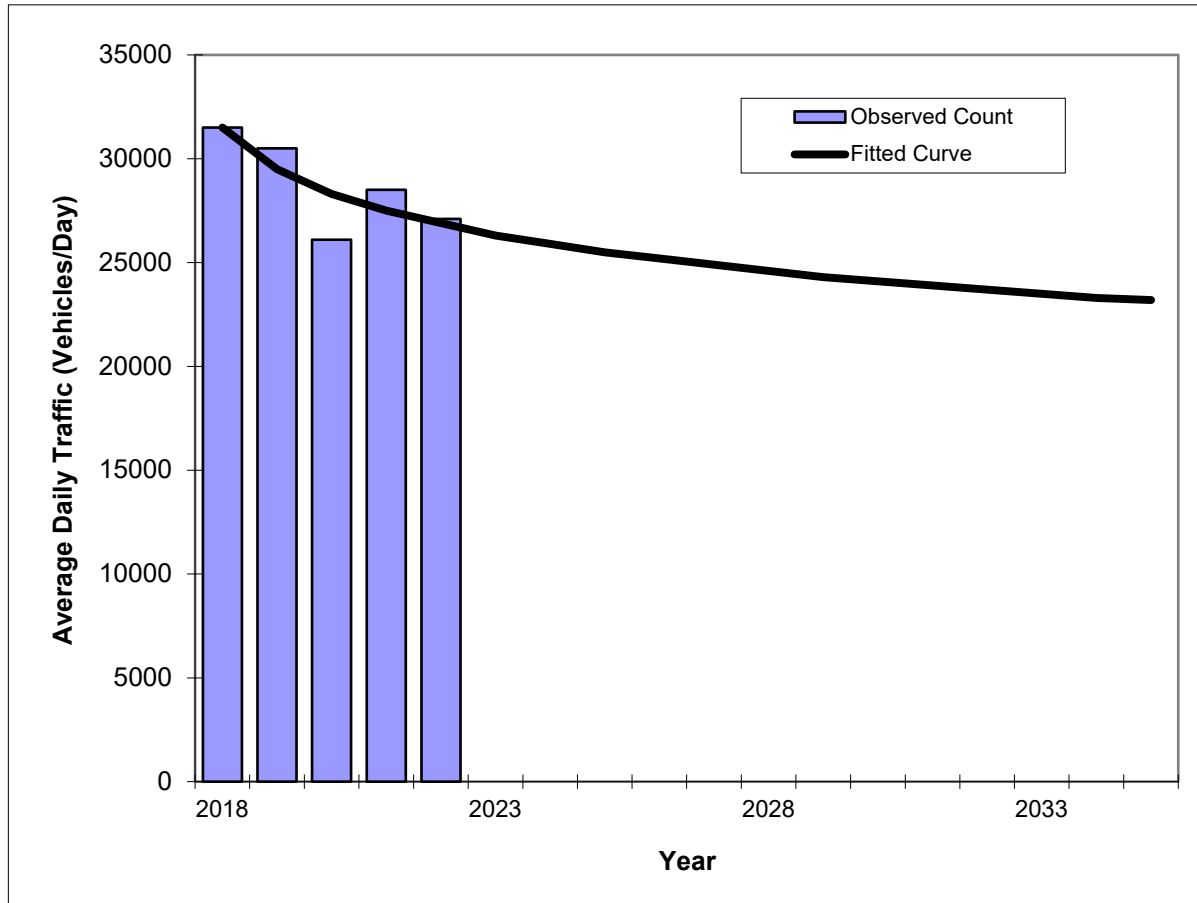
*Axle-Adjusted

Traffic Trends - V03.a

Howland Blvd, Wolf Pack Run to Catalina --

| | |
|----------|--|
| FIN# | |
| Location | |

| | |
|------------|---|
| County: | Volusia |
| Station #: | 903 |
| Highway: | Howland Blvd, Wolf Pack Run to Catalina |



| Year | Traffic (ADT/AADT) | |
|---------------------------|--------------------|---------|
| | Count* | Trend** |
| 2018 | 31500 | 31500 |
| 2019 | 30500 | 29500 |
| 2020 | 26100 | 28300 |
| 2021 | 28500 | 27500 |
| 2022 | 27100 | 26900 |
| 2025 Opening Year Trend | | |
| 2025 | N/A | 25500 |
| 2027 Mid-Year Trend | | |
| 2027 | N/A | 24900 |
| 2029 Design Year Trend | | |
| 2029 | N/A | 24300 |
| TRANPLAN Forecasts/Trends | | |
| | | |

| | |
|---|-----------|
| Trend R-squared: | 65.58% |
| Compounded Annual Historic Growth Rate: | -3.87% |
| Compounded Growth Rate (2022 to Design Year): | -1.44% |
| Printed: | 23-Feb-24 |
| Decaying Exponential Growth Option | |

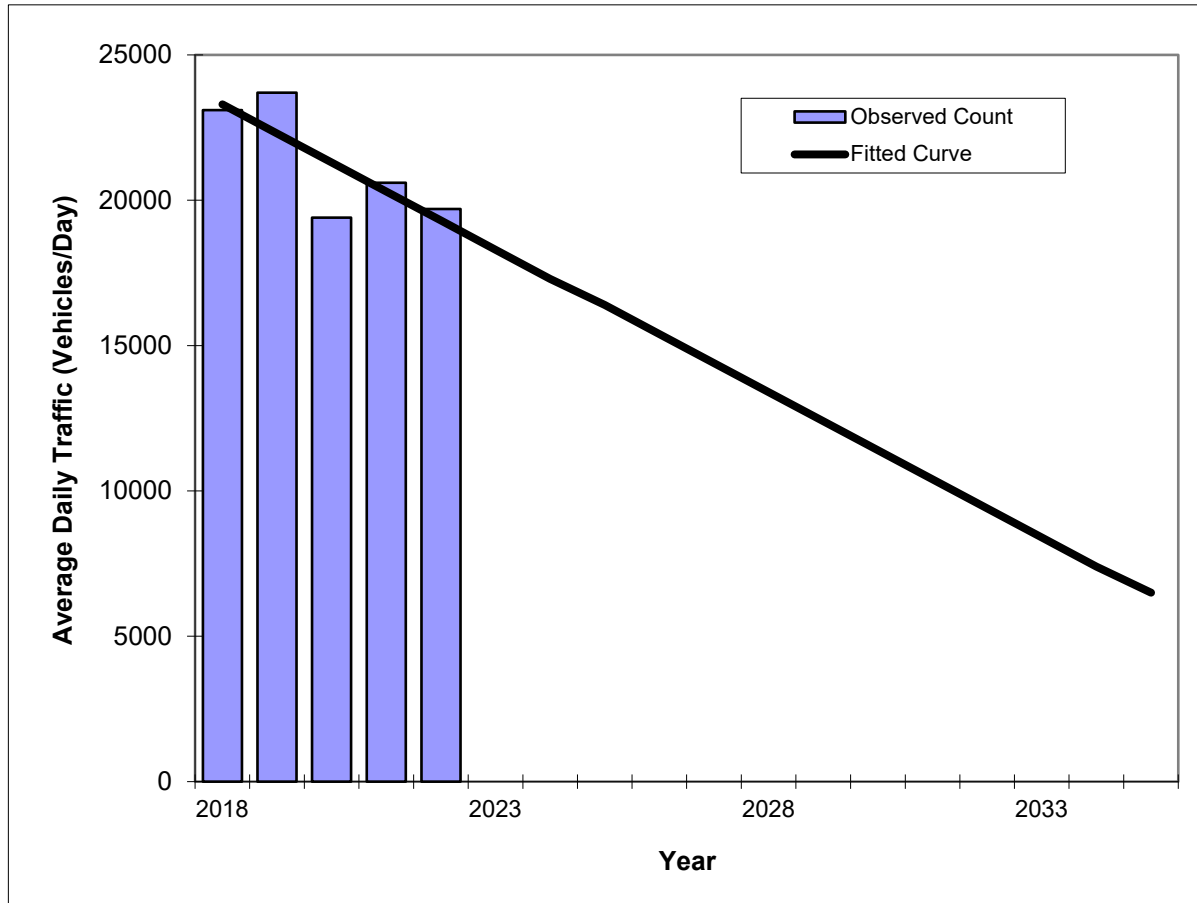
*Axle-Adjusted

Traffic Trends - V03.a

Howland Blvd, Catalina to Providence --

| | |
|----------|--|
| FIN# | |
| Location | |

| | |
|------------|--------------------------------------|
| County: | Volusia |
| Station #: | 905 |
| Highway: | Howland Blvd, Catalina to Providence |



| Year | Traffic (ADT/AADT) | |
|---------------------------|--------------------|---------|
| | Count* | Trend** |
| 2018 | 23100 | 23300 |
| 2019 | 23700 | 22300 |
| 2020 | 19400 | 21300 |
| 2021 | 20600 | 20300 |
| 2022 | 19700 | 19300 |
| 2025 Opening Year Trend | | |
| 2025 | N/A | 16400 |
| 2027 Mid-Year Trend | | |
| 2027 | N/A | 14400 |
| 2029 Design Year Trend | | |
| 2029 | N/A | 12400 |
| TRANPLAN Forecasts/Trends | | |
| | | |

| | |
|--|-----------|
| ** Annual Trend Increase: | -990 |
| Trend R-squared: | 62.59% |
| Trend Annual Historic Growth Rate: | -4.29% |
| Trend Growth Rate (2022 to Design Year): | -5.11% |
| Printed: | 23-Feb-24 |
| Straight Line Growth Option | |

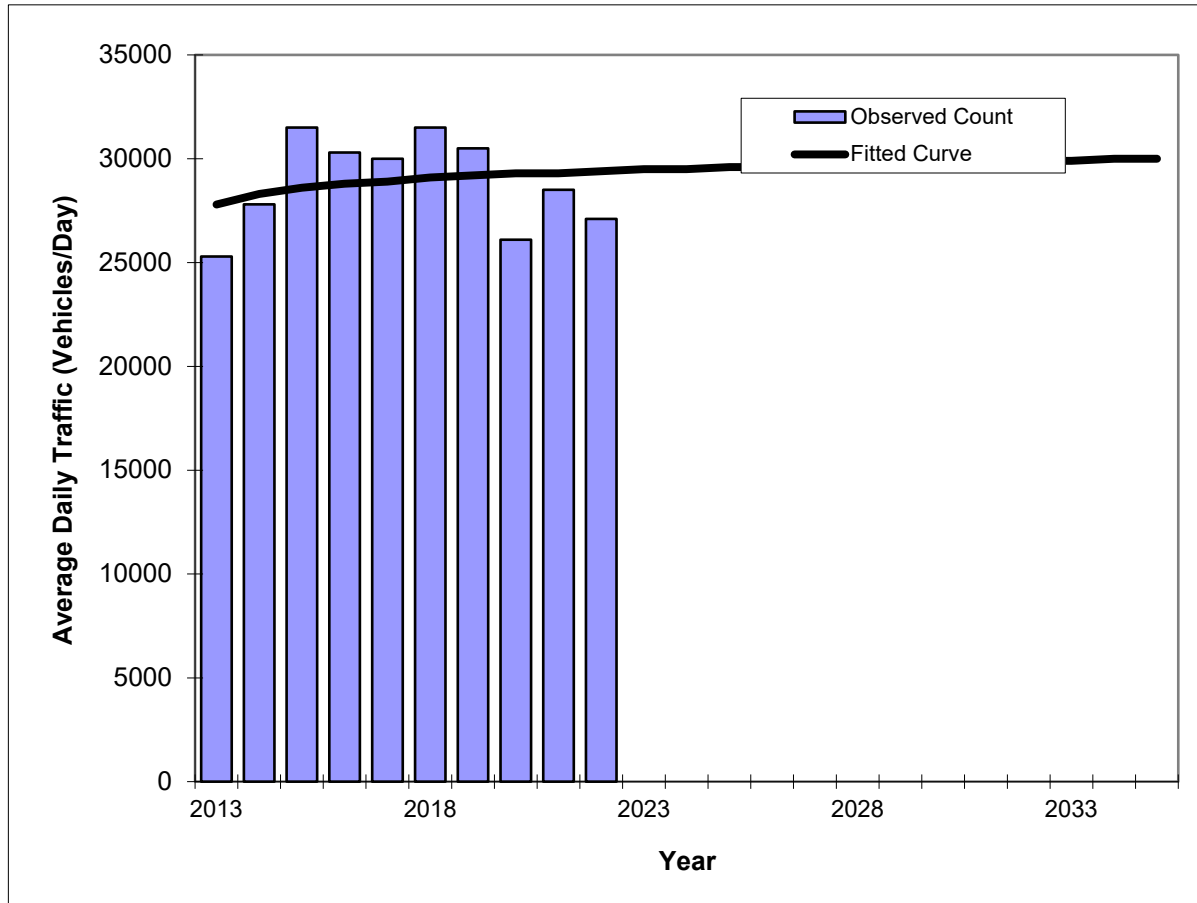
*Axle-Adjusted

Traffic Trends - V03.a

Howland Blvd, Wolf Pack Run to Catalina --

| | |
|----------|--|
| FIN# | |
| Location | |

| | |
|------------|---|
| County: | Volusia |
| Station #: | 903 |
| Highway: | Howland Blvd, Wolf Pack Run to Catalina |



| Year | Traffic (ADT/AADT) | |
|---------------------------|--------------------|---------|
| | Count* | Trend** |
| 2013 | 25300 | 27800 |
| 2014 | 27800 | 28300 |
| 2015 | 31500 | 28600 |
| 2016 | 30300 | 28800 |
| 2017 | 30000 | 28900 |
| 2018 | 31500 | 29100 |
| 2019 | 30500 | 29200 |
| 2020 | 26100 | 29300 |
| 2021 | 28500 | 29300 |
| 2022 | 27100 | 29400 |
| 2025 Opening Year Trend | | |
| 2025 | N/A | 29600 |
| 2027 Mid-Year Trend | | |
| 2027 | N/A | 29700 |
| 2029 Design Year Trend | | |
| 2029 | N/A | 29800 |
| TRANPLAN Forecasts/Trends | | |
| | | |

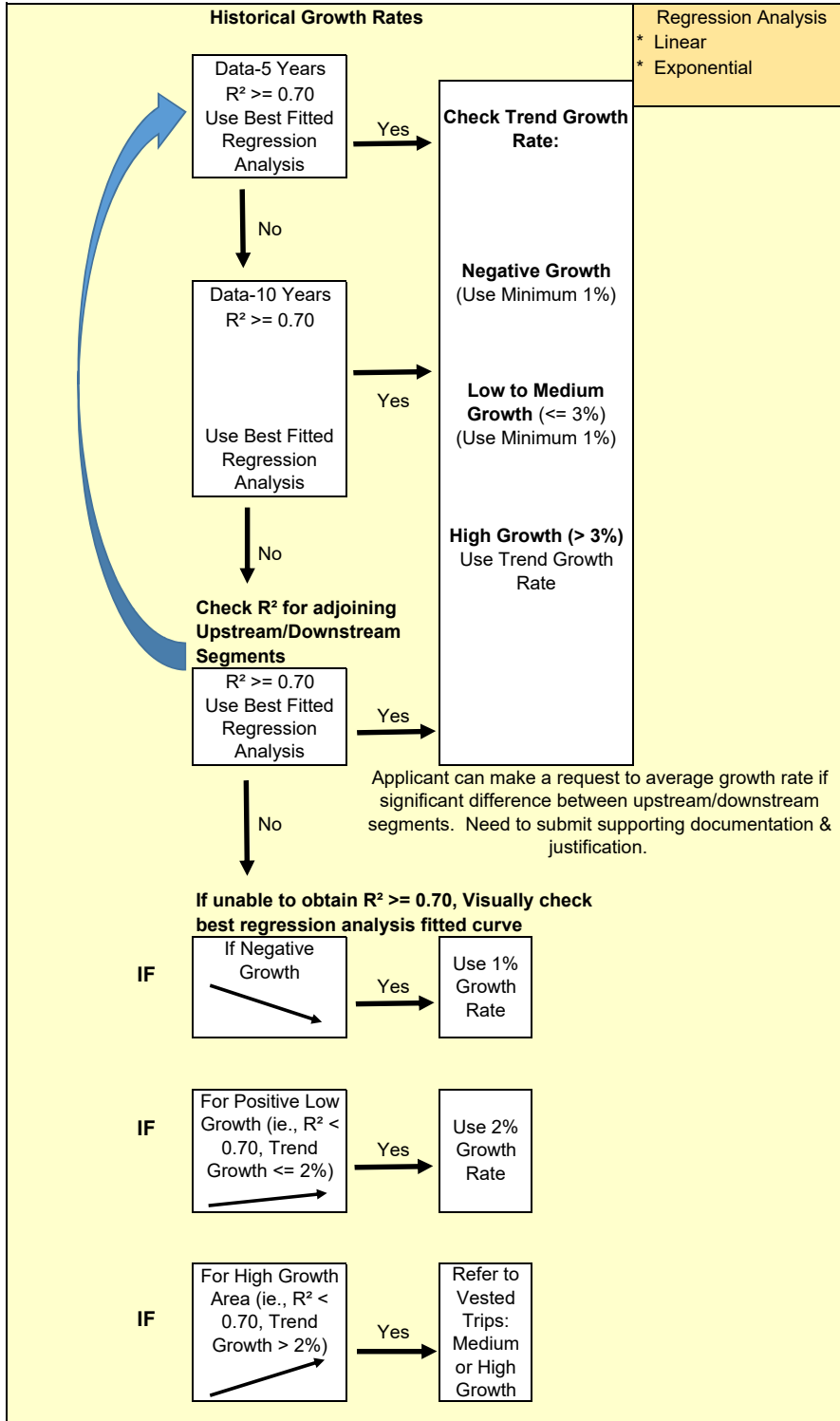
| | |
|---|-----------|
| Trend R-squared: | 5.15% |
| Compounded Annual Historic Growth Rate: | 0.62% |
| Compounded Growth Rate (2022 to Design Year): | 0.19% |
| Printed: | 23-Feb-24 |
| Decaying Exponential Growth Option | |

*Axle-Adjusted

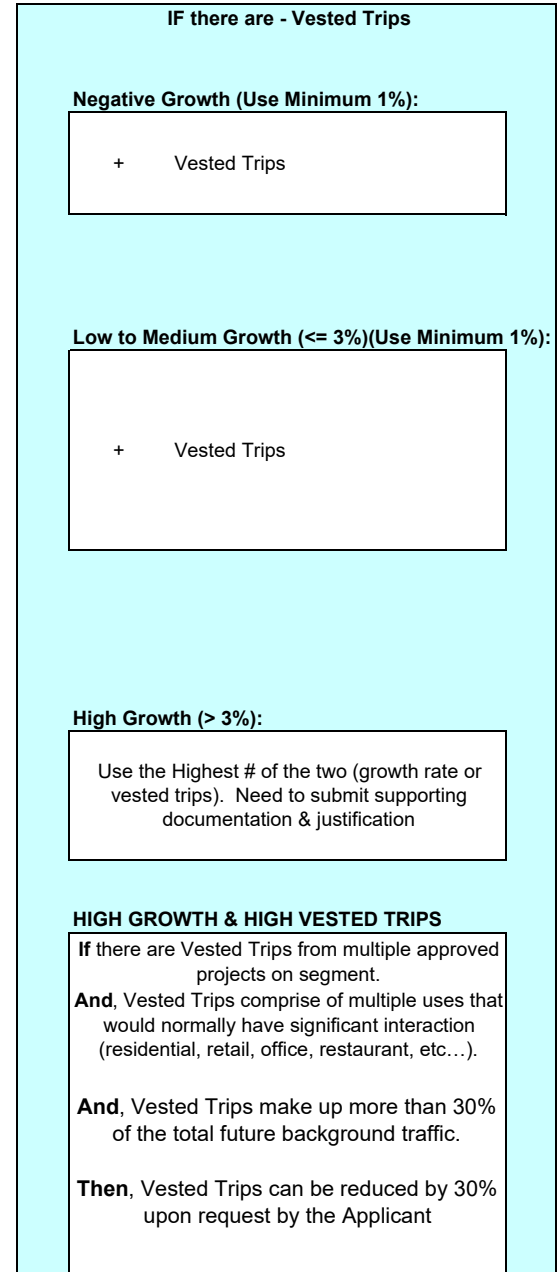
Background Growth Rate Determination Summary Table

| Roadway Segment | Future Background Volumes | | | | | | | | | |
|--|---------------------------|----------------|-------------------------------|---------------------|----------------|-------------------------------|--------------------------|---------------------------|-------------------------------|----------------------------|
| | 5 Year | | | 10 Year | | | Applied Growth | | | |
| | Best Fit Regression | R ² | Historical Annual Growth Rate | Best Fit Regression | R ² | Historical Annual Growth Rate | Applied Growth Procedure | Applicable R ² | Applicable Annual Growth Rate | Applied Annual Growth Rate |
| Lake Helen Osteen Road | | | | | | | | | | |
| Howland Blvd to Elkcaml Blvd | Straight Line | 24.8% | 2.9% | Exponential | 70.9% | 3.5% | Exponential | 70.9% | 3.5% | 3.5% |
| Elkcaml Blvd to Project | Decay Exp | 20.2% | -0.5% | Straight Line | 42.0% | 3.5% | Adjacent | 87.9% | 3.0% | 1.0% |
| Project to Haulover Blvd | Decay Exp | 20.2% | -0.5% | Straight Line | 42.0% | 3.5% | Adjacent | 87.9% | 3.0% | 1.0% |
| Haulover Blvd to Catalina Blvd | Straight Line | 62.2% | 3.2% | Exponential | 87.9% | 3.0% | Exponential | 87.9% | 3.0% | 1.0% |
| Catalina Blvd to Captain Dr | Straight Line | 13.9% | 1.5% | Exponential | 71.0% | 2.5% | Exponential | 71.0% | 2.5% | 1.0% |
| Catalina Boulevard | | | | | | | | | | |
| Eustace Ave to Howland Blvd | N/A | N/A | N/A | N/A | N/A | N/A | Adjacent | 89.9% | -1.9% | 1.0% |
| Howland Blvd to Lake Helen Osteen Rd | N/A | N/A | N/A | N/A | N/A | N/A | Adjacent | 87.9% | 3.0% | 1.0% |
| Elkcaml Boulevard | | | | | | | | | | |
| Howland Blvd to Lake Helen Osteen Rd | N/A | N/A | N/A | N/A | N/A | N/A | Adjacent | 70.9% | 3.5% | 3.5% |
| Lake Helen-Osteen Rd to Courtland Blvd | N/A | N/A | N/A | N/A | N/A | N/A | Adjacent | 70.9% | 3.5% | 3.5% |
| Howland Boulevard | | | | | | | | | | |
| Providence Blvd to Catalina Blvd | Linear | 62.6% | -5.1% | Exponential | 14.4% | -1.2% | Adjacent | 89.9% | -1.9% | 1.0% |
| Catalina Blvd to Wolf Pack Run | Decay Exp | 65.6% | -1.4% | Decay Exp | 5.2% | 0.2% | Adjacent | 89.9% | -1.9% | 1.0% |
| Wolf Pack Run to I-4 | Decay Exp | 89.9% | -1.9% | Decay Exp | 8.6% | 0.3% | Decay Exp | 89.9% | -1.9% | 1.0% |
| Providence Boulevard | | | | | | | | | | |
| Fort Smith Blvd to Elkcaml Blvd | Decay Exp | 17.4% | -0.2% | Exponential | 4.7% | -0.3% | Decay Exp | 17.4% | -0.2% | 1.0% |

Volusia County's Segment Growth Rates and Vested Trips Instructions Policy



AND



Signed: _____
 Jon E. Cheney, P.E.

Date: _____

Appendix F

Turning Movement Worksheets



Howland Boulevard at Catalina Boulevard AM Peak Hour

Existing TMCs

| | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | |
|----------------|-----------|-----|-----|----|-----------|----|-----|----|------------|-----|-----|----|------------|-----|----|-----|
| | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| Existing Count | 0 | 116 | 513 | 31 | 1 | 28 | 977 | 75 | 0 | 106 | 106 | 34 | 0 | 124 | 97 | 487 |
| Date of Count | 1/18/2024 | | | | SF | | | | 1.02 | | | | | | | |
| Adjusted Count | 0 | 118 | 523 | 32 | 1 | 29 | 997 | 77 | 0 | 108 | 108 | 35 | 0 | 126 | 99 | 497 |

| | West Leg | | | | East Leg | | | | South Leg | | | | North Leg | | | |
|--|-----------|--|--|--|-----------|--|--|--|-----------|--|--|--|-----------|--|--|--|
| Existing Approach & Departure Volumes | EB: 673 | | | | EB: 685 | | | | NB: 251 | | | | NB: 303 | | | |
| | WB: 1,602 | | | | WB: 1,104 | | | | SB: 160 | | | | SB: 722 | | | |
| Directional Factors Based on Existing Counts | EB: 0.30 | | | | EB: 0.38 | | | | NB: 0.61 | | | | NB: 0.30 | | | |
| | WB: 0.70 | | | | WB: 0.62 | | | | SB: 0.39 | | | | SB: 0.70 | | | |

Future Background Year 2029

| | | | | | | | | | | | | | | | | |
|--------------------------|------|------|------|------|------|------|-------|------|------|------|------|------|------|------|------|------|
| Annual Growth Rate | 1.0% | 1.0% | 1.0% | 1.0% | 1.0% | 1.0% | 1.0% | 1.0% | 1.0% | 1.0% | 1.0% | 1.0% | 1.0% | 1.0% | 1.0% | 1.0% |
| Simple Volume Growth | 0 | 6 | 26 | 2 | 0 | 1 | 50 | 4 | 0 | 5 | 5 | 2 | 0 | 6 | 5 | 25 |
| Applied Bckgrnd Growth | 0 | 6 | 26 | 2 | 0 | 1 | 50 | 4 | 0 | 5 | 5 | 2 | 0 | 6 | 5 | 25 |
| Total Bckgrnd Pk-Hr Vols | 0 | 124 | 549 | 34 | 1 | 30 | 1,047 | 81 | 0 | 113 | 113 | 37 | 0 | 132 | 104 | 522 |

Project Trips

| | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | |
|---------------------|-----------|-------|------|------|-----------|------|------|------|------------|------|------|------|------------|------|------|-------|
| | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| New Ext Inbound | 0.0% | 27.4% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 1.5% | 0.0% | 0.0% | 2.9% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| Volume | 0 | 16 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 |
| New Ext Outbound | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 1.5% | 2.9% | 27.4% |
| Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 18 |
| Pass-By Inbound | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-By Outbound | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Project Trips | 0 | 16 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 2 | 0 | 0 | 1 | 2 | 18 |

| | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | |
|---------------------|-----------|-----|-----|----|-----------|----|-------|----|------------|-----|-----|----|------------|-----|-----|-----|
| | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| Total Pk-Hr Volumes | 0 | 140 | 549 | 34 | 1 | 30 | 1,047 | 82 | 0 | 113 | 115 | 37 | 0 | 133 | 106 | 540 |

Howland Boulevard at Catalina Boulevard

PM Peak Hour

Existing TMCs

| | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | |
|----------------|-----------|-----|-------|----|-----------|----|-----|----|------------|----|----|----|------------|-----|----|-----|
| | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| Existing Count | 0 | 400 | 1,089 | 60 | 2 | 43 | 611 | 66 | 0 | 45 | 85 | 19 | 0 | 124 | 85 | 238 |
| Date of Count | 1/18/2024 | | | | SF | | | | 1.02 | | | | | | | |
| Adjusted Count | 0 | 408 | 1,111 | 61 | 2 | 44 | 623 | 67 | 0 | 46 | 87 | 19 | 0 | 126 | 87 | 243 |

| | West Leg | | | | East Leg | | | | South Leg | | | | North Leg | | | |
|--|-----------|--|--|--|-----------|--|--|--|-----------|--|--|--|-----------|--|--|--|
| Existing Approach & Departure Volumes | EB: 1,580 | | | | EB: 1,258 | | | | NB: 152 | | | | NB: 562 | | | |
| | WB: 912 | | | | WB: 736 | | | | SB: 192 | | | | SB: 456 | | | |
| Directional Factors Based on Existing Counts | EB: 0.63 | | | | EB: 0.63 | | | | NB: 0.44 | | | | NB: 0.55 | | | |
| | WB: 0.37 | | | | WB: 0.37 | | | | SB: 0.56 | | | | SB: 0.45 | | | |

Future Background Year 2029

| | | | | | | | | | | | | | | | | |
|--------------------------|------|------|-------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| Annual Growth Rate | 1.0% | 1.0% | 1.0% | 1.0% | 1.0% | 1.0% | 1.0% | 1.0% | 1.0% | 1.0% | 1.0% | 1.0% | 1.0% | 1.0% | 1.0% | 1.0% |
| Simple Volume Growth | 0 | 20 | 56 | 3 | 0 | 2 | 31 | 3 | 0 | 2 | 4 | 1 | 0 | 6 | 4 | 12 |
| Applied Bckgrnd Growth | 0 | 20 | 56 | 3 | 0 | 2 | 31 | 3 | 0 | 2 | 4 | 1 | 0 | 6 | 4 | 12 |
| Total Bckgrnd Pk-Hr Vols | 0 | 428 | 1,167 | 64 | 2 | 46 | 654 | 70 | 0 | 48 | 91 | 20 | 0 | 132 | 91 | 255 |

Project Trips

| | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | |
|---------------------|-----------|-------|------|------|-----------|------|------|------|------------|------|------|------|------------|------|------|-------|
| | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| New Ext Inbound | 0.0% | 27.4% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 1.5% | 0.0% | 0.0% | 2.9% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| Volume | 0 | 17 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 |
| New Ext Outbound | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 1.5% | 2.9% | 27.4% |
| Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 19 |
| Pass-By Inbound | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-By Outbound | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Project Trips | 0 | 17 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 2 | 0 | 0 | 1 | 2 | 19 |

| | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | |
|---------------------|-----------|-----|-------|----|-----------|----|-----|----|------------|----|----|----|------------|-----|----|-----|
| | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| Total Pk-Hr Volumes | 0 | 445 | 1,167 | 64 | 2 | 46 | 654 | 71 | 0 | 48 | 93 | 20 | 0 | 133 | 93 | 274 |

Lake Helen Osteen Road at Catalina Boulevard

AM Peak Hour

Existing TMCs

| | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | |
|----------------|-----------|----|---|-----|-----------|---|---|---|------------|-----|-----|---|------------|---|-----|-----|
| | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| Existing Count | 0 | 54 | 0 | 107 | 0 | 0 | 0 | 0 | 0 | 418 | 384 | 0 | 0 | 0 | 199 | 179 |
| Date of Count | 1/18/2024 | | | | SF | | | | 1.02 | | | | | | | |
| Adjusted Count | 0 | 55 | 0 | 109 | 0 | 0 | 0 | 0 | 0 | 426 | 392 | 0 | 0 | 0 | 203 | 183 |

| | West Leg | | | | East Leg | | | | South Leg | | | | North Leg | | | |
|--|----------|--|--|--|-------------|--|--|--|-----------|--|--|--|-----------|--|--|--|
| Existing Approach & Departure Volumes | EB: 164 | | | | EB: 0 | | | | NB: 818 | | | | NB: 447 | | | |
| | WB: 609 | | | | WB: 0 | | | | SB: 312 | | | | SB: 386 | | | |
| Directional Factors Based on Existing Counts | EB: 0.21 | | | | EB: #DIV/0! | | | | NB: 0.72 | | | | NB: 0.54 | | | |
| | WB: 0.79 | | | | WB: #DIV/0! | | | | SB: 0.28 | | | | SB: 0.46 | | | |

Future Background Year 2029

| | | | | | | | | | | | | | | | | |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| Annual Growth Rate | 1.0% | 1.0% | 1.0% | 1.0% | 0.0% | 0.0% | 0.0% | 0.0% | 1.0% | 1.0% | 1.0% | 1.0% | 1.0% | 1.0% | 1.0% | 1.0% |
| Simple Volume Growth | 0 | 3 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 21 | 20 | 0 | 0 | 0 | 10 | 9 |
| Applied Bckgrnd Growth | 0 | 3 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 21 | 20 | 0 | 0 | 0 | 10 | 9 |
| Total Bckgrnd Pk-Hr Vols | 0 | 58 | 0 | 114 | 0 | 0 | 0 | 0 | 0 | 447 | 412 | 0 | 0 | 0 | 213 | 192 |

Project Trips

| | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | |
|-------------------------|-----------|------|------|-------|-----------|------|------|------|------------|-------|-------|------|------------|------|-------|------|
| | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| New Ext Inbound Volume | 0.0% | 0.0% | 0.0% | 32.7% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 22.8% | 0.0% |
| | 0 | 0 | 0 | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14 | 0 |
| New Ext Outbound Volume | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 32.7% | 22.8% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 21 | 15 | 0 | 0 | 0 | 0 | 0 |
| Pass-By Inbound Volume | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-By Outbound Volume | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Project Trips | 0 | 0 | 0 | 20 | 0 | 0 | 0 | 0 | 0 | 21 | 15 | 0 | 0 | 0 | 14 | 0 |

| | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | |
|---------------------|-----------|----|---|-----|-----------|---|---|---|------------|-----|-----|---|------------|---|-----|-----|
| | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| Total Pk-Hr Volumes | 0 | 58 | 0 | 134 | 0 | 0 | 0 | 0 | 0 | 468 | 427 | 0 | 0 | 0 | 227 | 192 |

Lake Helen Osteen Road at Catalina Boulevard

PM Peak Hour

Existing TMCs

| | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | |
|----------------|-----------|-----|---|-----|-----------|---|---|---|------------|-----|-----|---|------------|---|-----|----|
| | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| Existing Count | 0 | 169 | 0 | 336 | 0 | 0 | 0 | 0 | 0 | 195 | 166 | 0 | 0 | 0 | 355 | 93 |
| Date of Count | 1/18/2024 | | | | SF | | | | 1.02 | | | | | | | |
| Adjusted Count | 0 | 172 | 0 | 343 | 0 | 0 | 0 | 0 | 0 | 199 | 169 | 0 | 0 | 0 | 362 | 95 |

| | West Leg | | | | East Leg | | | | South Leg | | | | North Leg | | | |
|--|----------|--|--|--|-------------|--|--|--|-----------|--|--|--|-----------|--|--|--|
| Existing Approach & Departure Volumes | EB: 515 | | | | EB: 0 | | | | NB: 368 | | | | NB: 341 | | | |
| | WB: 294 | | | | WB: 0 | | | | SB: 705 | | | | SB: 457 | | | |
| Directional Factors Based on Existing Counts | EB: 0.64 | | | | EB: #DIV/0! | | | | NB: 0.34 | | | | NB: 0.43 | | | |
| | WB: 0.36 | | | | WB: #DIV/0! | | | | SB: 0.66 | | | | SB: 0.57 | | | |

Future Background Year 2029

| | | | | | | | | | | | | | | | | |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| Annual Growth Rate | 1.0% | 1.0% | 1.0% | 1.0% | 0.0% | 0.0% | 0.0% | 0.0% | 1.0% | 1.0% | 1.0% | 1.0% | 1.0% | 1.0% | 1.0% | 1.0% |
| Simple Volume Growth | 0 | 9 | 0 | 17 | 0 | 0 | 0 | 0 | 0 | 10 | 8 | 0 | 0 | 0 | 18 | 5 |
| Applied Bckgrnd Growth | 0 | 9 | 0 | 17 | 0 | 0 | 0 | 0 | 0 | 10 | 8 | 0 | 0 | 0 | 18 | 5 |
| Total Bckgrnd Pk-Hr Vols | 0 | 181 | 0 | 360 | 0 | 0 | 0 | 0 | 0 | 209 | 177 | 0 | 0 | 0 | 380 | 100 |

Project Trips

| | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | |
|-------------------------|-----------|------|------|-------|-----------|------|------|------|------------|-------|-------|------|------------|------|-------|------|
| | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| New Ext Inbound Volume | 0.0% | 0.0% | 0.0% | 32.7% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 22.8% | 0.0% |
| | 0 | 0 | 0 | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14 | 0 |
| New Ext Outbound Volume | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 32.7% | 22.8% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 22 | 16 | 0 | 0 | 0 | 0 | 0 |
| Pass-By Inbound Volume | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-By Outbound Volume | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Project Trips | 0 | 0 | 0 | 20 | 0 | 0 | 0 | 0 | 0 | 22 | 16 | 0 | 0 | 0 | 14 | 0 |

| | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | |
|---------------------|-----------|-----|---|-----|-----------|---|---|---|------------|-----|-----|---|------------|---|-----|-----|
| | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| Total Pk-Hr Volumes | 0 | 181 | 0 | 380 | 0 | 0 | 0 | 0 | 0 | 231 | 193 | 0 | 0 | 0 | 394 | 100 |

Lake Helen Osteen Road at Driveway #1

AM Peak Hour

Existing TMCs

| | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | |
|----------------|-----------|---|---|---|-----------|---|---|---|------------|---|-----|---|------------|---|-----|---|
| | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| Existing Count | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 7 | 0 | 0 | 464 | 0 | 0 | 0 | 230 | 0 |
| Date of Count | 1/18/2024 | | | | SF | | | | 1.02 | | | | | | | |
| Adjusted Count | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 7 | 0 | 0 | 473 | 0 | 0 | 0 | 235 | 0 |

| | West Leg | | | | East Leg | | | | South Leg | | | | North Leg | | | |
|--|-------------|--|--|--|----------|--|--|--|-----------|--|--|--|-----------|--|--|--|
| Existing Approach & Departure Volumes | EB: 0 | | | | EB: 0 | | | | NB: 473 | | | | NB: 480 | | | |
| | WB: 0 | | | | WB: 10 | | | | SB: 238 | | | | SB: 235 | | | |
| Directional Factors Based on Existing Counts | EB: #DIV/0! | | | | EB: 0.00 | | | | NB: 0.67 | | | | NB: 0.67 | | | |
| | WB: #DIV/0! | | | | WB: 1.00 | | | | SB: 0.33 | | | | SB: 0.33 | | | |

Future Background

Year 2029

| | | | | | | | | | | | | | | | | |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| Annual Growth Rate | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 1.0% | 0.0% | 0.0% | 0.0% | 1.0% | 0.0% |
| Simple Volume Growth | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 24 | 0 | 0 | 0 | 12 | 0 |
| Applied Bckgrnd Growth | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 24 | 0 | 0 | 0 | 12 | 0 |
| Total Bckgrnd Pk-Hr Vols | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 7 | 0 | 0 | 497 | 0 | 0 | 0 | 247 | 0 |

Project Trips

| | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | |
|--------------------------------------|-----------|------|------|------|-----------|-------|------|-------|------------|------|-------|------|------------|------|-------|------|
| | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| Westside Development | | | | | | | | | | | | | | | | |
| New Ext Inbound | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 61.2% | 0.0% |
| Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 0 |
| New Ext Outbound | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 61.2% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 28 | 0 | 0 | 0 | 0 | 0 |
| Eastside Development | | | | | | | | | | | | | | | | |
| New Ext Inbound | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 61.2% | 0.0% |
| Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 51 | 0 |
| New Ext Outbound | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 11.0% | 0.0% | 25.0% | 0.0% | 0.0% | 36.2% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| Volume | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 13 | 0 | 0 | 18 | 0 | 0 | 0 | 0 | 0 |
| Pass-By Inbound | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-By Outbound | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Project Trips in Counts | 0 | 0 | 0 | 0 | 0 | -3 | 0 | -7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total New External Trips at Buildout | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 13 | 0 | 0 | 46 | 0 | 0 | 0 | 60 | 0 |
| Total Pass-By Trips at Buildout | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Net Change in Project Trips | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 6 | 0 | 0 | 46 | 0 | 0 | 0 | 60 | 0 |

| | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | |
|---------------------|-----------|---|---|---|-----------|---|---|----|------------|---|-----|---|------------|---|-----|---|
| | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| Total Pk-Hr Volumes | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 13 | 0 | 0 | 543 | 0 | 0 | 0 | 307 | 0 |

Lake Helen Osteen Road at Driveway #1

PM Peak Hour

Existing TMCs

| | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | |
|----------------|-----------|---|---|---|-----------|---|---|---|------------|---|-----|---|------------|---|-----|---|
| | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| Existing Count | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 6 | 0 | 0 | 258 | 0 | 0 | 0 | 436 | 0 |
| Date of Count | 1/18/2024 | | | | SF | | | | 1.02 | | | | | | | |
| Adjusted Count | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 6 | 0 | 0 | 263 | 0 | 0 | 0 | 445 | 0 |

| | West Leg | | | | East Leg | | | | South Leg | | | | North Leg | | | |
|--|-------------|--|--|--|----------|--|--|--|-----------|--|--|--|-----------|--|--|--|
| Existing Approach & Departure Volumes | EB: 0 | | | | EB: 0 | | | | NB: 263 | | | | NB: 269 | | | |
| | WB: 0 | | | | WB: 11 | | | | SB: 450 | | | | SB: 445 | | | |
| Directional Factors Based on Existing Counts | EB: #DIV/0! | | | | EB: 0.00 | | | | NB: 0.37 | | | | NB: 0.38 | | | |
| | WB: #DIV/0! | | | | WB: 1.00 | | | | SB: 0.63 | | | | SB: 0.62 | | | |

Future Background

Year 2029

| | | | | | | | | | | | | | | | | |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| Annual Growth Rate | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 1.0% | 0.0% | 0.0% | 0.0% | 1.0% | 0.0% |
| Simple Volume Growth | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 | 0 | 0 | 0 | 22 | 0 |
| Applied Bckgrnd Growth | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 | 0 | 0 | 0 | 22 | 0 |
| Total Bckgrnd Pk-Hr Vols | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 6 | 0 | 0 | 276 | 0 | 0 | 0 | 467 | 0 |

Project Trips

| | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | |
|--------------------------------------|-----------|------|------|------|-----------|-------|------|-------|------------|------|--------|------|------------|------|-------|------|
| | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| Westside Development | | | | | | | | | | | | | | | | |
| New Ext Inbound | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 61.2% | 0.0% |
| Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 28 | 0 |
| New Ext Outbound | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 61.2% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 17 | 0 | 0 | 0 | 0 | 0 |
| Eastside Development | | | | | | | | | | | | | | | | |
| New Ext Inbound | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 61.2% | 0.0% |
| Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 23 | 0 |
| New Ext Outbound | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 6.0% | 0.0% | 15.0% | 0.0% | 0.0% | 46.2% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| Volume | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 9 | 0 | 0 | 29 | 0 | 0 | 0 | 0 | 0 |
| Pass-By Inbound | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-By Outbound | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 20.0% | 0.0% | 20.0% | 0.0% | 0.0% | -20.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| Volume | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 0 | 0 | -4 | 0 | 0 | 0 | 0 | 0 |
| Existing Project Trips in Counts | 0 | 0 | 0 | 0 | 0 | -5 | 0 | -6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total New External Trips at Buildout | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 9 | 0 | 0 | 46 | 0 | 0 | 0 | 51 | 0 |
| Total Pass-By Trips at Buildout | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 0 | 0 | -4 | 0 | 0 | 0 | 0 | 0 |
| Net Change in Project Trips | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 7 | 0 | 0 | 42 | 0 | 0 | 0 | 51 | 0 |

| | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | |
|---------------------|-----------|---|---|---|-----------|---|---|----|------------|---|-----|---|------------|---|-----|---|
| | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| Total Pk-Hr Volumes | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 13 | 0 | 0 | 318 | 0 | 0 | 0 | 518 | 0 |

Lake Helen Osteen Road at Driveway #2

AM Peak Hour

Existing TMCs

| | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | |
|----------------|-----------|---|---|---|-----------|---|---|---|------------|---|-----|---|------------|---|-----|---|
| | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| Existing Count | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 465 | 5 | 0 | 7 | 223 | 0 |
| Date of Count | 1/18/2024 | | | | SF | | | | 1.02 | | | | | | | |
| Adjusted Count | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 474 | 5 | 0 | 7 | 227 | 0 |

| | West Leg | | | | East Leg | | | | South Leg | | | | North Leg | | | |
|--|-------------|--|--|--|----------|--|--|--|-----------|--|--|--|-----------|--|--|--|
| Existing Approach & Departure Volumes | EB: 0 | | | | EB: 12 | | | | NB: 479 | | | | NB: 474 | | | |
| | WB: 0 | | | | WB: 0 | | | | SB: 227 | | | | SB: 234 | | | |
| Directional Factors Based on Existing Counts | EB: #DIV/0! | | | | EB: 1.00 | | | | NB: 0.68 | | | | NB: 0.67 | | | |
| | WB: #DIV/0! | | | | WB: 0.00 | | | | SB: 0.32 | | | | SB: 0.33 | | | |

Future Background

Year 2029

| | | | | | | | | | | | | | | | | |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| Annual Growth Rate | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 1.0% | 0.0% | 0.0% | 0.0% | 1.0% | 0.0% |
| Simple Volume Growth | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 24 | 0 | 0 | 0 | 11 | 0 |
| Applied Bckgrnd Growth | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 24 | 0 | 0 | 0 | 11 | 0 |
| Total Bckgrnd Pk-Hr Vols | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 498 | 5 | 0 | 7 | 238 | 0 |

Project Trips

| | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | |
|--------------------------------------|-----------|-------|------|-------|-----------|-------|------|-------|------------|-------|------|-------|------------|-------|-------|-------|
| | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| Westside Development | | | | | | | | | | | | | | | | |
| New Ext Inbound | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 38.8% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 61.2% |
| Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 9 |
| New Ext Outbound | 0.0% | 61.2% | 0.0% | 38.8% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| Volume | 0 | 28 | 0 | 18 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Eastside Development | | | | | | | | | | | | | | | | |
| New Ext Inbound | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 38.8% | 0.0% | 61.2% | 0.0% | 0.0% |
| Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 32 | 0 | 51 | 0 | 0 |
| New Ext Outbound | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 27.8% | 0.0% | 36.2% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 11.0% | 0.0% |
| Volume | 0 | 0 | 0 | 0 | 0 | 14 | 0 | 18 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 0 |
| Pass-By Inbound | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-By Outbound | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Project Trips in Counts | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -5 | 0 | -7 | 0 | 0 |
| Total New External Trips at Buildout | 0 | 28 | 0 | 18 | 0 | 14 | 0 | 18 | 0 | 5 | 0 | 32 | 0 | 51 | 6 | 9 |
| Total Pass-By Trips at Buildout | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Net Change in Project Trips | 0 | 28 | 0 | 18 | 0 | 14 | 0 | 18 | 0 | 5 | 0 | 27 | 0 | 44 | 6 | 9 |

| | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | |
|---------------------|-----------|----|---|----|-----------|----|---|----|------------|---|-----|----|------------|----|-----|---|
| | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| Total Pk-Hr Volumes | 0 | 28 | 0 | 18 | 0 | 14 | 0 | 18 | 0 | 5 | 498 | 32 | 0 | 51 | 244 | 9 |

Lake Helen Osteen Road at Driveway #2

PM Peak Hour

Existing TMCs

| | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | |
|----------------|-----------|---|---|---|-----------|---|---|---|------------|---|-----|---|------------|---|-----|---|
| | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| Existing Count | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 259 | 2 | 0 | 5 | 436 | 0 |
| Date of Count | 1/18/2024 | | | | SF | | | | 1.02 | | | | | | | |
| Adjusted Count | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 264 | 2 | 0 | 5 | 445 | 0 |

| | West Leg | | East Leg | | South Leg | | North Leg | |
|--|-------------|--|----------|--|-----------|--|-----------|--|
| Existing Approach & Departure Volumes | EB: 0 | | EB: 7 | | NB: 266 | | NB: 264 | |
| | WB: 0 | | WB: 0 | | SB: 445 | | SB: 450 | |
| Directional Factors Based on Existing Counts | EB: #DIV/0! | | EB: 1.00 | | NB: 0.37 | | NB: 0.37 | |
| | WB: #DIV/0! | | WB: 0.00 | | SB: 0.63 | | SB: 0.63 | |

Future Background

Year 2029

| | | | | | | | | | | | | | | | | |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| Annual Growth Rate | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 1.0% | 0.0% | 0.0% | 0.0% | 1.0% | 0.0% |
| Simple Volume Growth | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 | 0 | 0 | 0 | 22 | 0 |
| Applied Bckgrnd Growth | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 | 0 | 0 | 0 | 22 | 0 |
| Total Bckgrnd Pk-Hr Vols | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 277 | 2 | 0 | 5 | 467 | 0 |

Project Trips

| | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | |
|--------------------------------------|-----------|-------|------|-------|-----------|-------|------|-------|------------|-------|--------|-------|------------|-------|--------|-------|
| | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| Westside Development | | | | | | | | | | | | | | | | |
| New Ext Inbound | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 38.8% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 61.2% |
| Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 17 | 0 | 0 | 0 | 0 | 0 | 28 |
| New Ext Outbound | 0.0% | 61.2% | 0.0% | 38.8% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| Volume | 0 | 17 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Eastside Development | | | | | | | | | | | | | | | | |
| New Ext Inbound | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 38.8% | 0.0% | 61.2% | 0.0% | 0.0% |
| Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14 | 0 | 23 | 0 | 0 |
| New Ext Outbound | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 32.8% | 0.0% | 46.2% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 6.0% | 0.0% |
| Volume | 0 | 0 | 0 | 0 | 0 | 21 | 0 | 29 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 |
| Pass-By Inbound | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | -40.0% | 40.0% | 0.0% | 60.0% | -60.0% | 0.0% |
| Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -8 | 8 | 0 | 11 | -11 | 0 |
| Pass-By Outbound | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 40.0% | 0.0% | 20.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 20.0% | 0.0% |
| Volume | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 |
| Existing Project Trips in Counts | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | 0 | -5 | 0 | 0 |
| Total New External Trips at Buildout | 0 | 17 | 0 | 10 | 0 | 21 | 0 | 29 | 0 | 17 | 0 | 14 | 0 | 23 | 4 | 28 |
| Total Pass-By Trips at Buildout | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 4 | 0 | 0 | -8 | 8 | 0 | 11 | -7 | 0 |
| Net Change in Project Trips | 0 | 17 | 0 | 10 | 0 | 29 | 0 | 33 | 0 | 17 | -8 | 20 | 0 | 29 | -3 | 28 |

| | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | |
|---------------------|-----------|----|---|----|-----------|----|---|----|------------|----|-----|----|------------|----|-----|----|
| | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| Total Pk-Hr Volumes | 0 | 17 | 0 | 10 | 0 | 29 | 0 | 33 | 0 | 17 | 269 | 22 | 0 | 34 | 464 | 28 |

Lake Helen Osteen Road at Elkcarn Boulevard AM Peak Hour

Existing TMCs

| | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | |
|----------------|-----------|----|-----|----|-----------|-----|-----|----|------------|---|-----|----|------------|---|-----|----|
| | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| Existing Count | 0 | 82 | 124 | 14 | 0 | 108 | 253 | 16 | 0 | 7 | 202 | 46 | 0 | 6 | 224 | 96 |
| Date of Count | 1/18/2024 | | | | SF | | | | 1.02 | | | | | | | |
| Adjusted Count | 0 | 84 | 126 | 14 | 0 | 110 | 258 | 16 | 0 | 7 | 206 | 47 | 0 | 6 | 228 | 98 |

| | West Leg | | | | East Leg | | | | South Leg | | | | North Leg | | | |
|--|----------|--|--|--|----------|--|--|--|-----------|--|--|--|-----------|--|--|--|
| Existing Approach & Departure Volumes | EB: 224 | | | | EB: 179 | | | | NB: 260 | | | | NB: 306 | | | |
| | WB: 363 | | | | WB: 384 | | | | SB: 352 | | | | SB: 332 | | | |
| Directional Factors Based on Existing Counts | EB: 0.38 | | | | EB: 0.32 | | | | NB: 0.42 | | | | NB: 0.48 | | | |
| | WB: 0.62 | | | | WB: 0.68 | | | | SB: 0.58 | | | | SB: 0.52 | | | |

Future Background Year 2029

| | | | | | | | | | | | | | | | | | |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| Annual Growth Rate | 3.5% | 3.5% | 3.5% | 3.5% | 3.5% | 3.5% | 3.5% | 3.5% | 3.5% | 3.5% | 3.5% | 3.5% | 3.5% | 1.0% | 1.0% | 1.0% | 1.0% |
| Simple Volume Growth | 0 | 15 | 22 | 2 | 0 | 19 | 45 | 3 | 0 | 1 | 36 | 8 | 0 | 0 | 11 | 5 | |
| Applied Bckgrnd Growth | 0 | 15 | 22 | 2 | 0 | 19 | 45 | 3 | 0 | 1 | 36 | 8 | 0 | 0 | 11 | 5 | |
| Total Bckgrnd Pk-Hr Vols | 0 | 99 | 148 | 16 | 0 | 129 | 303 | 19 | 0 | 8 | 242 | 55 | 0 | 6 | 239 | 103 | |

Project Trips

| | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | |
|-------------------------|-----------|-------|------|------|-----------|------|------|------|------------|------|-------|------|------------|------|-------|-------|
| | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| New Ext Inbound Volume | 0.0% | 12.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 1.5% | 0.0% | 0.0% | 20.3% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 12 | 0 | 0 | 0 | 0 | 0 |
| New Ext Outbound Volume | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 1.5% | 20.3% | 12.0% |
| | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 13 | 8 |
| Pass-By Inbound Volume | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-By Outbound Volume | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Project Trips | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 12 | 0 | 0 | 1 | 13 | 8 |

| | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | |
|---------------------|-----------|-----|-----|----|-----------|-----|-----|----|------------|---|-----|----|------------|---|-----|-----|
| | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| Total Pk-Hr Volumes | 0 | 106 | 148 | 16 | 0 | 129 | 303 | 20 | 0 | 8 | 254 | 55 | 0 | 7 | 252 | 111 |

Lake Helen Osteen Road at Elkcarn Boulevard

PM Peak Hour

Existing TMCs

| | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | |
|----------------|-----------|-----|-----|----|-----------|----|-----|----|------------|----|-----|-----|------------|----|-----|-----|
| | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| Existing Count | 0 | 154 | 350 | 14 | 0 | 87 | 206 | 14 | 0 | 19 | 227 | 135 | 0 | 32 | 280 | 112 |
| Date of Count | 1/18/2024 | | | | SF | | | | 1.02 | | | | | | | |
| Adjusted Count | 0 | 157 | 357 | 14 | 0 | 89 | 210 | 14 | 0 | 19 | 232 | 138 | 0 | 33 | 286 | 114 |

| | West Leg | | | | East Leg | | | | South Leg | | | | North Leg | | | |
|--|----------|--|--|--|----------|--|--|--|-----------|--|--|--|-----------|--|--|--|
| Existing Approach & Departure Volumes | EB: 528 | | | | EB: 528 | | | | NB: 389 | | | | NB: 403 | | | |
| | WB: 343 | | | | WB: 313 | | | | SB: 389 | | | | SB: 433 | | | |
| Directional Factors Based on Existing Counts | EB: 0.61 | | | | EB: 0.63 | | | | NB: 0.50 | | | | NB: 0.48 | | | |
| | WB: 0.39 | | | | WB: 0.37 | | | | SB: 0.50 | | | | SB: 0.52 | | | |

Future Background Year 2029

| | | | | | | | | | | | | | | | | |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| Annual Growth Rate | 3.5% | 3.5% | 3.5% | 3.5% | 3.5% | 3.5% | 3.5% | 3.5% | 3.5% | 3.5% | 3.5% | 3.5% | 1.0% | 1.0% | 1.0% | 1.0% |
| Simple Volume Growth | 0 | 27 | 62 | 2 | 0 | 16 | 37 | 2 | 0 | 3 | 41 | 24 | 0 | 2 | 14 | 6 |
| Applied Bckgrnd Growth | 0 | 27 | 62 | 2 | 0 | 16 | 37 | 2 | 0 | 3 | 41 | 24 | 0 | 2 | 14 | 6 |
| Total Bckgrnd Pk-Hr Vols | 0 | 184 | 419 | 16 | 0 | 105 | 247 | 16 | 0 | 22 | 273 | 162 | 0 | 35 | 300 | 120 |

Project Trips

| | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | |
|---------------------|-----------|-------|------|------|-----------|------|------|------|------------|------|-------|------|------------|------|-------|-------|
| | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| New Ext Inbound | 0.0% | 12.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 1.5% | 0.0% | 0.0% | 20.3% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| Volume | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 13 | 0 | 0 | 0 | 0 | 0 |
| New Ext Outbound | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 1.5% | 20.3% | 12.0% |
| Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 14 | 8 |
| Pass-By Inbound | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-By Outbound | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Project Trips | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 13 | 0 | 0 | 1 | 14 | 8 |

| | Eastbound | | | | Westbound | | | | Northbound | | | | Southbound | | | |
|---------------------|-----------|-----|-----|----|-----------|-----|-----|----|------------|----|-----|-----|------------|----|-----|-----|
| | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| Total Pk-Hr Volumes | 0 | 191 | 419 | 16 | 0 | 105 | 247 | 17 | 0 | 22 | 286 | 162 | 0 | 36 | 314 | 128 |

Appendix G

Future Buildout (2029) Synchro Printouts



Timings

101: Catalina Blvd & Howland Blvd

03/01/2024



| Lane Group | SEL | SET | NWL | NWT | NEL | NET | SWL | SWT | SWR |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | | | |
| Traffic Volume (vph) | 140 | 549 | 31 | 1047 | 113 | 115 | 133 | 106 | 540 |
| Future Volume (vph) | 140 | 549 | 31 | 1047 | 113 | 115 | 133 | 106 | 540 |
| Turn Type | pm+pt | NA | pm+pt | NA | pm+pt | NA | Perm | NA | Perm |
| Protected Phases | 1 | 6 | 5 | 2 | 7 | 4 | | 8 | |
| Permitted Phases | 6 | | 2 | | 4 | | 8 | | 8 |
| Detector Phase | 1 | 6 | 5 | 2 | 7 | 4 | 8 | 8 | 8 |
| Switch Phase | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 11.0 | 5.0 | 11.0 | 5.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Minimum Split (s) | 13.5 | 19.5 | 13.5 | 19.5 | 12.0 | 14.0 | 14.0 | 14.0 | 14.0 |
| Total Split (s) | 24.0 | 65.0 | 18.0 | 59.0 | 24.0 | 67.0 | 43.0 | 43.0 | 43.0 |
| Total Split (%) | 16.0% | 43.3% | 12.0% | 39.3% | 16.0% | 44.7% | 28.7% | 28.7% | 28.7% |
| Yellow Time (s) | 5.0 | 5.0 | 5.0 | 5.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 8.5 | 8.5 | 8.5 | 8.5 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Lead/Lag | Lead | Lag | Lead | Lag | Lead | | Lag | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | | Yes | Yes | Yes |
| Recall Mode | None | Max | None | Max | None | None | None | None | None |
| Act Effect Green (s) | 70.8 | 62.3 | 57.6 | 50.7 | 54.8 | 54.8 | 34.0 | 34.0 | 34.0 |
| Actuated g/C Ratio | 0.50 | 0.44 | 0.41 | 0.36 | 0.39 | 0.39 | 0.24 | 0.24 | 0.24 |
| v/c Ratio | 0.74 | 0.41 | 0.09 | 0.96 | 0.25 | 0.23 | 0.48 | 0.25 | 0.96 |
| Control Delay | 55.1 | 30.2 | 20.7 | 62.0 | 30.2 | 27.8 | 53.7 | 46.4 | 54.3 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 55.1 | 30.2 | 20.7 | 62.0 | 30.2 | 27.8 | 53.7 | 46.4 | 54.3 |
| LOS | E | C | C | E | C | C | D | D | D |
| Approach Delay | | 35.0 | | 60.9 | | 28.8 | | 53.1 | |
| Approach LOS | | D | | E | | C | | D | |

Intersection Summary

Cycle Length: 150

Actuated Cycle Length: 142

Natural Cycle: 100

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.96

Intersection Signal Delay: 49.5

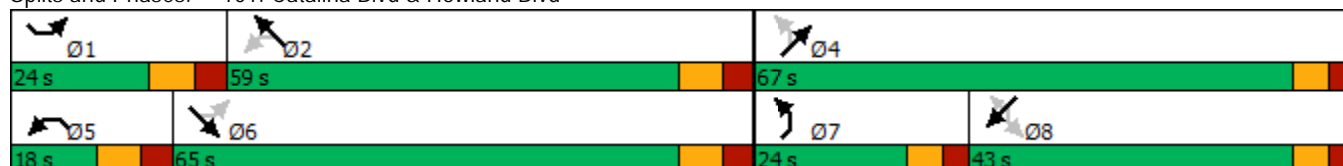
Intersection LOS: D

Intersection Capacity Utilization 90.0%

ICU Level of Service E

Analysis Period (min) 15






















Splits and Phases: 101: Catalina Blvd & Howland Blvd



HCM 6th Signalized Intersection Summary

101: Catalina Blvd & Howland Blvd

03/01/2024

| |  |  |  |  |  |  |  |  |  |  |  |  |
|------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | SEL | SET | SER | NWL | NWT | NWR | NEL | NET | NER | SWL | SWT | SWR |
| Lane Configurations |  |  | |  |  | |  |  | |  |  |  |
| Traffic Volume (veh/h) | 140 | 549 | 34 | 31 | 1047 | 82 | 113 | 115 | 37 | 133 | 106 | 540 |
| Future Volume (veh/h) | 140 | 549 | 34 | 31 | 1047 | 82 | 113 | 115 | 37 | 133 | 106 | 540 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | No | | | No | | | No | | | No | | |
| Adj Sat Flow, veh/h/ln | 1841 | 1826 | 1856 | 1870 | 1856 | 1856 | 1885 | 1885 | 1856 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 147 | 578 | 36 | 33 | 1102 | 86 | 119 | 121 | 39 | 140 | 112 | 517 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh, % | 4 | 5 | 3 | 2 | 3 | 3 | 1 | 1 | 3 | 2 | 2 | 2 |
| Cap, veh/h | 201 | 1384 | 86 | 337 | 1248 | 97 | 340 | 518 | 167 | 379 | 497 | 421 |
| Arrive On Green | 0.07 | 0.42 | 0.42 | 0.03 | 0.38 | 0.38 | 0.06 | 0.38 | 0.38 | 0.27 | 0.27 | 0.27 |
| Sat Flow, veh/h | 1753 | 3317 | 206 | 1781 | 3313 | 258 | 1795 | 1366 | 440 | 1226 | 1870 | 1585 |
| Grp Volume(v), veh/h | 147 | 302 | 312 | 33 | 586 | 602 | 119 | 0 | 160 | 140 | 112 | 517 |
| Grp Sat Flow(s),veh/h/ln | 1753 | 1735 | 1789 | 1781 | 1763 | 1809 | 1795 | 0 | 1806 | 1226 | 1870 | 1585 |
| Q Serve(g_s), s | 6.9 | 16.6 | 16.7 | 1.5 | 42.0 | 42.1 | 6.3 | 0.0 | 8.2 | 12.8 | 6.3 | 36.0 |
| Cycle Q Clear(g_c), s | 6.9 | 16.6 | 16.7 | 1.5 | 42.0 | 42.1 | 6.3 | 0.0 | 8.2 | 12.8 | 6.3 | 36.0 |
| Prop In Lane | 1.00 | | 0.12 | 1.00 | | 0.14 | 1.00 | | 0.24 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 201 | 724 | 746 | 337 | 664 | 681 | 340 | 0 | 685 | 379 | 497 | 421 |
| V/C Ratio(X) | 0.73 | 0.42 | 0.42 | 0.10 | 0.88 | 0.88 | 0.35 | 0.00 | 0.23 | 0.37 | 0.23 | 1.23 |
| Avail Cap(c_a), veh/h | 284 | 724 | 746 | 416 | 664 | 681 | 454 | 0 | 800 | 379 | 497 | 421 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 31.6 | 27.9 | 27.9 | 25.1 | 39.4 | 39.4 | 31.7 | 0.0 | 28.6 | 41.2 | 38.8 | 49.7 |
| Incr Delay (d2), s/veh | 5.7 | 1.8 | 1.7 | 0.1 | 15.7 | 15.5 | 0.6 | 0.0 | 0.2 | 0.6 | 0.2 | 121.6 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 3.1 | 7.1 | 7.3 | 0.6 | 20.4 | 20.9 | 2.8 | 0.0 | 3.6 | 4.0 | 3.0 | 28.4 |
| Unsig. Movement Delay, s/veh | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 37.3 | 29.6 | 29.6 | 25.2 | 55.1 | 54.9 | 32.3 | 0.0 | 28.8 | 41.8 | 39.1 | 171.4 |
| LnGrp LOS | D | C | C | C | E | D | C | A | C | D | D | F |
| Approach Vol, veh/h | 761 | | | 1221 | | | 279 | | | 769 | | |
| Approach Delay, s/veh | 31.1 | | | 54.2 | | | 30.3 | | | 128.5 | | |
| Approach LOS | C | | | D | | | C | | | F | | |
| Timer - Assigned Phs | 1 | 2 | | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 17.5 | 59.5 | | 58.4 | 12.1 | 65.0 | 15.4 | 43.0 | | | | |
| Change Period (Y+Rc), s | 8.5 | 8.5 | | 7.0 | 8.5 | 8.5 | 7.0 | 7.0 | | | | |
| Max Green Setting (Gmax), s | 15.5 | 50.5 | | 60.0 | 9.5 | 56.5 | 17.0 | 36.0 | | | | |
| Max Q Clear Time (g_c+I1), s | 8.9 | 44.1 | | 10.2 | 3.5 | 18.7 | 8.3 | 38.0 | | | | |
| Green Ext Time (p_c), s | 0.2 | 3.6 | | 1.0 | 0.0 | 3.6 | 0.2 | 0.0 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | 65.1 | | | | | | | | | | | |
| HCM 6th LOS | E | | | | | | | | | | | |

Timings

102: Lake Helen Osteen & Catalina Blvd

03/01/2024



| Lane Group | EBL | EBR | NBL | NBT | SBT |
|----------------------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | |
| Traffic Volume (vph) | 58 | 134 | 468 | 427 | 227 |
| Future Volume (vph) | 58 | 134 | 468 | 427 | 227 |
| Turn Type | Prot | Prot | pm+pt | NA | NA |
| Protected Phases | 8 | 8 | 1 | 6 | 2 |
| Permitted Phases | | | 6 | | |
| Detector Phase | 8 | 8 | 1 | 6 | 2 |
| Switch Phase | | | | | |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 15.0 | 15.0 |
| Minimum Split (s) | 11.5 | 11.5 | 11.5 | 21.5 | 21.5 |
| Total Split (s) | 26.5 | 26.5 | 26.5 | 63.0 | 36.5 |
| Total Split (%) | 29.6% | 29.6% | 29.6% | 70.4% | 40.8% |
| Yellow Time (s) | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.5 | 6.5 | 6.5 | 6.5 | 6.5 |
| Lead/Lag | | | Lead | | Lag |
| Lead-Lag Optimize? | | | Yes | | Yes |
| Recall Mode | None | None | None | Min | Min |
| Act Effect Green (s) | 8.0 | 8.0 | 46.8 | 46.8 | 22.1 |
| Actuated g/C Ratio | 0.12 | 0.12 | 0.69 | 0.69 | 0.32 |
| v/c Ratio | 0.31 | 0.47 | 0.79 | 0.37 | 0.78 |
| Control Delay | 34.1 | 11.5 | 20.6 | 5.5 | 28.8 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 34.1 | 11.5 | 20.6 | 5.5 | 28.8 |
| LOS | C | B | C | A | C |
| Approach Delay | 18.4 | | | 13.4 | 28.8 |
| Approach LOS | B | | | B | C |

Intersection Summary

Cycle Length: 89.5

Actuated Cycle Length: 68.1

Natural Cycle: 60

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.79

Intersection Signal Delay: 18.3

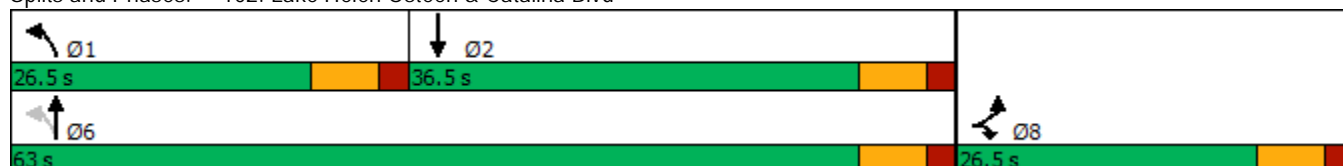
Intersection LOS: B

Intersection Capacity Utilization 70.0%

ICU Level of Service C

Analysis Period (min) 15

Splits and Phases: 102: Lake Helen Osteen & Catalina Blvd



HCM 6th Signalized Intersection Summary

102: Lake Helen Osteen & Catalina Blvd

03/01/2024






| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
|------------------------------|------|------|------|------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 58 | 134 | 468 | 427 | 227 | 192 |
| Future Volume (veh/h) | 58 | 134 | 468 | 427 | 227 | 192 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | No | | | No | No | |
| Adj Sat Flow, veh/h/ln | 1870 | 1856 | 1870 | 1856 | 1826 | 1870 |
| Adj Flow Rate, veh/h | 64 | 147 | 514 | 469 | 249 | 211 |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Percent Heavy Veh, % | 2 | 3 | 2 | 3 | 5 | 2 |
| Cap, veh/h | 227 | 201 | 582 | 1215 | 296 | 251 |
| Arrive On Green | 0.13 | 0.13 | 0.22 | 0.65 | 0.32 | 0.32 |
| Sat Flow, veh/h | 1781 | 1572 | 1781 | 1856 | 913 | 774 |
| Grp Volume(v), veh/h | 64 | 147 | 514 | 469 | 0 | 460 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 1572 | 1781 | 1856 | 0 | 1687 |
| Q Serve(g_s), s | 1.9 | 5.4 | 10.2 | 7.0 | 0.0 | 15.2 |
| Cycle Q Clear(g_c), s | 1.9 | 5.4 | 10.2 | 7.0 | 0.0 | 15.2 |
| Prop In Lane | 1.00 | 1.00 | 1.00 | | | 0.46 |
| Lane Grp Cap(c), veh/h | 227 | 201 | 582 | 1215 | 0 | 547 |
| V/C Ratio(X) | 0.28 | 0.73 | 0.88 | 0.39 | 0.00 | 0.84 |
| Avail Cap(c_a), veh/h | 596 | 526 | 782 | 1754 | 0 | 847 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 23.6 | 25.1 | 11.0 | 4.8 | 0.0 | 18.8 |
| Incr Delay (d2), s/veh | 0.7 | 5.1 | 9.2 | 0.2 | 0.0 | 4.7 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 0.8 | 2.1 | 3.9 | 1.4 | 0.0 | 5.6 |
| Unsig. Movement Delay, s/veh | | | | | | |
| LnGrp Delay(d),s/veh | 24.3 | 30.2 | 20.2 | 5.0 | 0.0 | 23.4 |
| LnGrp LOS | C | C | C | A | A | C |
| Approach Vol, veh/h | 211 | | | 983 | 460 | |
| Approach Delay, s/veh | 28.4 | | | 12.9 | 23.4 | |
| Approach LOS | C | | | B | C | |
| Timer - Assigned Phs | 1 | 2 | | | 6 | 8 |
| Phs Duration (G+Y+Rc), s | 19.8 | 25.9 | | | 45.6 | 14.1 |
| Change Period (Y+Rc), s | 6.5 | 6.5 | | | 6.5 | 6.5 |
| Max Green Setting (Gmax), s | 20.0 | 30.0 | | | 56.5 | 20.0 |
| Max Q Clear Time (g_c+I1), s | 12.2 | 17.2 | | | 9.0 | 7.4 |
| Green Ext Time (p_c), s | 1.1 | 2.2 | | | 2.9 | 0.5 |

Intersection Summary

| | |
|--------------------|------|
| HCM 6th Ctrl Delay | 17.8 |
| HCM 6th LOS | B |

HCM 6th TWSC
103: Lake Helen Osteen & Driveway #1

03/01/2024

| Intersection | | | | | | |
|--------------------------|---|--------|---|------|------|---|
| Int Delay, s/veh | 0.3 | | | | | |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations |  | |  | | |  |
| Traffic Vol, veh/h | 6 | 13 | 543 | 0 | 0 | 307 |
| Future Vol, veh/h | 6 | 13 | 543 | 0 | 0 | 307 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, # | 0 | - | 0 | - | - | 0 |
| Grade, % | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 85 | 85 | 85 | 85 | 85 | 85 |
| Heavy Vehicles, % | 2 | 2 | 3 | 2 | 2 | 4 |
| Mvmt Flow | 7 | 15 | 639 | 0 | 0 | 361 |
| Major/Minor | Minor1 | Major1 | Major2 | | | |
| Conflicting Flow All | 1000 | 639 | 0 | - | - | - |
| Stage 1 | 639 | - | - | - | - | - |
| Stage 2 | 361 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | - | - | - | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | - | - | - | - |
| Pot Cap-1 Maneuver | 270 | 476 | - | 0 | 0 | - |
| Stage 1 | 526 | - | - | 0 | 0 | - |
| Stage 2 | 705 | - | - | 0 | 0 | - |
| Platoon blocked, % | | | - | | | - |
| Mov Cap-1 Maneuver | 270 | 476 | - | - | - | - |
| Mov Cap-2 Maneuver | 270 | - | - | - | - | - |
| Stage 1 | 526 | - | - | - | - | - |
| Stage 2 | 705 | - | - | - | - | - |
| Approach | WB | NB | SB | | | |
| HCM Control Delay, s | 15 | 0 | 0 | | | |
| HCM LOS | C | | | | | |
| Minor Lane/Major Mvmt | NBTWBLn1 | | SBT | | | |
| Capacity (veh/h) | - | | 384 | | | |
| HCM Lane V/C Ratio | - | | 0.058 | | | |
| HCM Control Delay (s) | - | | 15 | | | |
| HCM Lane LOS | - | | C | | | |
| HCM 95th %tile Q(veh) | - | | 0.2 | | | |

HCM 6th TWSC
104: Lake Helen Osteen & Driveway #2

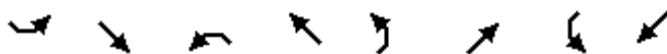
03/01/2024

| Intersection | | | | | | | | | | | | |
|--------------------------|--------|-------|--------|------------|--------|-------|--------|------|------|-------|------|------|
| Int Delay, s/veh | 2.3 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↕ | | | ↕ | | | ↕ | | | ↕ | |
| Traffic Vol, veh/h | 28 | 0 | 18 | 14 | 0 | 18 | 5 | 498 | 32 | 51 | 244 | 9 |
| Future Vol, veh/h | 28 | 0 | 18 | 14 | 0 | 18 | 5 | 498 | 32 | 51 | 244 | 9 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 3 | 2 | 2 | 4 | 2 |
| Mvmt Flow | 33 | 0 | 21 | 16 | 0 | 21 | 6 | 586 | 38 | 60 | 287 | 11 |
| Major/Minor | Minor2 | | Minor1 | | Major1 | | Major2 | | | | | |
| Conflicting Flow All | 1041 | 1049 | 293 | 1040 | 1035 | 605 | 298 | 0 | 0 | 624 | 0 | 0 |
| Stage 1 | 413 | 413 | - | 617 | 617 | - | - | - | - | - | - | - |
| Stage 2 | 628 | 636 | - | 423 | 418 | - | - | - | - | - | - | - |
| Critical Hdwy | 7.12 | 6.52 | 6.22 | 7.12 | 6.52 | 6.22 | 4.12 | - | - | 4.12 | - | - |
| Critical Hdwy Stg 1 | 6.12 | 5.52 | - | 6.12 | 5.52 | - | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.12 | 5.52 | - | 6.12 | 5.52 | - | - | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 4.018 | 3.318 | 3.518 | 4.018 | 3.318 | 2.218 | - | - | 2.218 | - | - |
| Pot Cap-1 Maneuver | 208 | 227 | 746 | 208 | 232 | 498 | 1263 | - | - | 957 | - | - |
| Stage 1 | 616 | 594 | - | 477 | 481 | - | - | - | - | - | - | - |
| Stage 2 | 471 | 472 | - | 609 | 591 | - | - | - | - | - | - | - |
| Platoon blocked, % | | | | | | | | - | - | | - | - |
| Mov Cap-1 Maneuver | 187 | 209 | 746 | 189 | 213 | 498 | 1263 | - | - | 957 | - | - |
| Mov Cap-2 Maneuver | 187 | 209 | - | 189 | 213 | - | - | - | - | - | - | - |
| Stage 1 | 612 | 549 | - | 474 | 478 | - | - | - | - | - | - | - |
| Stage 2 | 448 | 469 | - | 547 | 547 | - | - | - | - | - | - | - |
| Approach | EB | | WB | | NB | | SB | | | | | |
| HCM Control Delay, s | 22 | | 19.3 | | 0.1 | | 1.5 | | | | | |
| HCM LOS | C | | C | | | | | | | | | |
| Minor Lane/Major Mvmt | NBL | NBT | NBR | EBLn1WBLn1 | SBL | SBT | SBR | | | | | |
| Capacity (veh/h) | 1263 | - | - | 265 | 290 | 957 | - | - | | | | |
| HCM Lane V/C Ratio | 0.005 | - | - | 0.204 | 0.13 | 0.063 | - | - | | | | |
| HCM Control Delay (s) | 7.9 | 0 | - | 22 | 19.3 | 9 | 0 | - | | | | |
| HCM Lane LOS | A | A | - | C | C | A | A | - | | | | |
| HCM 95th %tile Q(veh) | 0 | - | - | 0.7 | 0.4 | 0.2 | - | - | | | | |

Timings

105: Elkcarn Blvd & Lake Helen Osteen

03/01/2024



| Lane Group | SEL | SET | NWL | NWT | NEL | NET | SWL | SWT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | | |
| Traffic Volume (vph) | 7 | 252 | 8 | 254 | 106 | 148 | 129 | 303 |
| Future Volume (vph) | 7 | 252 | 8 | 254 | 106 | 148 | 129 | 303 |
| Turn Type | pm+pt | NA | pm+pt | NA | pm+pt | NA | pm+pt | NA |
| Protected Phases | 5 | 2 | 1 | 6 | 3 | 8 | 7 | 4 |
| Permitted Phases | 2 | | 6 | | 8 | | 4 | |
| Detector Phase | 5 | 2 | 1 | 6 | 3 | 8 | 7 | 4 |
| Switch Phase | | | | | | | | |
| Minimum Initial (s) | 5.0 | 16.0 | 5.0 | 16.0 | 5.0 | 6.0 | 5.0 | 6.0 |
| Minimum Split (s) | 14.0 | 25.0 | 14.0 | 25.0 | 13.5 | 13.0 | 13.5 | 13.0 |
| Total Split (s) | 29.0 | 49.0 | 29.0 | 49.0 | 28.5 | 32.0 | 28.5 | 32.0 |
| Total Split (%) | 20.9% | 35.4% | 20.9% | 35.4% | 20.6% | 23.1% | 20.6% | 23.1% |
| Yellow Time (s) | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 4.0 | 5.5 | 4.0 |
| All-Red Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 9.0 | 9.0 | 9.0 | 9.0 | 8.5 | 7.0 | 8.5 | 7.0 |
| Lead/Lag | Lead | Lag | Lead | Lag | Lead | Lag | Lead | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | Min | None | Min | None | None | None | None |
| Act Effect Green (s) | 24.7 | 23.8 | 24.8 | 23.8 | 31.5 | 24.3 | 34.5 | 25.8 |
| Actuated g/C Ratio | 0.29 | 0.28 | 0.29 | 0.28 | 0.37 | 0.28 | 0.40 | 0.30 |
| v/c Ratio | 0.02 | 0.77 | 0.03 | 0.65 | 0.30 | 0.34 | 0.26 | 0.61 |
| Control Delay | 19.1 | 39.2 | 19.2 | 33.5 | 18.4 | 30.7 | 17.2 | 34.9 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 19.1 | 39.2 | 19.2 | 33.5 | 18.4 | 30.7 | 17.2 | 34.9 |
| LOS | B | D | B | C | B | C | B | C |
| Approach Delay | | 38.8 | | 33.2 | | 25.8 | | 29.8 |
| Approach LOS | | D | | C | | C | | C |

Intersection Summary

Cycle Length: 138.5

Actuated Cycle Length: 85.9

Natural Cycle: 80

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.77

Intersection Signal Delay: 32.2

Intersection LOS: C

Intersection Capacity Utilization 63.5%

ICU Level of Service B

Analysis Period (min) 15





















Splits and Phases: 105: Elkcarn Blvd & Lake Helen Osteen

| | | | |
|------|------|--------|------|
| Ø1 | Ø2 | Ø3 | Ø4 |
| 29 s | 49 s | 28.5 s | 32 s |
| Ø5 | Ø6 | Ø7 | Ø8 |
| 29 s | 49 s | 28.5 s | 32 s |

HCM 6th Signalized Intersection Summary

105: Elkcarn Blvd & Lake Helen Osteen



















03/01/2024

| |  |  |  |  |  |  |  |  |  |  |  |  |
|------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | SEL | SET | SER | NWL | NWT | NWR | NEL | NET | NER | SWL | SWT | SWR |
| Lane Configurations |  |  | |  |  | |  |  | |  |  | |
| Traffic Volume (veh/h) | 7 | 252 | 111 | 8 | 254 | 55 | 106 | 148 | 16 | 129 | 303 | 20 |
| Future Volume (veh/h) | 7 | 252 | 111 | 8 | 254 | 55 | 106 | 148 | 16 | 129 | 303 | 20 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1870 | 1841 | 1841 | 1870 | 1856 | 1841 | 1870 | 1870 | 1604 | 1856 | 1870 | 1811 |
| Adj Flow Rate, veh/h | 7 | 265 | 117 | 8 | 267 | 58 | 112 | 156 | 17 | 136 | 319 | 21 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh, % | 2 | 4 | 4 | 2 | 3 | 4 | 2 | 2 | 20 | 3 | 2 | 6 |
| Cap, veh/h | 217 | 318 | 141 | 169 | 390 | 85 | 264 | 341 | 37 | 390 | 380 | 25 |
| Arrive On Green | 0.01 | 0.26 | 0.26 | 0.01 | 0.26 | 0.26 | 0.07 | 0.21 | 0.21 | 0.08 | 0.22 | 0.22 |
| Sat Flow, veh/h | 1781 | 1210 | 534 | 1781 | 1477 | 321 | 1781 | 1657 | 181 | 1767 | 1736 | 114 |
| Grp Volume(v), veh/h | 7 | 0 | 382 | 8 | 0 | 325 | 112 | 0 | 173 | 136 | 0 | 340 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 0 | 1745 | 1781 | 0 | 1798 | 1781 | 0 | 1838 | 1767 | 0 | 1850 |
| Q Serve(g_s), s | 0.2 | 0.0 | 15.8 | 0.3 | 0.0 | 12.4 | 3.7 | 0.0 | 6.3 | 4.5 | 0.0 | 13.5 |
| Cycle Q Clear(g_c), s | 0.2 | 0.0 | 15.8 | 0.3 | 0.0 | 12.4 | 3.7 | 0.0 | 6.3 | 4.5 | 0.0 | 13.5 |
| Prop In Lane | 1.00 | | 0.31 | 1.00 | | 0.18 | 1.00 | | 0.10 | 1.00 | | 0.06 |
| Lane Grp Cap(c), veh/h | 217 | 0 | 459 | 169 | 0 | 475 | 264 | 0 | 378 | 390 | 0 | 405 |
| V/C Ratio(X) | 0.03 | 0.00 | 0.83 | 0.05 | 0.00 | 0.68 | 0.42 | 0.00 | 0.46 | 0.35 | 0.00 | 0.84 |
| Avail Cap(c_a), veh/h | 667 | 0 | 911 | 616 | 0 | 939 | 604 | 0 | 600 | 703 | 0 | 604 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 21.4 | 0.0 | 26.6 | 22.0 | 0.0 | 25.3 | 22.6 | 0.0 | 26.7 | 21.2 | 0.0 | 28.6 |
| Incr Delay (d2), s/veh | 0.1 | 0.0 | 4.0 | 0.1 | 0.0 | 1.8 | 1.1 | 0.0 | 0.9 | 0.5 | 0.0 | 6.7 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 0.1 | 0.0 | 6.7 | 0.1 | 0.0 | 5.2 | 1.5 | 0.0 | 2.7 | 1.8 | 0.0 | 6.4 |
| Unsig. Movement Delay, s/veh | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 21.4 | 0.0 | 30.6 | 22.1 | 0.0 | 27.1 | 23.6 | 0.0 | 27.6 | 21.8 | 0.0 | 35.3 |
| LnGrp LOS | C | A | C | C | A | C | C | A | C | C | A | D |
| Approach Vol, veh/h | | 389 | | | 333 | | | 285 | | | 476 | |
| Approach Delay, s/veh | | 30.5 | | | 26.9 | | | 26.0 | | | 31.4 | |
| Approach LOS | | C | | | C | | | C | | | C | |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 9.8 | 29.1 | 13.9 | 23.8 | 9.7 | 29.2 | 14.9 | 22.7 | | | | |
| Change Period (Y+Rc), s | 9.0 | 9.0 | 8.5 | 7.0 | 9.0 | 9.0 | 8.5 | 7.0 | | | | |
| Max Green Setting (Gmax), s | 20.0 | 40.0 | 20.0 | 25.0 | 20.0 | 40.0 | 20.0 | 25.0 | | | | |
| Max Q Clear Time (g_c+I1), s | 2.3 | 17.8 | 5.7 | 15.5 | 2.2 | 14.4 | 6.5 | 8.3 | | | | |
| Green Ext Time (p_c), s | 0.0 | 2.3 | 0.2 | 1.3 | 0.0 | 1.9 | 0.3 | 0.8 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 29.1 | | | | | | | | | |
| HCM 6th LOS | | | C | | | | | | | | | |

Timings

101: Catalina Blvd & Howland Blvd

03/01/2024

| |  |  |  |  |  |  |  |  |  |
|----------------------|---|---|---|---|---|---|---|---|---|
| Lane Group | SEL | SET | NWL | NWT | NEL | NET | SWL | SWT | SWR |
| Lane Configurations |  |  |  |  |  |  |  |  |  |
| Traffic Volume (vph) | 445 | 1167 | 48 | 654 | 48 | 93 | 133 | 93 | 274 |
| Future Volume (vph) | 445 | 1167 | 48 | 654 | 48 | 93 | 133 | 93 | 274 |
| Turn Type | pm+pt | NA | pm+pt | NA | pm+pt | NA | Perm | NA | Perm |
| Protected Phases | 1 | 6 | 5 | 2 | 7 | 4 | | 8 | |
| Permitted Phases | 6 | | 2 | | 4 | | 8 | | 8 |
| Detector Phase | 1 | 6 | 5 | 2 | 7 | 4 | 8 | 8 | 8 |
| Switch Phase | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 11.0 | 5.0 | 11.0 | 5.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Minimum Split (s) | 13.5 | 19.5 | 13.5 | 19.5 | 12.0 | 14.0 | 14.0 | 14.0 | 14.0 |
| Total Split (s) | 30.0 | 65.0 | 20.0 | 55.0 | 20.0 | 60.0 | 45.0 | 45.0 | 45.0 |
| Total Split (%) | 20.0% | 43.3% | 13.3% | 36.7% | 13.3% | 40.0% | 30.0% | 30.0% | 30.0% |
| Yellow Time (s) | 5.0 | 5.0 | 5.0 | 5.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 8.5 | 8.5 | 8.5 | 8.5 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Lead/Lag | Lead | Lag | Lead | Lag | Lead | | Lag | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | | Yes | Yes | Yes |
| Recall Mode | None | Max | None | Max | None | None | None | None | None |
| Act Effect Green (s) | 77.4 | 65.1 | 54.1 | 47.0 | 32.4 | 32.4 | 19.6 | 19.6 | 19.6 |
| Actuated g/C Ratio | 0.62 | 0.52 | 0.43 | 0.37 | 0.26 | 0.26 | 0.16 | 0.16 | 0.16 |
| v/c Ratio | 0.96 | 0.71 | 0.25 | 0.58 | 0.17 | 0.25 | 0.71 | 0.34 | 0.59 |
| Control Delay | 53.7 | 30.0 | 18.3 | 35.3 | 34.2 | 33.7 | 70.5 | 50.9 | 10.4 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 53.7 | 30.0 | 18.3 | 35.3 | 34.2 | 33.7 | 70.5 | 50.9 | 10.4 |
| LOS | D | C | B | D | C | C | E | D | B |
| Approach Delay | | 36.3 | | 34.2 | | 33.8 | | 34.0 | |
| Approach LOS | | D | | C | | C | | C | |

Intersection Summary

Cycle Length: 150

Actuated Cycle Length: 125.5

Natural Cycle: 90

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.96

Intersection Signal Delay: 35.3

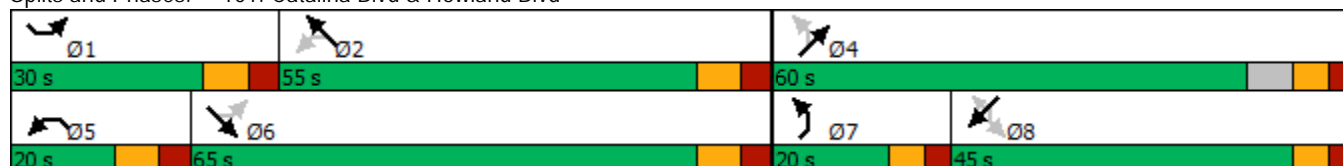
Intersection LOS: D

Intersection Capacity Utilization 79.0%

ICU Level of Service D

Analysis Period (min) 15






















Splits and Phases: 101: Catalina Blvd & Howland Blvd



HCM 6th Signalized Intersection Summary

101: Catalina Blvd & Howland Blvd

03/01/2024

| |  |  |  |  |  |  |  |  |  |  |  |  |
|------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | SEL | SET | SER | NWL | NWT | NWR | NEL | NET | NER | SWL | SWT | SWR |
| Lane Configurations |  |  | |  |  | |  |  | |  |  |  |
| Traffic Volume (veh/h) | 445 | 1167 | 64 | 48 | 654 | 71 | 48 | 93 | 20 | 133 | 93 | 274 |
| Future Volume (veh/h) | 445 | 1167 | 64 | 48 | 654 | 71 | 48 | 93 | 20 | 133 | 93 | 274 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | No | | | | No | | | | No | | | |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1826 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1856 |
| Adj Flow Rate, veh/h | 468 | 1228 | 67 | 51 | 688 | 75 | 51 | 98 | 21 | 140 | 98 | 237 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh, % | 2 | 2 | 5 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 3 |
| Cap, veh/h | 505 | 1748 | 95 | 217 | 1201 | 131 | 253 | 396 | 85 | 281 | 329 | 277 |
| Arrive On Green | 0.17 | 0.51 | 0.51 | 0.03 | 0.37 | 0.37 | 0.03 | 0.27 | 0.27 | 0.18 | 0.18 | 0.18 |
| Sat Flow, veh/h | 1781 | 3427 | 187 | 1781 | 3232 | 352 | 1781 | 1493 | 320 | 1273 | 1870 | 1572 |
| Grp Volume(v), veh/h | 468 | 636 | 659 | 51 | 378 | 385 | 51 | 0 | 119 | 140 | 98 | 237 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 1777 | 1837 | 1781 | 1777 | 1807 | 1781 | 0 | 1813 | 1273 | 1870 | 1572 |
| Q Serve(g_s), s | 19.7 | 34.2 | 34.3 | 2.2 | 21.3 | 21.3 | 2.9 | 0.0 | 6.5 | 12.7 | 5.7 | 18.3 |
| Cycle Q Clear(g_c), s | 19.7 | 34.2 | 34.3 | 2.2 | 21.3 | 21.3 | 2.9 | 0.0 | 6.5 | 12.7 | 5.7 | 18.3 |
| Prop In Lane | 1.00 | | 0.10 | 1.00 | | 0.19 | 1.00 | | 0.18 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 505 | 906 | 937 | 217 | 660 | 671 | 253 | 0 | 480 | 281 | 329 | 277 |
| V/C Ratio(X) | 0.93 | 0.70 | 0.70 | 0.23 | 0.57 | 0.57 | 0.20 | 0.00 | 0.25 | 0.50 | 0.30 | 0.86 |
| Avail Cap(c_a), veh/h | 505 | 906 | 937 | 322 | 660 | 671 | 379 | 0 | 768 | 444 | 568 | 477 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 22.1 | 23.4 | 23.4 | 24.1 | 31.4 | 31.4 | 38.9 | 0.0 | 36.2 | 47.8 | 44.9 | 50.0 |
| Incr Delay (d2), s/veh | 23.3 | 4.5 | 4.4 | 0.5 | 3.6 | 3.5 | 0.4 | 0.0 | 0.3 | 1.4 | 0.5 | 7.5 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 10.7 | 14.5 | 15.0 | 0.9 | 9.4 | 9.6 | 1.3 | 0.0 | 2.9 | 4.2 | 2.7 | 7.8 |
| Unsig. Movement Delay, s/veh | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 45.4 | 27.9 | 27.8 | 24.7 | 35.0 | 35.0 | 39.3 | 0.0 | 36.5 | 49.1 | 45.4 | 57.6 |
| LnGrp LOS | D | C | C | C | C | C | D | A | D | D | D | E |
| Approach Vol, veh/h | 1763 | | | | 814 | | | | 170 | | | |
| Approach Delay, s/veh | 32.5 | | | | 34.3 | | | | 37.3 | | | |
| Approach LOS | C | | | | C | | | | D | | | |
| Timer - Assigned Phs | 1 | 2 | | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 30.0 | 55.0 | | 40.2 | 12.7 | 72.3 | 11.2 | 29.0 | | | | |
| Change Period (Y+Rc), s | 8.5 | 8.5 | | 7.0 | 8.5 | 8.5 | 7.0 | 7.0 | | | | |
| Max Green Setting (Gmax), s | 21.5 | 46.5 | | 53.0 | 11.5 | 56.5 | 13.0 | 38.0 | | | | |
| Max Q Clear Time (g_c+I1), s | 21.7 | 23.3 | | 8.5 | 4.2 | 36.3 | 4.9 | 20.3 | | | | |
| Green Ext Time (p_c), s | 0.0 | 4.4 | | 0.7 | 0.0 | 8.2 | 0.0 | 1.7 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | 36.2 | | | | | | | | | | | |
| HCM 6th LOS | D | | | | | | | | | | | |

Timings

102: Lake Helen Osteen & Catalina Blvd

03/01/2024



| Lane Group | EBL | EBR | NBL | NBT | SBT |
|----------------------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | |
| Traffic Volume (vph) | 181 | 380 | 231 | 193 | 394 |
| Future Volume (vph) | 181 | 380 | 231 | 193 | 394 |
| Turn Type | Prot | Prot | pm+pt | NA | NA |
| Protected Phases | 8 | 8 | 1 | 6 | 2 |
| Permitted Phases | | | 6 | | |
| Detector Phase | 8 | 8 | 1 | 6 | 2 |
| Switch Phase | | | | | |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 15.0 | 15.0 |
| Minimum Split (s) | 11.5 | 11.5 | 11.5 | 21.5 | 21.5 |
| Total Split (s) | 26.5 | 26.5 | 26.5 | 63.0 | 36.5 |
| Total Split (%) | 29.6% | 29.6% | 29.6% | 70.4% | 40.8% |
| Yellow Time (s) | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.5 | 6.5 | 6.5 | 6.5 | 6.5 |
| Lead/Lag | | | Lead | | Lag |
| Lead-Lag Optimize? | | | Yes | | Yes |
| Recall Mode | None | None | None | Min | Min |
| Act Effect Green (s) | 13.3 | 13.3 | 42.9 | 42.9 | 25.2 |
| Actuated g/C Ratio | 0.19 | 0.19 | 0.62 | 0.62 | 0.36 |
| v/c Ratio | 0.58 | 0.65 | 0.57 | 0.18 | 0.81 |
| Control Delay | 34.7 | 8.5 | 12.2 | 6.6 | 32.5 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 34.7 | 8.5 | 12.2 | 6.6 | 32.5 |
| LOS | C | A | B | A | C |
| Approach Delay | 17.0 | | | 9.6 | 32.5 |
| Approach LOS | B | | | A | C |

Intersection Summary

Cycle Length: 89.5

Actuated Cycle Length: 69.7

Natural Cycle: 60

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.81

Intersection Signal Delay: 20.1

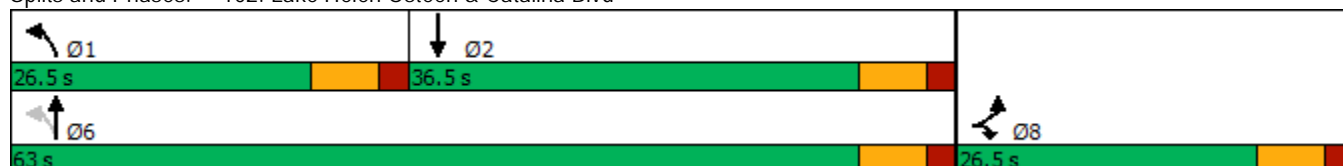
Intersection LOS: C

Intersection Capacity Utilization 65.9%

ICU Level of Service C

Analysis Period (min) 15

Splits and Phases: 102: Lake Helen Osteen & Catalina Blvd



HCM 6th Signalized Intersection Summary

102: Lake Helen Osteen & Catalina Blvd

03/01/2024






| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
|------------------------------|------|------|------|------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 181 | 380 | 231 | 193 | 394 | 100 |
| Future Volume (veh/h) | 181 | 380 | 231 | 193 | 394 | 100 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | No | | | No | No | |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1826 | 1870 | 1856 | 1841 |
| Adj Flow Rate, veh/h | 195 | 409 | 248 | 208 | 424 | 108 |
| Peak Hour Factor | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Percent Heavy Veh, % | 2 | 2 | 5 | 2 | 3 | 4 |
| Cap, veh/h | 492 | 437 | 354 | 1019 | 478 | 122 |
| Arrive On Green | 0.28 | 0.28 | 0.12 | 0.54 | 0.33 | 0.33 |
| Sat Flow, veh/h | 1781 | 1585 | 1739 | 1870 | 1427 | 363 |
| Grp Volume(v), veh/h | 195 | 409 | 248 | 208 | 0 | 532 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 1585 | 1739 | 1870 | 0 | 1790 |
| Q Serve(g_s), s | 6.5 | 18.3 | 6.2 | 4.1 | 0.0 | 20.4 |
| Cycle Q Clear(g_c), s | 6.5 | 18.3 | 6.2 | 4.1 | 0.0 | 20.4 |
| Prop In Lane | 1.00 | 1.00 | 1.00 | | | 0.20 |
| Lane Grp Cap(c), veh/h | 492 | 437 | 354 | 1019 | 0 | 600 |
| V/C Ratio(X) | 0.40 | 0.94 | 0.70 | 0.20 | 0.00 | 0.89 |
| Avail Cap(c_a), veh/h | 492 | 437 | 625 | 1458 | 0 | 741 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 21.3 | 25.6 | 15.7 | 8.5 | 0.0 | 22.8 |
| Incr Delay (d2), s/veh | 0.5 | 27.5 | 2.5 | 0.1 | 0.0 | 10.8 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 2.6 | 9.7 | 2.2 | 1.3 | 0.0 | 9.3 |
| Unsig. Movement Delay, s/veh | | | | | | |
| LnGrp Delay(d),s/veh | 21.9 | 53.1 | 18.2 | 8.6 | 0.0 | 33.7 |
| LnGrp LOS | C | D | B | A | A | C |
| Approach Vol, veh/h | 604 | | | 456 | 532 | |
| Approach Delay, s/veh | 43.0 | | | 13.8 | 33.7 | |
| Approach LOS | D | | | B | C | |
| Timer - Assigned Phs | 1 | 2 | | | 6 | 8 |
| Phs Duration (G+Y+Rc), s | 15.2 | 30.8 | | | 46.0 | 26.5 |
| Change Period (Y+Rc), s | 6.5 | 6.5 | | | 6.5 | 6.5 |
| Max Green Setting (Gmax), s | 20.0 | 30.0 | | | 56.5 | 20.0 |
| Max Q Clear Time (g_c+I1), s | 8.2 | 22.4 | | | 6.1 | 20.3 |
| Green Ext Time (p_c), s | 0.5 | 1.9 | | | 1.1 | 0.0 |

Intersection Summary

| | |
|--------------------|------|
| HCM 6th Ctrl Delay | 31.5 |
| HCM 6th LOS | C |





HCM 6th TWSC
103: Lake Helen Osteen & Driveway #1

03/01/2024

| Intersection | | | | | | |
|--------------------------|---|--------|---|------|------|---|
| Int Delay, s/veh | 0.3 | | | | | |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations |  | |  | | |  |
| Traffic Vol, veh/h | 8 | 13 | 318 | 0 | 0 | 518 |
| Future Vol, veh/h | 8 | 13 | 318 | 0 | 0 | 518 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, # | 0 | - | 0 | - | - | 0 |
| Grade, % | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 86 | 86 | 86 | 86 | 86 | 86 |
| Heavy Vehicles, % | 2 | 17 | 2 | 2 | 2 | 3 |
| Mvmt Flow | 9 | 15 | 370 | 0 | 0 | 602 |
| Major/Minor | Minor1 | Major1 | Major2 | | | |
| Conflicting Flow All | 972 | 370 | 0 | - | - | - |
| Stage 1 | 370 | - | - | - | - | - |
| Stage 2 | 602 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.37 | - | - | - | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.453 | - | - | - | - |
| Pot Cap-1 Maneuver | 280 | 644 | - | 0 | 0 | - |
| Stage 1 | 699 | - | - | 0 | 0 | - |
| Stage 2 | 547 | - | - | 0 | 0 | - |
| Platoon blocked, % | | | - | | | - |
| Mov Cap-1 Maneuver | 280 | 644 | - | - | - | - |
| Mov Cap-2 Maneuver | 280 | - | - | - | - | - |
| Stage 1 | 699 | - | - | - | - | - |
| Stage 2 | 547 | - | - | - | - | - |
| Approach | WB | NB | SB | | | |
| HCM Control Delay, s | 13.9 | 0 | 0 | | | |
| HCM LOS | B | | | | | |
| Minor Lane/Major Mvmt | NBTWBLn1 | | SBT | | | |
| Capacity (veh/h) | - | | 431 | | | |
| HCM Lane V/C Ratio | - | | 0.057 | | | |
| HCM Control Delay (s) | - | | 13.9 | | | |
| HCM Lane LOS | - | | B | | | |
| HCM 95th %tile Q(veh) | - | | 0.2 | | | |

HCM 6th TWSC
104: Lake Helen Osteen & Driveway #2

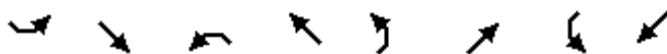
03/01/2024

| Intersection | | | | | | | | | | | | |
|--------------------------|--------|---|--------|------------|---|--------|-------|---|--------|-------|---|------|
| Int Delay, s/veh | 2.3 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | |  | | |  | | |  | | |  | |
| Traffic Vol, veh/h | 17 | 0 | 10 | 29 | 0 | 33 | 17 | 269 | 22 | 34 | 464 | 28 |
| Future Vol, veh/h | 17 | 0 | 10 | 29 | 0 | 33 | 17 | 269 | 22 | 34 | 464 | 28 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 87 | 87 | 87 | 87 | 87 | 87 | 87 | 87 | 87 | 87 | 87 | 87 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 3 | 2 |
| Mvmt Flow | 20 | 0 | 11 | 33 | 0 | 38 | 20 | 309 | 25 | 39 | 533 | 32 |
| | | | | | | | | | | | | |
| Major/Minor | Minor2 | | Minor1 | | | Major1 | | | Major2 | | | |
| Conflicting Flow All | 1008 | 1001 | 549 | 995 | 1005 | 322 | 565 | 0 | 0 | 334 | 0 | 0 |
| Stage 1 | 627 | 627 | - | 362 | 362 | - | - | - | - | - | - | - |
| Stage 2 | 381 | 374 | - | 633 | 643 | - | - | - | - | - | - | - |
| Critical Hdwy | 7.12 | 6.52 | 6.22 | 7.12 | 6.52 | 6.22 | 4.12 | - | - | 4.12 | - | - |
| Critical Hdwy Stg 1 | 6.12 | 5.52 | - | 6.12 | 5.52 | - | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.12 | 5.52 | - | 6.12 | 5.52 | - | - | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 4.018 | 3.318 | 3.518 | 4.018 | 3.318 | 2.218 | - | - | 2.218 | - | - |
| Pot Cap-1 Maneuver | 219 | 243 | 535 | 224 | 241 | 719 | 1007 | - | - | 1225 | - | - |
| Stage 1 | 471 | 476 | - | 657 | 625 | - | - | - | - | - | - | - |
| Stage 2 | 641 | 618 | - | 468 | 468 | - | - | - | - | - | - | - |
| Platoon blocked, % | | | | | | | | - | - | | - | - |
| Mov Cap-1 Maneuver | 196 | 226 | 535 | 207 | 224 | 719 | 1007 | - | - | 1225 | - | - |
| Mov Cap-2 Maneuver | 196 | 226 | - | 207 | 224 | - | - | - | - | - | - | - |
| Stage 1 | 460 | 454 | - | 641 | 610 | - | - | - | - | - | - | - |
| Stage 2 | 593 | 603 | - | 436 | 446 | - | - | - | - | - | - | - |
| | | | | | | | | | | | | |
| Approach | EB | | WB | | | NB | | | SB | | | |
| HCM Control Delay, s | 21 | | 18.7 | | | 0.5 | | | 0.5 | | | |
| HCM LOS | C | | C | | | | | | | | | |
| | | | | | | | | | | | | |
| Minor Lane/Major Mvmt | NBL | NBT | NBR | EBLn1WBLn1 | SBL | SBT | SBR | | | | | |
| Capacity (veh/h) | 1007 | - | - | 256 | 333 | 1225 | - | - | | | | |
| HCM Lane V/C Ratio | 0.019 | - | - | 0.121 | 0.214 | 0.032 | - | - | | | | |
| HCM Control Delay (s) | 8.6 | 0 | - | 21 | 18.7 | 8 | 0 | - | | | | |
| HCM Lane LOS | A | A | - | C | C | A | A | - | | | | |
| HCM 95th %tile Q(veh) | 0.1 | - | - | 0.4 | 0.8 | 0.1 | - | - | | | | |

Timings

105: Elkcarn Blvd & Lake Helen Osteen

03/01/2024



| Lane Group | SEL | SET | NWL | NWT | NEL | NET | SWL | SWT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | | |
| Traffic Volume (vph) | 36 | 314 | 22 | 286 | 191 | 419 | 105 | 247 |
| Future Volume (vph) | 36 | 314 | 22 | 286 | 191 | 419 | 105 | 247 |
| Turn Type | pm+pt | NA | pm+pt | NA | pm+pt | NA | pm+pt | NA |
| Protected Phases | 5 | 2 | 1 | 6 | 3 | 8 | 7 | 4 |
| Permitted Phases | 2 | | 6 | | 8 | | 4 | |
| Detector Phase | 5 | 2 | 1 | 6 | 3 | 8 | 7 | 4 |
| Switch Phase | | | | | | | | |
| Minimum Initial (s) | 5.0 | 16.0 | 5.0 | 16.0 | 5.0 | 6.0 | 5.0 | 6.0 |
| Minimum Split (s) | 14.0 | 25.0 | 14.0 | 25.0 | 13.5 | 13.0 | 13.5 | 13.0 |
| Total Split (s) | 29.0 | 49.0 | 29.0 | 49.0 | 28.5 | 32.0 | 28.5 | 32.0 |
| Total Split (%) | 20.9% | 35.4% | 20.9% | 35.4% | 20.6% | 23.1% | 20.6% | 23.1% |
| Yellow Time (s) | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 4.0 | 5.5 | 4.0 |
| All-Red Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 9.0 | 9.0 | 9.0 | 9.0 | 8.5 | 7.0 | 8.5 | 7.0 |
| Lead/Lag | Lead | Lag | Lead | Lag | Lead | Lag | Lead | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | Min | None | Min | None | None | None | None |
| Act Effect Green (s) | 38.5 | 34.4 | 37.6 | 34.0 | 40.5 | 28.4 | 34.0 | 25.2 |
| Actuated g/C Ratio | 0.36 | 0.32 | 0.35 | 0.32 | 0.38 | 0.27 | 0.32 | 0.24 |
| v/c Ratio | 0.16 | 0.80 | 0.10 | 0.82 | 0.52 | 0.92 | 0.47 | 0.64 |
| Control Delay | 20.6 | 44.9 | 20.0 | 46.9 | 27.9 | 66.8 | 30.2 | 48.7 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 20.6 | 44.9 | 20.0 | 46.9 | 27.9 | 66.8 | 30.2 | 48.7 |
| LOS | C | D | B | D | C | E | C | D |
| Approach Delay | | 43.1 | | 45.6 | | 55.0 | | 43.4 |
| Approach LOS | | D | | D | | D | | D |

Intersection Summary

Cycle Length: 138.5

Actuated Cycle Length: 107

Natural Cycle: 90

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.92

Intersection Signal Delay: 47.6

Intersection LOS: D

Intersection Capacity Utilization 79.2%

ICU Level of Service D

Analysis Period (min) 15





















Splits and Phases: 105: Elkcarn Blvd & Lake Helen Osteen

| | | | |
|------|------|--------|------|
| Ø1 | Ø2 | Ø3 | Ø4 |
| 29 s | 49 s | 28.5 s | 32 s |
| Ø5 | Ø6 | Ø7 | Ø8 |
| 29 s | 49 s | 28.5 s | 32 s |

HCM 6th Signalized Intersection Summary

105: Elkcarn Blvd & Lake Helen Osteen



















03/01/2024

| |  |  |  |  |  |  |  |  |  |  |  |  |
|------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | SEL | SET | SER | NWL | NWT | NWR | NEL | NET | NER | SWL | SWT | SWR |
| Lane Configurations |  |  | |  |  | |  |  | |  |  | |
| Traffic Volume (veh/h) | 36 | 314 | 128 | 22 | 286 | 162 | 191 | 419 | 16 | 105 | 247 | 17 |
| Future Volume (veh/h) | 36 | 314 | 128 | 22 | 286 | 162 | 191 | 419 | 16 | 105 | 247 | 17 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1856 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1885 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 38 | 331 | 135 | 23 | 301 | 171 | 201 | 441 | 17 | 111 | 260 | 18 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh, % | 3 | 2 | 2 | 2 | 2 | 2 | 2 | 1 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 173 | 393 | 160 | 178 | 338 | 192 | 350 | 461 | 18 | 206 | 368 | 25 |
| Arrive On Green | 0.03 | 0.31 | 0.31 | 0.02 | 0.30 | 0.30 | 0.11 | 0.26 | 0.26 | 0.07 | 0.21 | 0.21 |
| Sat Flow, veh/h | 1767 | 1263 | 515 | 1781 | 1120 | 636 | 1781 | 1803 | 70 | 1781 | 1729 | 120 |
| Grp Volume(v), veh/h | 38 | 0 | 466 | 23 | 0 | 472 | 201 | 0 | 458 | 111 | 0 | 278 |
| Grp Sat Flow(s),veh/h/ln | 1767 | 0 | 1778 | 1781 | 0 | 1756 | 1781 | 0 | 1873 | 1781 | 0 | 1849 |
| Q Serve(g_s), s | 1.4 | 0.0 | 23.9 | 0.9 | 0.0 | 25.1 | 8.4 | 0.0 | 23.6 | 4.7 | 0.0 | 13.6 |
| Cycle Q Clear(g_c), s | 1.4 | 0.0 | 23.9 | 0.9 | 0.0 | 25.1 | 8.4 | 0.0 | 23.6 | 4.7 | 0.0 | 13.6 |
| Prop In Lane | 1.00 | | 0.29 | 1.00 | | 0.36 | 1.00 | | 0.04 | 1.00 | | 0.06 |
| Lane Grp Cap(c), veh/h | 173 | 0 | 553 | 178 | 0 | 530 | 350 | 0 | 479 | 206 | 0 | 393 |
| V/C Ratio(X) | 0.22 | 0.00 | 0.84 | 0.13 | 0.00 | 0.89 | 0.57 | 0.00 | 0.96 | 0.54 | 0.00 | 0.71 |
| Avail Cap(c_a), veh/h | 477 | 0 | 727 | 499 | 0 | 718 | 519 | 0 | 479 | 452 | 0 | 473 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 25.5 | 0.0 | 31.4 | 25.3 | 0.0 | 32.6 | 26.5 | 0.0 | 35.9 | 29.2 | 0.0 | 35.7 |
| Incr Delay (d2), s/veh | 0.6 | 0.0 | 6.9 | 0.3 | 0.0 | 10.5 | 1.5 | 0.0 | 30.3 | 2.2 | 0.0 | 3.8 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 0.6 | 0.0 | 10.9 | 0.4 | 0.0 | 11.8 | 3.6 | 0.0 | 14.4 | 2.1 | 0.0 | 6.4 |
| Unsig. Movement Delay, s/veh | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 26.1 | 0.0 | 38.4 | 25.6 | 0.0 | 43.1 | 27.9 | 0.0 | 66.2 | 31.4 | 0.0 | 39.5 |
| LnGrp LOS | C | A | D | C | A | D | C | A | E | C | A | D |
| Approach Vol, veh/h | | 504 | | | 495 | | | 659 | | | 389 | |
| Approach Delay, s/veh | | 37.4 | | | 42.3 | | | 54.5 | | | 37.2 | |
| Approach LOS | | D | | | D | | | D | | | D | |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 11.3 | 39.4 | 19.2 | 27.8 | 12.2 | 38.5 | 15.0 | 32.0 | | | | |
| Change Period (Y+Rc), s | 9.0 | 9.0 | 8.5 | 7.0 | 9.0 | 9.0 | 8.5 | 7.0 | | | | |
| Max Green Setting (Gmax), s | 20.0 | 40.0 | 20.0 | 25.0 | 20.0 | 40.0 | 20.0 | 25.0 | | | | |
| Max Q Clear Time (g_c+I1), s | 2.9 | 25.9 | 10.4 | 15.6 | 3.4 | 27.1 | 6.7 | 25.6 | | | | |
| Green Ext Time (p_c), s | 0.0 | 2.5 | 0.4 | 1.0 | 0.0 | 2.4 | 0.2 | 0.0 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 44.1 | | | | | | | | | |
| HCM 6th LOS | | | D | | | | | | | | | |

Timings

101: Catalina Blvd & Howland Blvd

03/04/2024

| |  |  |  |  |  |  |  |  |  |
|----------------------|---|---|---|---|---|---|---|---|---|
| Lane Group | SEL | SET | NWL | NWT | NEL | NET | SWL | SWT | SWR |
| Lane Configurations |  |  |  |  |  |  |  |  |  |
| Traffic Volume (vph) | 140 | 549 | 31 | 1047 | 113 | 115 | 133 | 106 | 540 |
| Future Volume (vph) | 140 | 549 | 31 | 1047 | 113 | 115 | 133 | 106 | 540 |
| Turn Type | pm+pt | NA | pm+pt | NA | pm+pt | NA | Perm | NA | Perm |
| Protected Phases | 1 | 6 | 5 | 2 | 7 | 4 | | 8 | |
| Permitted Phases | 6 | | 2 | | 4 | | 8 | | 8 |
| Detector Phase | 1 | 6 | 5 | 2 | 7 | 4 | 8 | 8 | 8 |
| Switch Phase | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 11.0 | 5.0 | 11.0 | 5.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Minimum Split (s) | 13.5 | 19.5 | 13.5 | 19.5 | 12.0 | 14.0 | 14.0 | 14.0 | 14.0 |
| Total Split (s) | 19.0 | 65.0 | 13.6 | 59.6 | 14.0 | 71.4 | 57.4 | 57.4 | 57.4 |
| Total Split (%) | 12.7% | 43.3% | 9.1% | 39.7% | 9.3% | 47.6% | 38.3% | 38.3% | 38.3% |
| Yellow Time (s) | 5.0 | 5.0 | 5.0 | 5.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 8.5 | 8.5 | 8.5 | 8.5 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Lead/Lag | Lead | Lag | Lead | Lag | Lead | | Lag | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | | Yes | Yes | Yes |
| Recall Mode | None | Max | None | Max | None | None | None | None | None |
| Act Effect Green (s) | 68.4 | 62.3 | 56.4 | 51.3 | 58.6 | 58.6 | 44.5 | 44.5 | 44.5 |
| Actuated g/C Ratio | 0.47 | 0.43 | 0.39 | 0.36 | 0.41 | 0.41 | 0.31 | 0.31 | 0.31 |
| v/c Ratio | 0.86 | 0.42 | 0.10 | 0.96 | 0.25 | 0.22 | 0.37 | 0.20 | 0.94 |
| Control Delay | 74.4 | 31.5 | 22.9 | 63.8 | 28.2 | 25.7 | 41.6 | 37.0 | 58.0 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 74.4 | 31.5 | 22.9 | 63.8 | 28.2 | 25.7 | 41.6 | 37.0 | 58.0 |
| LOS | E | C | C | E | C | C | D | D | E |
| Approach Delay | | 39.8 | | 62.7 | | 26.8 | | 52.3 | |
| Approach LOS | | D | | E | | C | | D | |

Intersection Summary

Cycle Length: 150

Actuated Cycle Length: 144.3

Natural Cycle: 100

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.96

Intersection Signal Delay: 51.0

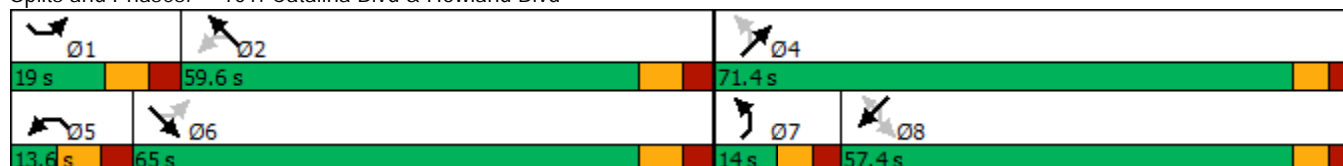
Intersection LOS: D

Intersection Capacity Utilization 90.0%

ICU Level of Service E

Analysis Period (min) 15






















Splits and Phases: 101: Catalina Blvd & Howland Blvd



HCM 6th Signalized Intersection Summary

101: Catalina Blvd & Howland Blvd

03/04/2024

| |  |  |  |  |  |  |  |  |  |  |  |  |
|------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | SEL | SET | SER | NWL | NWT | NWR | NEL | NET | NER | SWL | SWT | SWR |
| Lane Configurations |  |  | |  |  | |  |  | |  |  |  |
| Traffic Volume (veh/h) | 140 | 549 | 34 | 31 | 1047 | 82 | 113 | 115 | 37 | 133 | 106 | 540 |
| Future Volume (veh/h) | 140 | 549 | 34 | 31 | 1047 | 82 | 113 | 115 | 37 | 133 | 106 | 540 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | No | | | No | | | No | | | No | | |
| Adj Sat Flow, veh/h/ln | 1841 | 1826 | 1856 | 1870 | 1856 | 1856 | 1885 | 1885 | 1856 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 147 | 578 | 36 | 33 | 1102 | 86 | 119 | 121 | 39 | 140 | 112 | 517 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh, % | 4 | 5 | 3 | 2 | 3 | 3 | 1 | 1 | 3 | 2 | 2 | 2 |
| Cap, veh/h | 173 | 1276 | 79 | 298 | 1134 | 88 | 368 | 587 | 189 | 460 | 628 | 532 |
| Arrive On Green | 0.07 | 0.38 | 0.38 | 0.02 | 0.34 | 0.34 | 0.05 | 0.43 | 0.43 | 0.34 | 0.34 | 0.34 |
| Sat Flow, veh/h | 1753 | 3317 | 206 | 1781 | 3313 | 258 | 1795 | 1366 | 440 | 1226 | 1870 | 1585 |
| Grp Volume(v), veh/h | 147 | 302 | 312 | 33 | 586 | 602 | 119 | 0 | 160 | 140 | 112 | 517 |
| Grp Sat Flow(s),veh/h/ln | 1753 | 1735 | 1789 | 1781 | 1763 | 1809 | 1795 | 0 | 1806 | 1226 | 1870 | 1585 |
| Q Serve(g_s), s | 8.1 | 19.4 | 19.4 | 1.8 | 48.9 | 49.0 | 6.4 | 0.0 | 8.3 | 12.8 | 6.3 | 48.0 |
| Cycle Q Clear(g_c), s | 8.1 | 19.4 | 19.4 | 1.8 | 48.9 | 49.0 | 6.4 | 0.0 | 8.3 | 12.8 | 6.3 | 48.0 |
| Prop In Lane | 1.00 | | 0.12 | 1.00 | | 0.14 | 1.00 | | 0.24 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 173 | 667 | 688 | 298 | 603 | 619 | 368 | 0 | 776 | 460 | 628 | 532 |
| V/C Ratio(X) | 0.85 | 0.45 | 0.45 | 0.11 | 0.97 | 0.97 | 0.32 | 0.00 | 0.21 | 0.30 | 0.18 | 0.97 |
| Avail Cap(c_a), veh/h | 178 | 667 | 688 | 315 | 603 | 619 | 368 | 0 | 779 | 462 | 631 | 535 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 37.1 | 34.2 | 34.3 | 31.1 | 48.4 | 48.4 | 29.4 | 0.0 | 26.6 | 37.2 | 35.0 | 48.9 |
| Incr Delay (d2), s/veh | 29.8 | 2.2 | 2.2 | 0.2 | 30.2 | 30.0 | 0.5 | 0.0 | 0.1 | 0.4 | 0.1 | 31.4 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 4.8 | 8.4 | 8.7 | 0.8 | 25.9 | 26.6 | 2.9 | 0.0 | 3.7 | 3.9 | 3.0 | 23.6 |
| Unsig. Movement Delay, s/veh | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 66.9 | 36.4 | 36.4 | 31.2 | 78.6 | 78.4 | 29.9 | 0.0 | 26.8 | 37.5 | 35.2 | 80.3 |
| LnGrp LOS | E | D | D | C | E | E | C | A | C | D | D | F |
| Approach Vol, veh/h | 761 | | | 1221 | | | 279 | | | 769 | | |
| Approach Delay, s/veh | 42.3 | | | 77.3 | | | 28.1 | | | 65.9 | | |
| Approach LOS | D | | | E | | | C | | | E | | |
| Timer - Assigned Phs | 1 | 2 | | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 18.6 | 59.6 | | 71.2 | 12.2 | 65.9 | 14.0 | 57.2 | | | | |
| Change Period (Y+Rc), s | 8.5 | 8.5 | | 7.0 | 8.5 | 8.5 | 7.0 | 7.0 | | | | |
| Max Green Setting (Gmax), s | 10.5 | 51.1 | | 64.4 | 5.1 | 56.5 | 7.0 | 50.4 | | | | |
| Max Q Clear Time (g_c+I1), s | 10.1 | 51.0 | | 10.3 | 3.8 | 21.4 | 8.4 | 50.0 | | | | |
| Green Ext Time (p_c), s | 0.0 | 0.1 | | 1.0 | 0.0 | 3.6 | 0.0 | 0.2 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | 61.1 | | | | | | | | | | | |
| HCM 6th LOS | E | | | | | | | | | | | |

Appendix H

Internal Queue Assessment



Appendix I

Signal Four Analytics Crash Summary Screenshot



Search Crashes



Crashes in Custom Area

From 1/1/2018 - 12/31/2023



Injury Summary [Common Attributes](#) [FDOT Attributes](#)

| | Total | Fatal Crashes | Serious Injury Cras... | Injury Crashes | Property Damage ... |
|-----------------------------|-------|---------------|------------------------|----------------|---------------------|
| Crashes | 1 | 0 | 0 | 0 | 1 |
| Fatalities (within 30 Days) | 0 | 0 | 0 | 0 | 0 |
| Incapacitating Injuries | 0 | 0 | 0 | 0 | 0 |
| Non-Incapacitating Injuries | 0 | 0 | 0 | 0 | 0 |

Charting

